

FCC ID: A3LSMG998U

Power Density Simulation Report

Revision A

December 11, 2020

SAMSUNG ELECTRONICS

1. Simulation methodology for Power Density (PD)

1.1 Simulation tool

1.1.1 Tool description

For the simulation approach to calculating power density (PD) evaluation for mobile phone with mmWave antenna modules, ANSYS Electromagnetics suite version 2020.R2 (HFSS) is used. ANSYS HFSS is one of several commercial tools for 3D full-wave electromagnetic simulation used for antenna and RF structure design of high frequency component. ANSYS Electromagnetics suite version 2020.R2 (HFSS) is implemented based on Finite Element Method (FEM), which operates in the frequency domain.

1.1.2 Mesh and Convergence criteria

To solve the PD analysis using FEM, volume area containing simulated objects should be subdivided into electrically small parts that are called finite elements as the unknown functions. To subdivide system, the adaptive mesh technique in ANSYS Electromagnetics suite version 2020.R2 (HFSS) is used. ANSYS Electromagnetics suite version 2020.R2 (HFSS) starts to refine the initial mesh based on wavelength and calculate the error to iterative process for adaptive mesh refinement. The determination parameter of the number of iteration in ANSYS Electromagnetics suite version 2020.R2 (HFSS) is defined as convergence criteria, delta S, and the iterative adaptive mesh process repeats until the delta S is met. In ANSYS Electromagnetics suite version 2020.R2 (HFSS), the accuracy of converged results depends on the delta S. Figure 1 is an example of adaptive mesh of the device (cross-section of top view).

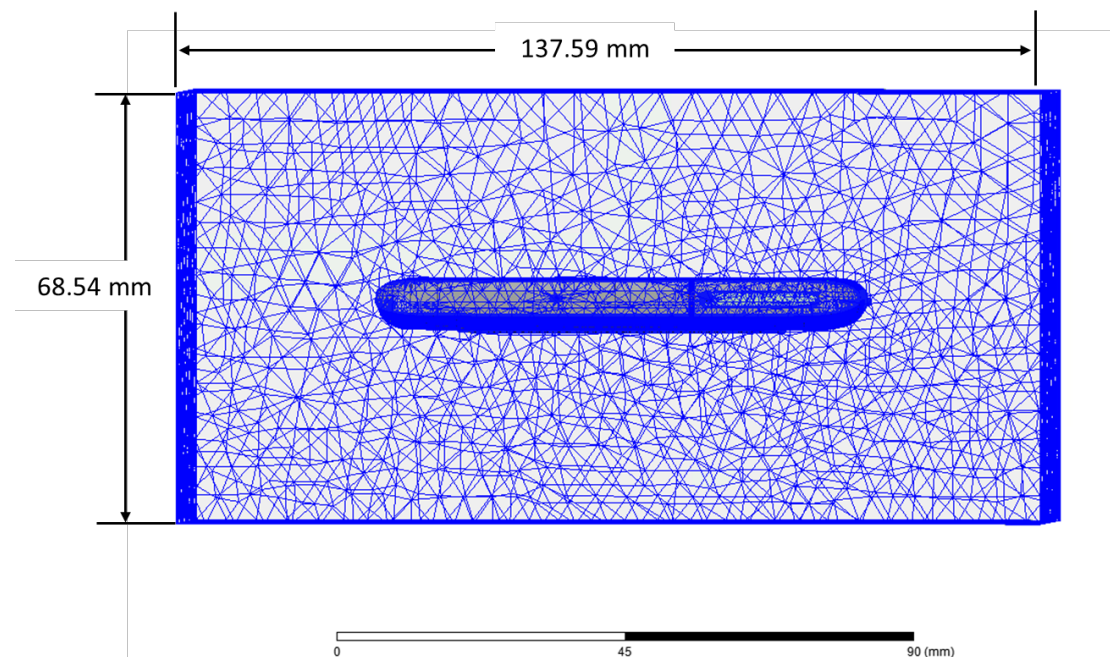


Figure 1 Example of the adaptive mesh technique (Top view)

1.1.3 Power density calculation

After solving 3D full-wave electromagnetic simulation, various kinds of physical quantities can be obtained. To calculate PD evaluation, two physical quantities, an electric field ($\vec{E}$) and a magnetic field ($\vec{H}$) are needed. The actual consumption power can be expressed as the real term of the Poynting vector ($\vec{S}$) from the cross product of $\vec{E}$ and complex conjugation of $\vec{H}$ as shown below:

$$\langle \vec{S} \rangle = \text{Re} \left(\frac{1}{2} \vec{E} \times \vec{H}^* \right)$$

$\langle \vec{S} \rangle$ can be expressed as point power density based on a peak value of each spatial point on mesh grids, and obtained directly from ANSYS Electromagnetics suite version 2020.R2 (HFSS).

From the point power density $\langle \vec{S} \rangle$, the spatial-averaged power density (PD_{av}) on an evaluated area (A) can be derived as shown below:

$$PD_{av} = \frac{1}{A} \int_A \langle \vec{S} \rangle \cdot d\vec{s} = \frac{1}{2A_{av}} \iint_{A_{av}} \| \text{Re}\{E \times H^*\} \| dA$$

, where the spatial-averaged power density (PD_{av}) is total power density value considering on x, y and z components of point power density $\langle \vec{S} \rangle$ and the evaluated area (A) is 4cm^2 .

1.2 Simulation setup

1.2.1 3D modeling

Figure 2 shows the simulation model which is mounted two mmWave antenna modules. The simulation modeling includes most of the entire structure of device itself such as PCB, metal frame, battery, cables, and legacy antennas as well as mmWave antenna modules called as Ant K and Ant L. The modeling contains the entire EUT to enable a Smart transmit GEN2, as well. Ant K is placed on the left side and antennas are facing the left side, and Ant L is placed on the right side and antennas are facing the right side of the device.

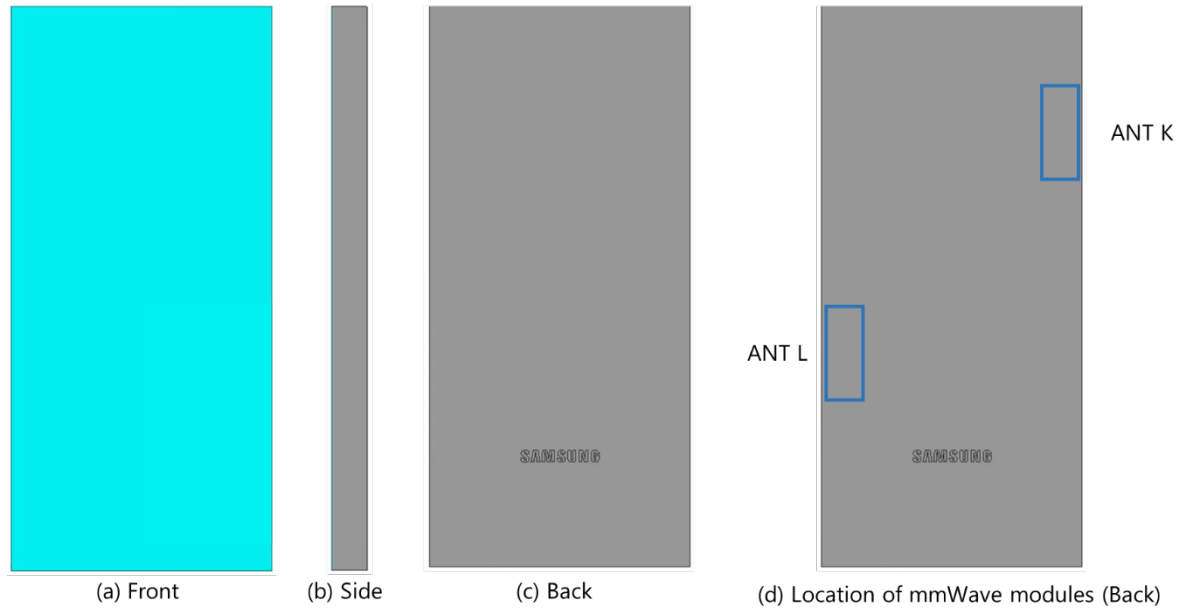


Figure 2 Simulation model which is mounted two mmWave antenna modules

1.2.2 PD evaluation planes

Table 1 shows the PD evaluation planes for each mmWave antenna module and Figure 3 shows the PD evaluation planes and truncation area of the simulation model to find worst case of beamforming cases. In Ant K case, five PD evaluation planes except bottom side are set up. The Ant K is placed at the upper of the device and the bottom side is excluded from the worst case because the distance from the bottom side is more than 10 lambda at 28GHz and 39 GHz. In Ant L case, five PD evaluation planes except top side are set up, Ant L is placed at the lower of the device and the top side is excluded from the worst case for the same reason as Ant K.

Please note that the “right” and “left” edge of mentioned in this report are defined from the perspective of looking at the device from the front side.

Table 1. PD evaluation planes

Module	Front	Back	Left From Front View	Right From Front View	Top	Bottom
	S1	S2	S3	S4	S5	S6
Ant K	O	O	O	O	O	X
Ant L	O	O	O	O	X	O

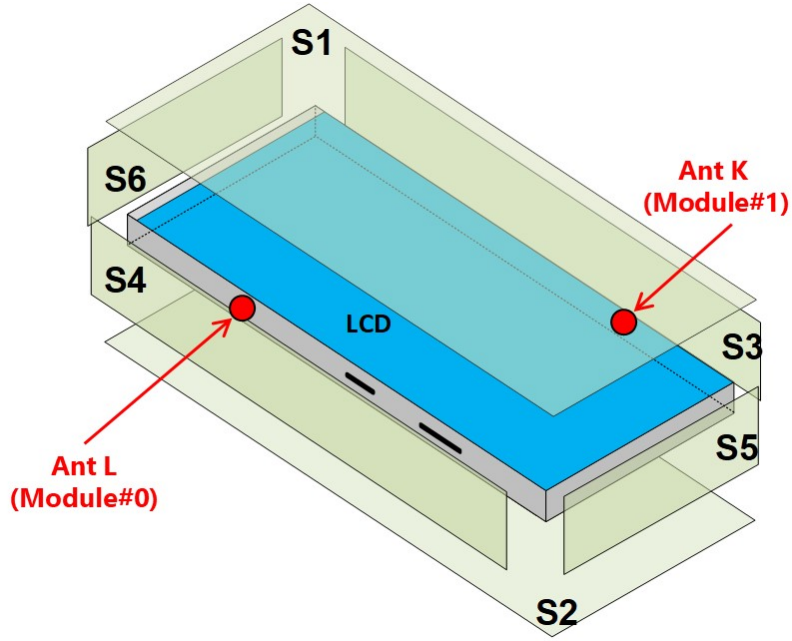


Figure 3. PD evaluation planes

1.2.3 Boundary condition

To simulate electromagnetic tool based on FEM, the boundary condition allows electromagnetic waves to be electrically open at the boundary and radiated far away without reflection. ANSYS Electromagnetics suite version 2020.R2 (HFSS) can support the absorbing boundary condition (ABC) for radiation boundary and make normally a quarter wave length from the radiating structure. In this report, to cover all beamforming cases of mmWave antenna modules, 40 mm spacing from the device for each surfaces were adopted. This distance is sufficiently large enough for “Qualcomm MG script” to extract valid E- and H-fields from all adjacent exposure surfaces of the EUT.

1.2.4 Source excitation condition

The number of antenna ports of ANT K and ANT L for source excitation are the same. The antenna port of ANT K and L is divided into 10 ports for n261 1 x 5 patch array antennas, 10 ports for n260 1 x 5 patch array antennas. In the 10 ports included in each patch antenna, 5 ports are divided into vertical polarization feeding, and the other 5 ports are divided into horizontal polarization feeding.

Figure 4 shows the ANT K module structure and surrounding structure. The ANT K module is encrypted in the ANSYS Electromagnetics suite (HFSS) and can only check the feeding position.

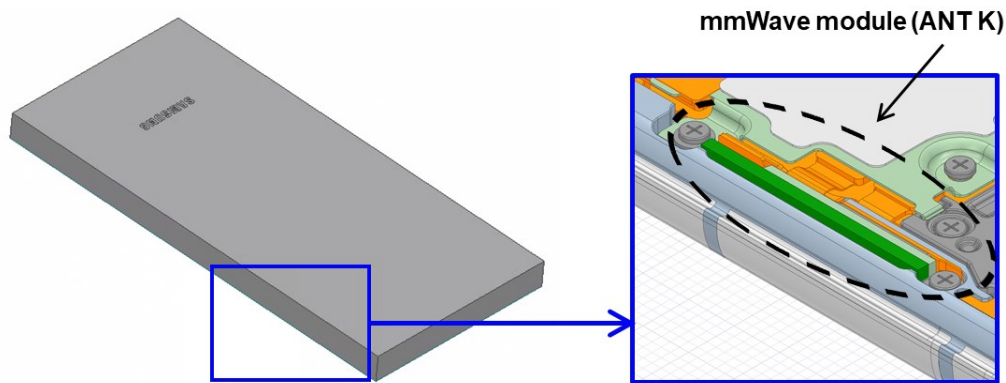


Figure 4. mmWave module (ANT K)

After finishing 3D full wave electromagnetic simulation of modeling structure, the magnitude and phase information can be loaded for each port by using “Edit Sources” function in ANSYS Electromagnetics suite (HFSS). Figure 5 shows an example of antenna port excitations.

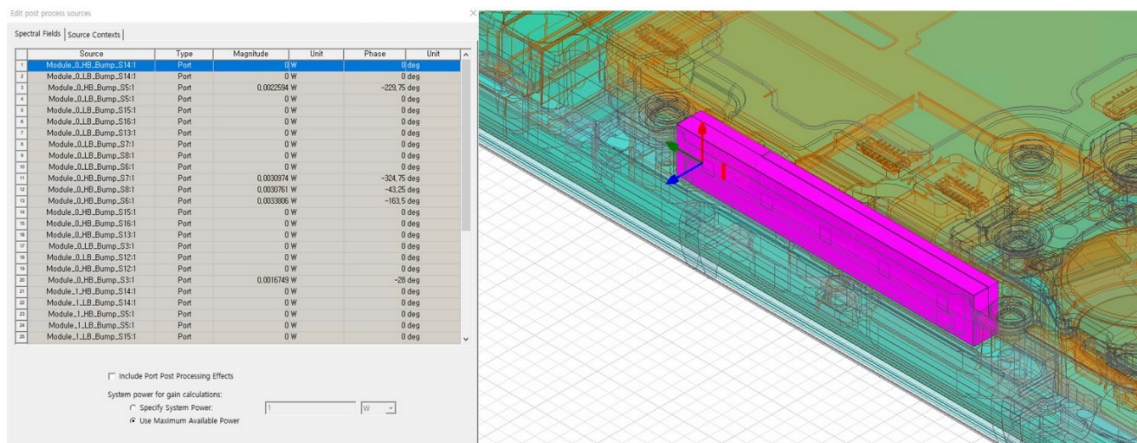


Figure 5. An example of port excitation (ANT K)

Since ANSYS Electromagnetics suite (HFSS) uses FEM solver based on frequency domain analysis method, the input source for the port excitation applies sinusoidal waveform for each frequency.

1.2.5 Condition of simulation completion

The simulation completion condition of ANSYS Electromagnetics suite (HFSS) is defined as delta S. The ANSYS Electromagnetics suite (HFSS) calculates the S-parameter for the mesh conditions of each step and determines whether to proceed with the operation of the next step by comparing the difference between the S-parameters in the previous step. A difference between the previous step and the current step of S-parameter is expressed as delta S, and the delta S generally sets 0.02. The simulation result of this report is the result of setting delta S to 0.02.

2. Simulation verification

2.1 Spatial-averaged power density and $\text{sim.power}_{\text{limit}}$

As mentioned in the previous chapter, the Poynting vector ($\vec{S}$) can be obtained through cross product of an electric field ($\vec{E}$) and complex conjugate of a magnetic field ($\vec{H}$). The real term of the Poynting vector can be described as the point power density or peak power density. Using the point power density, the spatial-averaged power density can be obtained by the integral of 4 cm^2 at 2.5 mm intervals of the point power density result. Figure 6 shows examples of the distribution plot of point power density and the averaged power density.

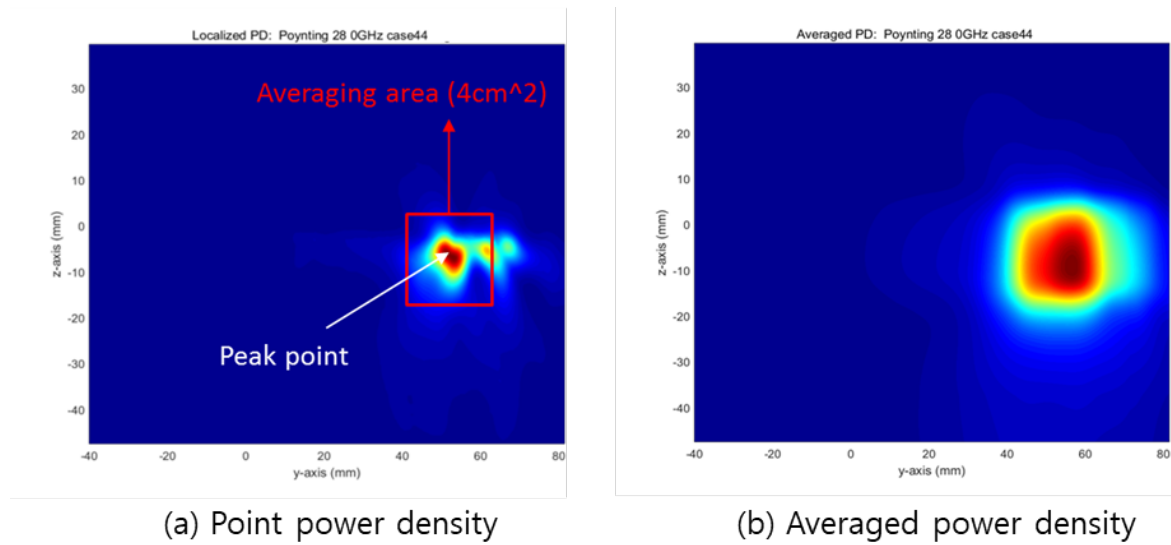


Figure 6. Power density distribution (Example)

For the Smart transmit GEN2, the “Qualcomm MG script” were used to extract E- and H-fields from the validated simulation and to assess the mutual coupling between all the mmWave antenna modules and all the beams in the codebook to determine the backoff value for each mmWave module. Note the assessment and backoff value derivation are automated with “Qualcomm MG script”. Once the script is done with assessment, it will provide the $\text{sim.power}_{\text{limit}}$ (backoff is already included) for all the beams for all three channels for the specified PD_design_target . This mode take the minimum $\text{sim.power}_{\text{limit}}$ out of all three channels (low, mid and high) and use the resulted $\text{sim.power}_{\text{limit}}$.

2.2 Comparison between simulation, measurement

In this section, the simulated-power density distributions and measured-power density distributions are compared to each mmWave antenna. Furthermore, to verify the Smart transmit GEN2, the PD distributions printing out from the “Qualcomm MG script” are added.

Based on comparison of power density distributions, the power densities of simulated, measured and the “Qualcomm MG Script” have a good correlation. The discrepancy in amplitude between the “Qualcomm MG Script” 4 cm^2 averaged power density and measured 4 cm^2 averaged power density is

considered as housing influence and used in determining input power limit for each beam for RF exposure compliance.

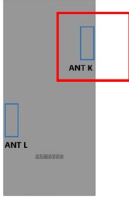
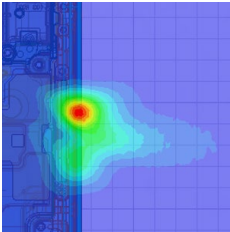
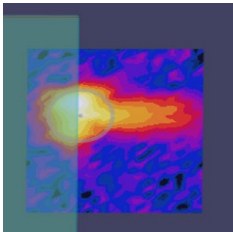
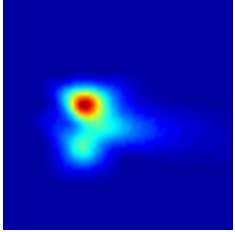
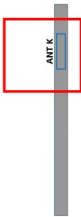
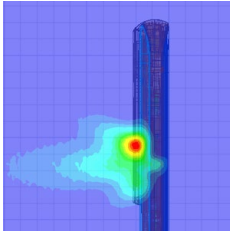
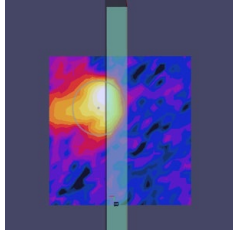
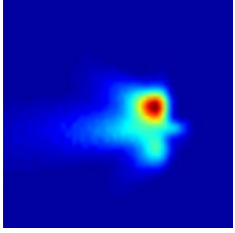
The input powers per each active port are listed below for both Simulation and Measurement validation and power density characterization. For Simulation, these values were entered directly into HFSS model. For measurement, FTM S/W was used to input these values for each active port also.

Mode/Band	Antenna	Input Power (dBm)	Input Power (dBm)
		SISO	MIMO
5G NR n261	K Patch	6.0	6.0
	L Patch	6.0	6.0
5G NR n260	K Patch	6.0	6.0
	L Patch	6.0	6.0

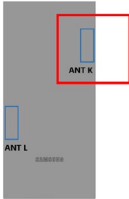
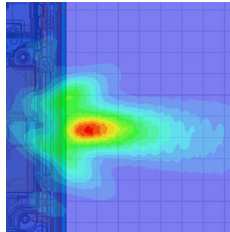
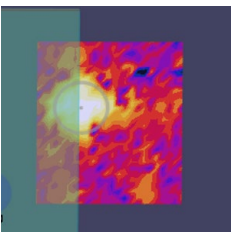
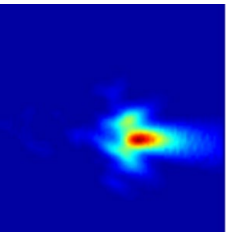
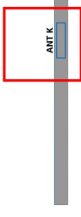
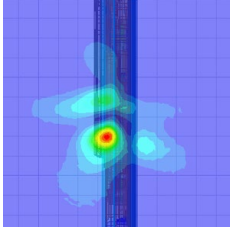
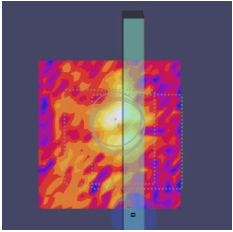
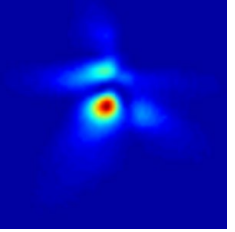
* The below simulation and measurement result were performed at 2mm evaluation distance and 28GHz / 38.5GHz. The *input.power.limit* was determined based on below results.

					4cm ² avg. PD (mW/cm ²)	
Band	Beam ID	Antenna	Surface	Channel	Meas.	Sim
n261	22	K	Rear	Mid Ch. 2077891 (27923.5 MHz)	1.110	1.363
			Left		1.160	1.374
			Rear		0.610	0.659
			Left		0.441	0.919
	150	L	Rear		1.130	1.627
			Right		1.290	1.603
			Rear		1.380	1.161
			Right		0.618	1.414
n260	25	K	Rear	Mid Ch. 2253331 (38449.9 MHz)	0.321	0.348
			Left		0.655	0.575
			Rear		0.551	0.832
			Left		0.748	1.005
	161	L	Rear		0.431	0.430
			Right		0.740	0.701
			Rear		0.524	0.815
			Right		0.674	0.891

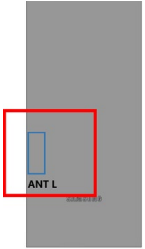
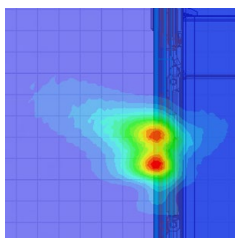
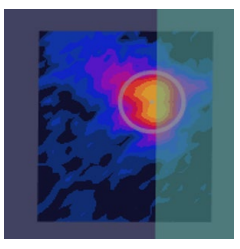
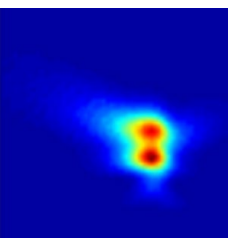
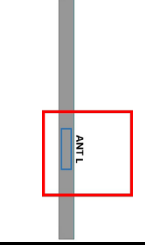
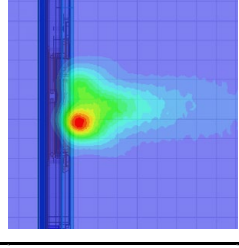
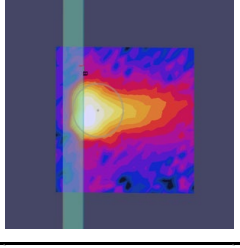
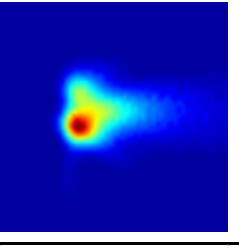
● Table 2-1, n261 ANT K-Patch: Mid Channel, Beam ID 22

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
22	S2 (Rear)				
	S3 (Left)				

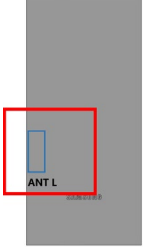
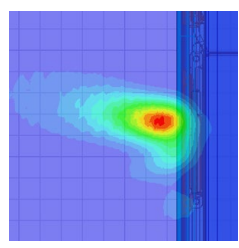
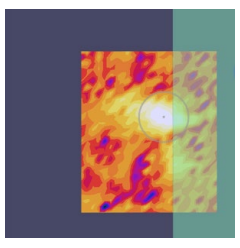
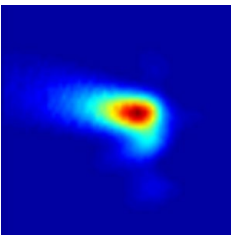
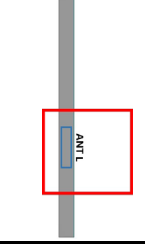
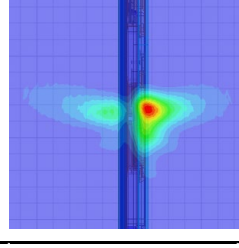
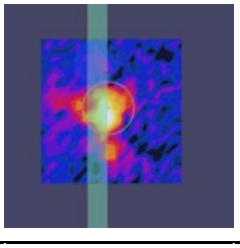
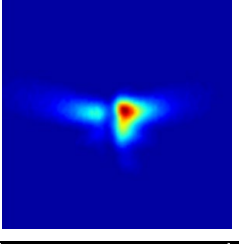
● Table 2-2, n261 ANT K-Patch: Mid Channel, Beam ID 150 for Rear and 152 for Left surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
150	S2 (Rear)				
152	S3 (Left)				

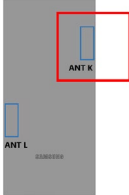
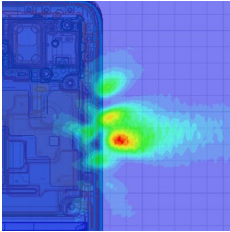
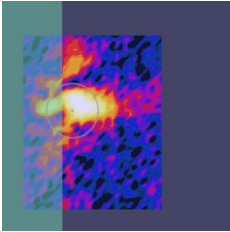
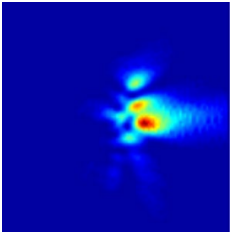
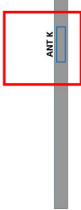
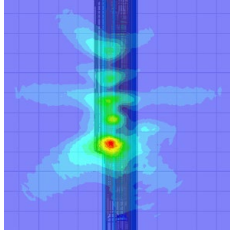
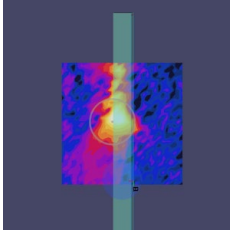
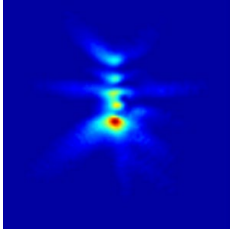
- Table 2-3, n261 ANT L-Patch: Mid Channel, Beam ID 18 for Rear and 26 for Right surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
18	S2 (Rear)				
	S4 (Right)				

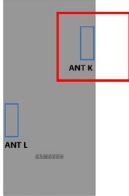
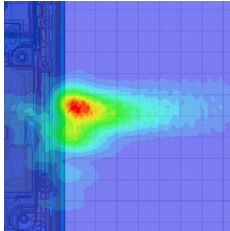
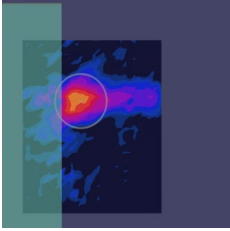
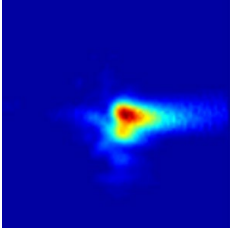
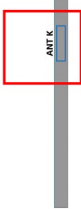
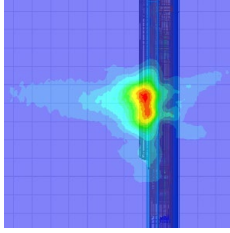
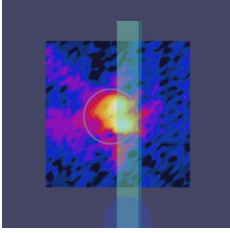
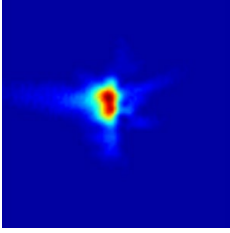
- Table 2-4, n261 ANT L-Patch: Mid Channel, Beam ID 155

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
155	S2 (Rear)				
	S4 (Right)				

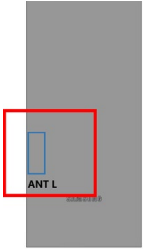
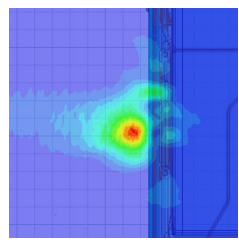
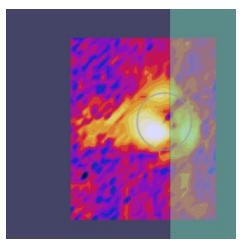
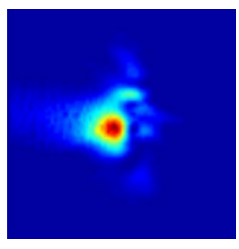
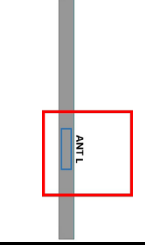
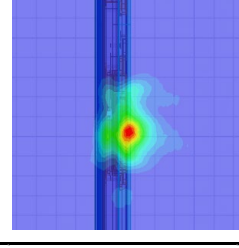
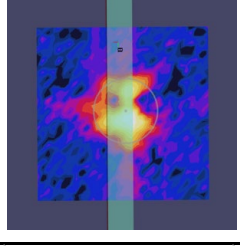
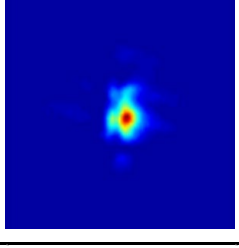
- Table 2-5, n260 ANT K-Patch: Mid Channel, Beam ID 25 for Rear and 35 for Left surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
25	S2 (Rear)				
35	S3 (Left)				

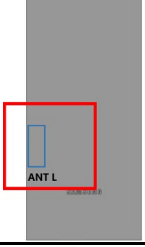
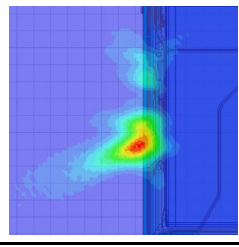
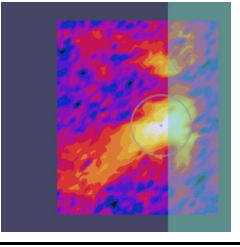
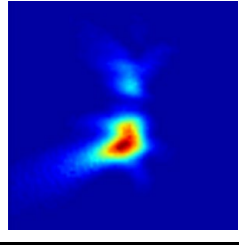
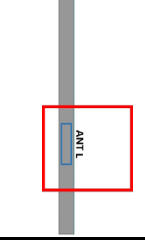
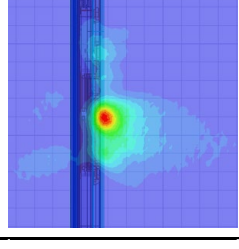
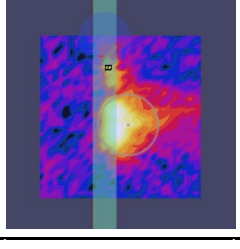
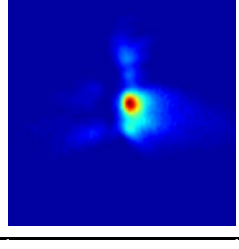
- Table 2-6, n260 ANT K-Patch: Mid Channel, Beam ID 161

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
161	S2 (Rear)				
	S3 (Left)				

● Table 2-7, n260 ANT L-Patch: Mid Channel, Beam ID 20

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
20	S2 (Rear)				
	S4 (Right)				

● Table 2-8, n260 ANT L-Patch: Mid Channel, Beam ID 147 for Rear and 157 for Right surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
147	S2 (Rear)				
157	S4 (Right)				

Worst-case surface:					S1 (Front surface)	
Worst-case location (x,y,z) in meters:					Worst 4cm2 PD value location is 0.02121m, 0.03179m, 0.00200m	
PD design target (W/m ²)					6.166	
Values printed from Qualcomm MG Script					Values obtained by OEM using EM simulation tool	
QTM #	Beam ID	c(ij) i = beam ID j = QTM #	Backoff factor b _j	verification.sim. power _{limit} (before backoffs) [dBm]	simulated 4cm2 PD(ij) at (0.02121, 0.03179, 0.00200) at verification.sim.power _{limit} on S1	C _{simulated} (ij)= 4cm ² PD(ij)/ PD_design_target
0	8	1.000	0.977	10.35	6.16238	0.999
1	163	0.008	0.977	5.21	0.05181	0.008
Verify 1:		$C(i,j) = C_{simulated}(i,j), i = 8, 163; j = 0, 1$				
Verify 2:		$b_0 * c(8,0) + b_1 * c(163,1) = 0.977 * 1.000 + 0.977 * 0.008 = 0.985 \leq 1$				

VERIFICATION3: Measured 4cm² PD on worst surface and combined PD at worst-case location for A3LSMG998U device with 2 QTMS. The device should be measured at the reference power level and scaled to the input.power.limit. The combined PD should be less than or equal to the *PD_Design_Target* within the uncertainty at the reference power level.

[n261 band]

QTM #	Beam ID	c(i,j) i = beam ID j = QTM #	Dominant surface	4cm ² PD at input.power.limit on QTM dominant surface (W/m ²)	input.power.limit (before permanent backoff)	Measured PD at reference power power level on Beam Dominant Surface (W/m ²)
0	2	0.999	S2 (Back)	4.463	8.5	2.510
1	24	0.015	S2 (Back)	3.965	3.9	6.430
combined PD at the worst-case location (x,y,z)				$c(2,0)*\text{meas.4cm}^2\text{PD}(2,0) + c(24,1)*\text{meas.4cm}^2\text{PD}(24,1)$ $= 0.999*4.463 + 0.015*3.965 = 4.518 \text{ W/m}^2$		
PD_design_target + uncertainty at reference power level of 0.5 dB				$= 6.166*10^{(0.5/10)} = 6.918 \text{ W/m}^2$		
Verify				combined PD < PD_design_target + uncertainty at reference power level		

[n260 band]

QTM #	Beam ID	c(i,j) i = beam ID j = QTM #	Dominant surface	4cm ² PD at input.power.limit on QTM dominant surface (W/m ²)	input.power.limit (before permanent backoff)	Measured PD at reference power power level on Beam Dominant Surface (W/m ²)
0	8	1.000	S1 (Front)	4.908	8.5	2.760
1	163	0.008	S3 (Left)	4.702	5	5.920
combined PD at the worst-case location (x,y,z)				$c(8,0)*\text{meas.4cm}^2\text{PD}(8,0) + c(163,1)*\text{meas.4cm}^2\text{PD}(163,1)$ $= 1.000*4.908 + 0.008*4.702 = 4.946 \text{ W/m}^2$		
PD_design_target + uncertainty at reference power level of 0.5 dB				$= 6.166*10^{(0.5/10)} = 6.918 \text{ W/m}^2$		
Verify				combined PD < PD_design_target + uncertainty at reference power level		

3 Simulation results

This section shows the PD simulation results of Ant K and Ant L at 28GHz and 39GHz for each evaluation plane specified in Table 1 at two separation distances of 2mm and 10mm. The ratio of PD exposure from front surface to the worst surface at 2mm, and the ratio of PD exposure from 2mm to 10mm evaluation distance for each beam are also reported in this section to support RF exposure analysis for simultaneous transmission scenarios performed in the Part 1 Near Field PD report.

The relative phase between beam pairs is not controlled in the chipset design. Therefore, the relative phase between each beam pair was considered mathematically to identify the worst case conditions. The below MIMO results represent the highest reported MIMO simulation results after sweeping across the relative phase between beams a 5° step interval from 0° to 360°,

The worst-case simulated PD determined from the tables in this section were used for conservativeness in *input.power.limit* determination in RF Exposure Part 0 Report.

3.1 PD for Low/Mid/High Channel at 28GHz / 39GHz

Table 2 & Table 3 show the PD simulation evaluation of Ant K patch antenna at 28GHz / 39GHz for the corresponding evaluation planes specified in Table 1. As shown, a per beam back-off for TER analysis is added to Table 4 (39GHz Ant. K). This back-off is originated by the 2mm PD ratio of (front surface) / (worst surface) which is used for TER calculation of 'Head' condition. If the ratio is large, the *input.power.limit* of this model should be decreased large enough to meet the TER analysis. To avoid the large back-off, therefore, the per beam back-off is adopted and the back-off are applied to several beam IDs in Table 4 to meet the 72% ratio of front / worst surface, satisfying the 'Head' TER analysis.

For the Ant. L, the TER analysis could be excluded with 10 dB contours criteria method based on the Appendix G.1.3 of 80-W2112-4 Rev. M (Qualcomm's Smart Transmit Part#1 document), so there is no per beam back-off for the Ant. L 39 GHz (Table 6).

3.1.1 Ant K– Patch Antenna

Table 3. PD of Ant K – patch antenna (28GHz – n261)

- K-patch Low CH

											max ratio out of all beams				max ratio out of all beams												
No.	Module	Type	Beam ID_1	Bema ID_2	Feed no.	4cm2 PD(mW/cm2)						63.0%		8.8%		4cm2 PD(mW/cm2) at 10mm evaluation distance						56.1%		56.1%		54.0%	
						S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Front 2mm)/(worst surface 2mm)	ratio (Top 2mm)/(worst surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	worst-ratio surface (10mm/2mm)	ratio (back 10mm)/(worst surface 2mm)	ratio (Left 10mm)/(worst surface 2mm)					
1	K	Patch	3	1	0.00	0.21	0.01	0.00	0.01	0.21	4.7%	2.4%	0.00	0.07	0.00	0.00	0.01	0.08	37.4%	37.4%	35.1%	35.1%	37.4%	37.4%	35.1%	35.1%	
2			4	1	0.00	0.32	0.01	0.00	0.02	0.31	4.7%	3.4%	0.00	0.11	0.01	0.00	0.01	0.14	44.2%	44.2%	42.2%	42.2%	44.2%	44.2%	42.2%	42.2%	
3			8	2	0.00	0.64	0.03	0.00	0.07	0.60	10.3%	4.1%	0.00	0.26	0.02	0.00	0.03	0.30	47.0%	47.0%	46.6%	46.6%	47.0%	47.0%	46.6%	46.6%	
4			9	2	0.00	0.47	0.00	0.00	0.03	0.46	5.9%	0.7%	0.00	0.18	0.00	0.00	0.02	0.26	46.6%	46.6%	46.6%	46.6%	46.6%	46.6%	46.6%	46.6%	
5			10	2	0.00	0.44	0.01	0.00	0.12	0.42	26.2%	1.4%	0.00	0.18	0.00	0.00	0.04	0.21	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	
6			13	2	0.00	0.48	0.01	0.00	0.03	0.53	6.1%	1.5%	0.00	0.20	0.01	0.00	0.01	0.25	48.2%	48.2%	48.2%	48.2%	48.2%	48.2%	48.2%	48.2%	
7			14	2	0.01	0.43	0.01	0.01	0.04	0.52	7.1%	1.9%	0.00	0.16	0.01	0.01	0.02	0.24	46.6%	46.6%	46.6%	46.6%	46.6%	46.6%	46.6%	46.6%	
8			20	5	0.01	1.12	0.10	0.01	0.12	1.17	10.2%	8.8%	0.01	0.53	0.07	0.01	0.06	0.65	56.1%	56.1%	56.1%	56.1%	56.1%	56.1%	56.1%	56.1%	
9			21	5	0.01	1.35	0.04	0.00	0.14	1.31	10.5%	2.6%	0.01	0.60	0.03	0.00	0.07	0.69	51.3%	51.3%	51.3%	51.3%	51.3%	51.3%	51.3%	51.3%	
10			22	5	0.01	1.44	0.01	0.00	0.16	1.43	10.9%	0.8%	0.01	0.67	0.01	0.00	0.07	0.79	54.5%	54.5%	54.5%	54.5%	54.5%	54.5%	54.5%	54.5%	
11			23	5	0.01	1.34	0.01	0.01	0.16	1.40	11.3%	0.9%	0.01	0.57	0.01	0.00	0.08	0.72	51.0%	51.0%	51.0%	51.0%	51.0%	51.0%	51.0%	51.0%	
12			24	5	0.02	0.88	0.01	0.04	0.11	0.98	11.1%	1.4%	0.02	0.31	0.01	0.03	0.05	0.42	42.8%	42.8%	42.8%	42.8%	42.8%	42.8%	42.8%	42.8%	
13			29	5	0.01	1.31	0.05	0.00	0.14	1.25	10.3%	3.8%	0.01	0.60	0.03	0.00	0.07	0.68	51.8%	51.8%	51.8%	51.8%	51.8%	51.8%	51.8%	51.8%	
14			30	5	0.01	1.33	0.05	0.00	0.15	1.25	10.8%	3.3%	0.01	0.59	0.03	0.00	0.07	0.70	51.7%	51.7%	51.7%	51.7%	51.7%	51.7%	51.7%	51.7%	
15			31	5	0.01	1.40	0.01	0.01	0.18	1.40	12.9%	0.7%	0.01	0.64	0.01	0.01	0.08	0.78	56.0%	56.0%	56.0%	56.0%	56.0%	56.0%	56.0%	56.0%	
16			32	5	0.01	1.21	0.02	0.01	0.14	1.33	10.6%	1.6%	0.01	0.49	0.02	0.01	0.07	0.62	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	
17			131	1	0.00	0.19	0.00	0.00	0.11	0.12	56.4%	1.1%	0.00	0.06	0.00	0.00	0.04	0.05	33.5%	33.5%	33.5%	33.5%	33.5%	33.5%	33.5%	33.5%	
18			132	1	0.00	0.15	0.01	0.00	0.09	0.10	61.8%	3.9%	0.00	0.06	0.00	0.00	0.04	0.05	41.4%	41.4%	41.4%	41.4%	41.4%	41.4%	41.4%	41.4%	
19			136	2	0.00	0.34	0.01	0.00	0.21	0.22	62.6%	4.1%	0.00	0.15	0.01	0.00	0.08	0.10	43.8%	43.8%	43.8%	43.8%	43.8%	43.8%	43.8%	43.8%	
20			137	2	0.01	0.48	0.01	0.00	0.28	0.35	57.6%	1.0%	0.00	0.23	0.00	0.00	0.14	0.16	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	46.5%	
21			138	2	0.00	0.54	0.00	0.01	0.32	0.37	59.2%	0.7%	0.00	0.21	0.00	0.01	0.15	0.15	38.6%	38.6%	38.6%	38.6%	38.6%	38.6%	38.6%	38.6%	
22			141	2	0.01	0.43	0.01	0.01	0.25	0.32	57.2%	1.4%	0.01	0.21	0.00	0.00	0.12	0.15	47.7%	47.7%	47.7%	47.7%	47.7%	47.7%	47.7%	47.7%	
23			142	2	0.00	0.55	0.00	0.01	0.32	0.37	58.5%	0.7%	0.00	0.22	0.00	0.01	0.16	0.15	40.1%	40.1%	40.1%	40.1%	40.1%	40.1%	40.1%	40.1%	
24			148	5	0.01	0.62	0.04	0.00	0.39	0.41	63.0%	6.8%	0.01	0.24	0.03	0.00	0.16	0.20	39.3%	39.3%	39.3%	39.3%	39.3%	39.3%	39.3%	39.3%	
25			149	5	0.01	0.78	0.01	0.01	0.41	0.56	52.4%	1.7%	0.01	0.42	0.01	0.01	0.23	0.28	54.0%	54.0%	54.0%	54.0%	54.0%	54.0%	54.0%	54.0%	
26			150	5	0.02	0.95	0.01	0.01	0.51	0.67	54.2%	1.3%	0.01	0.48	0.01	0.00	0.28	0.38	50.5%	50.5%	50.5%	50.5%	50.5%	50.5%	50.5%	50.5%	
27			151	5	0.01	0.91	0.02	0.01	0.49	0.63	53.9%	1.7%	0.01	0.45	0.01	0.01	0.28	0.29	49.9%	49.9%	49.9%	49.9%	49.9%	49.9%	49.9%	49.9%	
28			152	5	0.01	0.97	0.02	0.01	0.55	0.66	57.0%	1.7%	0.01	0.35	0.01	0.01	0.27	0.24	36.2%	36.2%	36.2%	36.2%	36.2%	36.2%	36.2%	36.2%	
29			157	5	0.01	0.76	0.03	0.01	0.40	0.50	53.0%	3.5%	0.01	0.38	0.01	0.00	0.20	0.25	49.4%	49.4%	49.4%	49.4%	49.4%	49.4%	49.4%	49.4%	
30			158	5	0.01	0.84	0.01	0.00	0.46	0.64	50.8%	1.7%	0.01	0.44	0.01	0.00	0.23	0.34	52.6%	52.6%	52.6%	52.6%	52.6%	52.6%	52.6%	52.6%	
31			159	5	0.02	0.94	0.02	0.01	0.58	0.62	61.4%	1.7%	0.01	0.48	0.01	0.01	0.34	0.31	50.5%	50.5%	50.5%	50.5%	50.5%	50.5%	50.5%	50.5%	
32			160	5	0.01	0.99	0.02	0.01	0.56	0.68	56.2%	1.5%	0.01	0.45	0.01	0.01	0.30	0.28	45.5%	45.5%	45.5%	45.5%	45.5%	45.5%	45.5%	45.5%	
33			3 131	2	0.00	0.49	0.01	0.01	0.12	0.42	25.4%	2.7%	0.00	0.17	0.01	0.01	0.05	0.18	36.7%	36.7%	36.7%	36.7%	36.7%	36.7%	36.7%	36.7%	
34			4 132	2	0.00	0.49	0.03	0.00	0.12	0.44	24.2%	5.3%	0.00	0.19	0.02	0.00	0.05	0.20	40.8%	40.8%	40.8%	40.8%	40.8%	40.8%	40.8%	40.8%	
35			9 136	4	0.00	1.11	0.05	0.00	0.28	1.26	29.6%	4.7%	0.00	0.45	0.04	0.00	0.14	0.48	43.4%	43.4%	43.4%	43.4%	43.4%	43.4%	43.4%	43.4%	
36			9 137	4	0.01	1.03	0.01	0.02	0.38	0.94	36.8%	1.3%	0.01	0.45	0.01	0.01	0.18	0.45	43.9%	43.9%	43.9%	43.9%	43.9%	43.9%	43.9%	43.9%	
37			10 138	4	0.01	0.98	0.01	0.02	0.47	0.73	47.8%	1.1%	0.01	0.40	0.01	0.02	0.23	0.37	40.1%	40.1%	40.1%	40.1%	40.1%	40.1%	40.1%	40.1%	
38			13 141	4	0.01	1.02	0.02	0.01	0.35	0.88	34.6%	2.1%	0.01	0.49	0.02	0.01	0.15	0.44	48.0%	48.0%	48.0%	48.0%	48.0%	48.0%	48.0%	48.0%	
39			14 142	4	0.01	1.09	0.02	0.04	0.38	1.01	35.1%	1.8%	0.01	0.39	0.02	0.03	0.19	0.44	40.4%	40.4%	40.4%	40.4%	40.4%	40.4%	40.4%	40.4%	
40			20 148	10	0.01	1.96	0.17	0.02	0.58	1.86	29.7%	8.8%	0.01	0.83	0.12	0.02	0.28	1.00	51.2%	51.2%	51.2%	51.2%	51.2%	51.2%	51.2%	51.2%	
41			21 149	10	0.02	2.24	0.06	0.01					0.02	1.11	0.04	0.01	0.31	1.10	49.4%	49.4%	49.4%	49.4%	49.4%	49.4%	49.4%	49.4%	
42	22 150	10	0.03	2.51	0.03	0.01	0.71	2.32	28.4%	1.1%	0.02	1.27	0.02	0.01	0.37	1.23	50.7%	50.7%	50.7%	50.7%	50.7%	50.7%	50.7%	50.7%			
43	23 151	10	0.02	2.52	0.05	0.02	0.76	2.38	30.1%	2.0%	0.02	1.11	0.04	0.01	0.39	1.15	45.7%	45.7%	45.7%	45.7%	45.7%	45.7%	45.7%	45.7%			
44	24 152	10	0.04	2.25	0.05	0.08	0.77	1.95	34.3%	2.1%	0.03	0.71	0.03	0.06	0.38	0.84	37.3%	37.3%	37.3%	37.3%	37.3%	37.3%	37.3%	37.3%			
45	29 157	10	0.02	2.11	0.08	0.02	0.64	2.07	30.4%	3.8%	0.02	1.06	0.04	0.02	0.33	1.08	51.4%	51.4%	51.4%	51.4%	51.4%	51.4%	51.4%	51.4%			
46	30 158	20	0.02	2.01	0.09	0.03	0.89	2.21	25.8%	3.3%	0.02	1.04	0.06	0.02	0.34	1.14	48.7%	48.7%	48.7%	48.7%	48.7%	48.7%	48.7%	48.7%			
47	31 159	10	0.03	2.38	0.03	0.03	0.88	2.11	36.7%	1.2%	0.02	1.21	0.02	0.02	0.47	1.12	53.0%	53.0%	53.0%	53.0%	53.0%	53.0%	53.0%	53.0%			
48	32 160	10	0.03	2.52	0.07	0.03	0.80	2.38	21.5%	2.7%	0.02	1.06	0.05	0.02	0.41	1.02	41.9%	41.9%	41.9%	41.9%	41.9%	41.9%	41.9%	41.9%			

- K-patch High CH

													max ratio out of all beams																	max ratio out of all beams			
No.	Module	Type	Beam ID_1	Bema ID_2	Feed no.	4cm2 PD(mW/cm2)						68.5%		9.9%		4cm2 PD(mW/cm2) at 10mm evaluation distance						54.3%		54.3%		53.7%							
						S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Font 2mm)/(worst-surface 2mm)	ratio (Top 2mm)/(worst-surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (back 10mm)/(worst-surface 2mm)	ratio (Left 10mm)/(worst-surface 2mm)											
1	K	Patch	3		1	0.00	0.16	0.00	0.00	0.01	0.16	4.3%	2.5%	0.00	0.05	0.00	0.00	0.00	0.00	0.06	37.7%	37.7%	33.3%										
2			4		1	0.00	0.30	0.01	0.00	0.01	0.28	4.7%	3.1%	0.00	0.11	0.01	0.00	0.01	0.13	44.7%	44.7%	35.6%											
3			8		2	0.00	0.64	0.02	0.00	0.05	0.58	8.5%	3.6%	0.00	0.26	0.02	0.00	0.02	0.29	45.3%	45.3%	41.0%											
4			9		2	0.00	0.37	0.00	0.00	0.03	0.43	7.5%	0.7%	0.00	0.15	0.00	0.00	0.02	0.21	49.3%	49.3%	34.5%											
5			10		2	0.00	0.44	0.01	0.01	0.10	0.41	23.5%	1.6%	0.00	0.17	0.01	0.00	0.05	0.19	43.4%	43.4%	39.7%											
6			13		2	0.00	0.38	0.01	0.00	0.03	0.43	6.9%	1.2%	0.00	0.16	0.00	0.00	0.01	0.21	50.5%	50.5%	39.9%											
7			14		0.00	0.34	0.01	0.01	0.04	0.39	8.9%	2.8%	0.00	0.13	0.01	0.01	0.02	0.18	45.9%	45.9%	32.1%												
8			20		5	0.01	1.13	0.09	0.01	0.11	1.09	9.4%	8.3%	0.01	0.54	0.06	0.01	0.05	0.58	51.0%	51.0%	47.7%											
9			21		5	0.01	1.23	0.04	0.00	0.11	1.19	9.1%	2.9%	0.01	0.56	0.03	0.00	0.05	0.61	49.8%	49.8%	45.1%											
10			22		5	0.01	1.25	0.01	0.00	0.16	1.24	12.5%	0.5%	0.01	0.60	0.00	0.00	0.08	0.67	53.5%	53.5%	47.9%											
11			23		5	0.01	1.20	0.01	0.00	0.13	1.23	10.9%	1.0%	0.01	0.54	0.01	0.00	0.06	0.63	51.3%	51.3%	44.3%											
12			24		5	0.01	0.82	0.02	0.03	0.09	0.85	10.3%	2.2%	0.01	0.30	0.01	0.02	0.04	0.35	40.5%	40.5%	35.3%											
13			29		5	0.01	1.26	0.05	0.01	0.11	1.20	8.8%	4.2%	0.01	0.60	0.03	0.00	0.05	0.63	49.7%	49.7%	47.5%											
14			30		5	0.01	1.17	0.03	0.00	0.15	1.17	12.4%	2.7%	0.01	0.52	0.02	0.00	0.07	0.59	50.6%	50.6%	44.6%											
15			31		5	0.01	1.20	0.01	0.00	0.16	1.19	13.5%	0.8%	0.01	0.57	0.01	0.00	0.08	0.65	54.3%	54.3%	47.1%											
16			32		5	0.01	1.07	0.02	0.01	0.11	1.13	9.9%	1.8%	0.01	0.45	0.02	0.01	0.05	0.53	46.8%	46.8%	39.9%											
17			131		1	0.00	0.17	0.00	0.00	0.09	0.11	56.0%	1.2%	0.00	0.06	0.00	0.00	0.04	0.05	36.3%	36.3%	36.3%											
18			132		1	0.00	0.15	0.01	0.00	0.09	0.11	59.9%	3.3%	0.00	0.06	0.00	0.00	0.04	0.05	37.5%	37.5%	37.5%											
19			136		2	0.00	0.29	0.01	0.00	0.19	0.19	64.5%	4.4%	0.00	0.12	0.01	0.00	0.08	0.08	41.6%	41.6%	41.6%											
20			137		2	0.01	0.45	0.00	0.00	0.23	0.33	52.0%	0.9%	0.00	0.21	0.00	0.00	0.11	0.14	47.8%	47.8%	42.1%											
21			138		2	0.00	0.50	0.00	0.01	0.28	0.34	55.8%	0.6%	0.00	0.21	0.00	0.00	0.14	0.13	42.2%	42.2%	42.2%											
22			141		2	0.01	0.40	0.01	0.00	0.20	0.29	51.5%	1.3%	0.01	0.19	0.00	0.00	0.10	0.13	48.0%	48.0%	48.0%											
23			142		2	0.00	0.50	0.00	0.01	0.28	0.35	55.0%	0.6%	0.00	0.22	0.00	0.00	0.13	0.14	43.5%	43.5%	43.5%											
24			148		5	0.01	0.55	0.05	0.00	0.38	0.39	68.5%	8.7%	0.00	0.21	0.03	0.00	0.17	0.21	37.8%	37.8%	37.8%											
25			149		5	0.01	0.61	0.02	0.00	0.28	0.47	46.2%	2.5%	0.01	0.32	0.01	0.00	0.15	0.21	51.6%	51.6%	51.6%											
26			150		5	0.01	0.88	0.01	0.00	0.42	0.66	48.2%	1.4%	0.01	0.47	0.01	0.00	0.25	0.34	53.2%	53.2%	53.2%											
27			151		5	0.01	0.73	0.01	0.00	0.36	0.53	49.6%	1.4%	0.01	0.37	0.01	0.00	0.18	0.26	50.1%	50.1%	50.1%											
28			152		5	0.01	0.84	0.02	0.01	0.45	0.61	53.0%	1.9%	0.01	0.34	0.01	0.01	0.23	0.24	40.8%	40.8%	40.8%											
29			157		5	0.01	0.61	0.03	0.00	0.34	0.40	56.7%	5.1%	0.01	0.26	0.02	0.00	0.16	0.20	43.6%	43.6%	43.6%											
30			158		5	0.01	0.74	0.01	0.01	0.31	0.59	41.3%	1.4%	0.01	0.39	0.01	0.01	0.17	0.30	53.2%	53.2%	53.2%											
31			159		5	0.02	0.86	0.01	0.00	0.47	0.62	54.6%	1.6%	0.02	0.46	0.01	0.00	0.24	0.30	53.7%	53.7%	53.7%											
32			160		5	0.01	0.76	0.01	0.01	0.41	0.55	54.7%	1.5%	0.01	0.35	0.01	0.01	0.21	0.24	46.6%	46.6%	46.6%											
33			3 131		2	0.00	0.41	0.01	0.01	0.11	0.35	26.8%	2.7%	0.00	0.15	0.01	0.01	0.05	0.14	36.3%	35.0%	36.3%											
34			4 132		2	0.00	0.49	0.02	0.00	0.13	0.45	26.9%	4.5%	0.00	0.19	0.02	0.00	0.06	0.20	41.4%	41.4%	38.2%											
35			6 136		2	0.00	0.45	0.06	0.00	0.21	0.38	31.8%	4.5%	0.00	0.18	0.01	0.00	0.08	0.11	43.2%	43.2%	40.9%											
36			9 137		4	0.01	0.90	0.01	0.01	0.38	0.81	41.8%	1.0%	0.01	0.43	0.01	0.01	0.17	0.38	48.0%	48.0%	48.0%											
37			10 138		4	0.01	0.99	0.01	0.02	0.37	0.71	37.6%	1.3%	0.01	0.42	0.01	0.01	0.18	0.33	42.0%	42.0%	42.0%											
38			13 141		4	0.01	0.90	0.01	0.01	0.33	0.78	36.6%	1.4%	0.01	0.43	0.01	0.01	0.14	0.38	47.2%	47.2%	47.2%											
39			14 142		4	0.01	0.94	0.02	0.03	0.40	0.88	42.9%	2.0%	0.01	0.38	0.02	0.02	0.19	0.37	40.8%	38.7%	40.8%											
40			20 148		10	0.02	1.49	0.19	0.01	0.59	1.41	29.7%	9.9%	0.02	0.94	0.01	0.01	0.29	0.49	46.8%	46.8%	46.8%											
41			21 149		10	0.02	2.03	0.06	0.01	0.43	1.91	20.9%	2.9%	0.02	0.99	0.04	0.01	0.28	0.91	48.6%	48.6%	48.6%											
42			22 150		10	0.03	2.36	0.02	0.01	0.74	2.15	31.2%	0.9%	0.02	1.25	0.02	0.01	0.40	1.12	52.9%	47.5%	52.9%											
43			23 151		10	0.02	2.18	0.03	0.01	0.68	2.23	30.4%	1.4%	0.02	1.02	0.02	0.01	0.33	1.12	50.0%	50.0%	45.6%											
44			24 152		10	0.03	2.07	0.06	0.07	0.67	1.90	32.4%	2.9%	0.03	0.69	0.04	0.05	0.32	0.74	35.8%	35.8%	33.4%											
45			29 157		10	0.02	1.96	0.09	0.01	0.49	1.79	25.1%	4.7%	0.02	0.99	0.05	0.01	0.29	0.86	50.5%	44.2%	50.5%											
46			30 158		10	0.02	2.27	0.05	0.01	0.50	2.12	22.1%	2.1%	0.02	1.08	0.03	0.01	0.28	1.03	47.8%	45.5%	47.8%											
47			31 159		10	0.04	2.17	0.04	0.01	0.88	1.97	40.4%	1.7%	0.03	1.11	0.03	0.01	0.43	1.03	51.0%	47.4%	51.0%											
48	32 160		10	0.03	2.14	0.05	0.02	0.66	2.19	30.0%	2.3%	0.02	0.92	0.04	0.01	0.31	0.98	44.6%	44.6%	42.1%													

- K-patch Mid CH

						max ratio out of all beams										max ratio out of all beams											
						4cm2 PD(mW/cm2)					per Beam Back-off (dB)		69.4%		13.4%		4cm2 PD(mW/cm2) at 10mm evaluation distance					57.8%		50.6%		57.8%	
No.	Module	Type	Beam ID_1	Bema ID_2	Feed no.	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Front 2mm)/(worst surface 2mm)*(per Beam Back-off (dB))	ratio (Top 2mm)/(worst surface 2mm)*(per Beam Back-off (dB))	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio worst-surface 10mm/2mm*(per Beam Back-off (dB))	ratio (back 10mm)/(worst-surface 2mm)*(per Beam Back-off (dB))	ratio (left 10mm)/(worst-surface 2mm)*(per Beam Back-off (dB))					
1	4	1	0.00	0.13	0.00	0.00	0.05	0.07				38.6%	3.0%	0.00	0.05	0.00	0.00	0.02	0.02	35.6%	17.4%	35.6%					
2	5	1	0.00	0.09	0.00	0.00	0.09	0.05	1.24			69.4%	2.5%	0.00	0.04	0.00	0.00	0.04	0.01	31.9%	15.0%	30.2%					
3	6	1	0.00	0.12	0.00	0.00	0.05	0.07				40.5%	2.8%	0.00	0.05	0.00	0.00	0.02	0.03	43.1%	25.0%	43.1%					
4	7	1	0.00	0.10	0.01	0.00	0.06	0.06				55.4%	5.0%	0.00	0.04	0.00	0.00	0.02	0.02	39.6%	18.8%	39.6%					
5	8	1	0.00	0.18	0.01	0.01	0.18	0.10	0.49			68.0%	6.0%	0.00	0.05	0.00	0.00	0.00	0.01	44.3%	23.3%	43.1%					
6	12	2	0.01	0.16	0.00	0.00	0.18	0.12				51.9%	1.9%	0.00	0.07	0.00	0.00	0.03	0.06	45.0%	34.4%	45.0%					
7	13	2	0.00	0.28	0.01	0.00	0.09	0.14				31.7%	2.2%	0.00	0.08	0.01	0.00	0.03	0.05	28.1%	18.7%	28.1%					
8	16	2	0.00	0.26	0.01	0.00	0.09	0.13				34.0%	2.3%	0.00	0.08	0.01	0.00	0.03	0.05	29.3%	18.5%	29.3%					
9	17	2	0.00	0.24	0.00	0.00	0.07	0.16				36.5%	2.7%	0.00	0.08	0.01	0.00	0.03	0.05	30.1%	19.1%	30.1%					
10	23	5	0.01	0.48	0.03	0.00	0.30	0.26				62.2%	6.4%	0.01	0.16	0.02	0.00	0.14	0.11	32.4%	22.5%	32.4%					
11	24	5	0.00	0.32	0.01	0.00	0.18	0.21				55.3%	4.1%	0.00	0.15	0.01	0.00	0.08	0.08	46.2%	25.5%	46.2%					
12	25	5	0.01	0.55	0.02	0.00	0.26	0.35				47.1%	4.2%	0.01	0.30	0.02	0.00	0.12	0.18	54.2%	30.2%	54.2%					
13	26	5	0.01	0.46	0.01	0.01	0.21	0.25				42.9%	3.9%	0.01	0.28	0.01	0.00	0.10	0.13	41.1%	29.6%	41.1%					
14	27	5	0.01	0.57	0.03	0.01	0.25	0.31				43.4%	5.6%	0.01	0.16	0.02	0.01	0.12	0.18	28.5%	23.0%	28.5%					
15	32	5	0.01	0.33	0.02	0.01	0.19	0.25	0.18			53.9%	4.3%	0.01	0.10	0.01	0.01	0.11	0.11	32.3%	32.3%	27.9%					
16	33	5	0.01	0.52	0.01	0.00	0.23	0.30				44.9%	1.5%	0.01	0.30	0.01	0.00	0.11	0.15	57.8%	28.2%	57.8%					
17	34	5	0.01	0.40	0.01	0.00	0.21	0.25				52.0%	1.0%	0.01	0.19	0.01	0.00	0.10	0.09	47.0%	23.5%	47.0%					
18	35	5	0.01	0.58	0.03	0.01	0.24	0.32				42.3%	5.2%	0.01	0.17	0.02	0.01	0.11	0.15	30.1%	25.6%	30.1%					
19	132	1	0.00	0.19	0.01	0.00	0.07	0.16				38.0%	2.7%	0.00	0.07	0.00	0.00	0.03	0.06	36.9%	33.2%	36.9%					
20	133	1	0.00	0.28	0.01	0.00	0.07	0.21				24.1%	2.5%	0.00	0.11	0.01	0.00	0.02	0.09	37.9%	32.3%	37.9%					
21	134	1	0.00	0.19	0.01	0.00	0.05	0.15				27.0%	0.0%	0.00	0.08	0.01	0.00	0.05	0.06	40.2%	36.9%	40.2%					
22	135	1	0.00	0.13	0.00	0.00	0.05	0.11				34.6%	2.3%	0.00	0.06	0.00	0.00	0.02	0.04	46.6%	32.3%	46.6%					
23	139	2	0.00	0.35	0.02	0.00	0.12	0.27				34.8%	4.2%	0.00	0.11	0.01	0.00	0.04	0.09	30.6%	26.3%	30.6%					
24	140	2	0.00	0.47	0.01	0.00	0.15	0.37				31.7%	1.9%	0.00	0.24	0.01	0.00	0.05	0.20	51.7%	42.1%	51.7%					
25	141	2	0.00	0.42	0.01	0.00	0.11	0.34				26.2%	1.1%	0.00	0.12	0.01	0.00	0.05	0.14	31.3%	26.3%	31.3%					
26	144	2	0.00	0.49	0.02	0.00	0.14	0.42				27.5%	3.5%	0.00	0.23	0.01	0.00	0.05	0.20	46.6%	40.2%	46.6%					
27	145	2	0.00	0.45	0.01	0.00	0.14	0.34				31.6%	2.0%	0.00	0.16	0.01	0.00	0.06	0.16	36.3%	36.3%	35.2%					
28	151	5	0.01	0.74	0.08	0.01	0.18	0.56				24.2%	10.8%	0.01	0.30	0.06	0.01	0.07	0.26	40.4%	35.5%	40.4%					
29	152	5	0.01	0.62	0.02	0.00	0.20	0.40				21.8%	0.0%	0.00	0.21	0.01	0.00	0.10	0.44	44.2%	33.2%	44.2%					
30	153	5	0.01	0.96	0.01	0.00	0.29	0.79				30.4%	4.4%	0.01	0.46	0.01	0.00	0.12	0.39	47.3%	40.6%	47.3%					
31	154	5	0.01	0.86	0.02	0.01	0.30	0.65				25.2%	2.2%	0.01	0.37	0.01	0.00	0.13	0.34	43.4%	39.4%	43.4%					
32	155	5	0.01	0.62	0.08	0.01	0.21	0.60				34.0%	13.4%	0.01	0.23	0.06	0.01	0.09	0.30	48.2%	48.2%	47.4%					
33	160	10	0.00	0.70	0.08	0.01	0.24	0.63				26.5%	0.6%	0.00	0.43	0.02	0.00	0.15	0.48	50.6%	46.8%	50.6%					
34	161	5	0.01	1.01	0.02	0.00	0.30	0.83				29.4%	1.5%	0.01	0.57	0.01	0.00	0.14	0.45	56.5%	44.7%	56.5%					
35	162	5	0.01	0.97	0.01	0.01	0.32	0.77				33.3%	1.5%	0.01	0.41	0.01	0.01	0.13	0.38	42.7%	39.2%	42.7%					
36	163	5	0.01	0.74	0.08	0.01	0.17	0.56				22.8%	10.3%	0.01	0.28	0.05	0.01	0.07	0.25	38.3%	34.1%	38.3%					
37	145	2	0.00	0.46	0.01	0.00	0.13	0.36				28.0%	0.0%	0.00	0.28	0.01	0.00	0.11	0.15	37.7%	26.3%	37.7%					
38	5	132	2	0.00	0.57	0.02	0.00	0.19	0.36			33.8%	2.6%	0.00	0.23	0.01	0.00	0.09	0.13	40.4%	23.3%	40.4%					
39	6	134	2	0.00	0.41	0.02	0.00	0.13	0.26			32.7%	4.2%	0.00	0.18	0.01	0.00	0.06	0.12	43.7%	28.5%	43.7%					
40	7	135	2	0.00	0.34	0.01	0.00	0.14	0.24			41.6%	3.2%	0.00	0.16	0.01	0.00	0.07	0.09	46.6%	27.3%	46.6%					
41	119	10	0.00	0.70	0.01	0.00	0.24	0.63				47.3%	4.3%	0.01	0.27	0.01	0.00	0.11	0.13	31.0%	25.3%	31.0%					
42	12	140	4	0.01	0.72	0.00	0.00	0.26	0.57			35.7%	2.9%	0.01	0.39	0.01	0.00	0.10	0.13	50.0%	41.4%	55.0%					
43	13	141	4	0.01	1.00	0.03	0.01	0.28	0.60			27.8%	2.6%	0.01	0.33	0.02	0.01	0.11	0.23	32.4%	22.9%	32.4%					
44	16	144	4	0.01	0.88	0.04	0.02	0.25	0.63			28.8%	4.1%	0.01	0.40	0.03	0.01	0.09	0.31	45.7%	34.9%	45.7%					
45	17	145	4	0.01	0.83	0.07	0.01	0.27	0.61			27.3%	3.0%	0.01	0.36	0.02	0.01	0.11	0.11	38.1%	33.3%	38.1%					
46	23	151	10	0.03	1.77	0.18	0.02	0.69	1.11			38.9%	10.4%	0.02	0.73	0.13	0.01	0.28	0.54	41.2%	30.4%	41.2%					
47	24	152	10	0.03	1.68	0.03	0.01	0.49	1.22			29.3%	1.8%	0.01	0.93	0.02	0.01	0.28	0.62	55.6%	37.2%	55.6%					
48	25	153	10	0.02	2.10	0.07	0.01	0.62	1.50			29.6%	3.1%	0.02	1.12	0.05	0.01	0.28	0.81	53.1%	38.6%	53.1%					
49	26	154	10	0.02	1.85	0.04	0.01	0.58	1.29			29.2%	3.2%	0.02	1.04	0.03	0.01	0.32	0.72	46.7%	36.8%	46.7%					
50	27	155	10	0.02	1.82	0.19	0.03	0.71	1.18			39.2%	10.5%	0.02	0.67	0.14	0.03	0.32	0.58	37.1%	32.0%	37.1%					
51	32	160	10	0.02	1.35	0.10	0.02	0.51	0.88			37.6%	7.6%	0.02	0.51	0.06	0.02	0.23	0.51	37.1%	37.5%	37.8%					
52	33	161	10	0.02	2.15	0.03	0.01	0.57	1.54			26.3%	1.3%	0.01	1.24	0.02	0.01	0.30	0.85	57.9%	39.3%	57.9%					
53	34	162	10	0.03	2.08	0.04	0.02	0.64	1.38			27.1%	1.1%	0.02	1.16	0.03	0.01	0.47	0.77	47.1%	36.2%	47.1%					
54	35	163	10	0.03	2.02	0.18	0.02	0.60	1.25			29.6%	8.7%	0.02	0.82	0.13	0.02	0.26	0.57	40.7%	28.3%	40.7%					

Table 4 & Table 5 show the PD simulation evaluation of Ant L patch antenna at 28GHz / 39GHz for the corresponding evaluation plane specified in Table 1.

Table 5. PD of Ant L – patch antenna (28GHz – n261)

- L-patch Low CH

						max ratio out of all beams										max ratio out of all beams									
No.	Module	Type	Beam ID_1	Berna ID_2	Feed no.	4cm2 PD(mW/cm2)						77.9%		6.0%		4cm2 PD(mW/cm2) at 10mm evaluation distance						58.4%		58.4%	
												ratio (Font 2mm)/(worst- surface 2mm)	ratio (Bottom 2mm)/(worst- surface 2mm)							ratio worst-surface (10mm/2mm)	ratio (back 10mm)/(worst- surface 2mm)				
						S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)			S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)						
49			0	1	2	0.20	0.00	0.00	0.00	0.01	0.23	3.4%	0.00	0.00	0.00	0.00	0.10	41.6%	41.6%						
50			1	1	1	0.31	0.00	0.00	0.00	0.01	0.32	4.4%	1.6%	0.12	0.00	0.00	0.00	0.01	0.14	43.4%	43.4%				
51			2	1	1	0.32	0.00	0.00	0.00	0.01	0.01	0.32	4.3%	2.8%	0.11	0.00	0.00	0.00	0.01	0.13	39.8%	39.8%			
52			5	2	0.79	0.00	0.00	0.02	0.05	0.07	5.9%	1.9%	0.34	0.00	0.00	0.01	0.02	0.38	48.5%	48.5%					
53			6	4	0.48	0.01	0.00	0.00	0.01	0.02	0.55	4.2%	0.20	0.00	0.00	0.01	0.01	0.37	49.8%	49.8%					
54			7	5	0.58	0.00	0.01	0.02	0.04	0.04	0.62	5.8%	2.6%	0.24	0.00	0.01	0.01	0.01	0.28	44.8%	44.8%				
55			11	2	0.48	0.00	0.00	0.00	0.00	0.02	0.53	4.4%	0.8%	0.21	0.00	0.00	0.00	0.01	0.27	50.4%	50.4%				
56			12	2	0.43	0.01	0.01	0.02	0.02	0.02	0.53	3.4%	2.9%	0.18	0.00	0.01	0.01	0.01	0.24	46.4%	46.4%				
57			15	3	1.53	0.02	0.01	0.05	0.15	1.53	18.2%	0.00	0.75	0.03	0.00	0.04	0.04	0.92	53.9%	53.9%					
58			16	5	1.68	0.02	0.00	0.01	0.11	1.68	6.5%	0.5%	0.82	0.02	0.00	0.01	0.05	0.93	55.5%	55.5%					
59			17	5	1.67	0.02	0.00	0.02	0.10	1.68	6.1%	1.1%	0.85	0.02	0.00	0.02	0.05	0.98	54.8%	54.8%					
60			18	5	1.64	0.02	0.00	0.00	0.11	1.75	6.1%	0.7%	0.80	0.02	0.00	0.01	0.05	0.95	54.6%	54.6%					
61			19	138	0.02	0.02	0.01	0.12	1.60	6.4%	0.00	0.61	0.02	0.01	0.01	0.05	0.91	48.1%	48.1%						
62			25	5	1.63	0.02	0.00	0.02	0.12	1.62	7.3%	1.1%	0.80	0.02	0.00	0.01	0.06	0.91	55.4%	55.4%					
63			26	5	1.72	0.02	0.00	0.02	0.11	1.71	6.4%	1.0%	0.87	0.01	0.00	0.01	0.05	0.99	57.5%	57.5%					
64			27	5	1.66	0.02	0.01	0.01	0.10	1.71	6.0%	0.5%	0.82	0.02	0.00	0.01	0.05	0.97	56.9%	56.9%					
65			38	10	5	1.71	0.01	0.02	0.12	0.72	6.8%	0.9%	0.71	0.02	0.00	0.01	0.05	0.67	50.8%	50.8%					
66			128	1	0.25	0.00	0.00	0.00	0.17	0.18	69.2%	1.2%	0.11	0.00	0.00	0.00	0.07	0.08	42.9%	33.6%					
67			129	1	0.23	0.00	0.00	0.01	0.15	0.18	68.4%	2.7%	0.09	0.00	0.00	0.00	0.06	0.07	39.6%	32.4%					
68			130	1	0.23	0.00	0.00	0.00	0.16	0.17	69.0%	0.9%	0.11	0.00	0.00	0.00	0.06	0.08	46.5%	36.3%					
69			133	2	0.48	0.00	0.00	0.01	0.30	0.36	61.9%	2.5%	0.21	0.00	0.00	0.01	0.13	0.17	35.8%	35.8%					
70			134	2	0.47	0.00	0.00	0.01	0.31	0.36	65.8%	1.7%	0.20	0.00	0.00	0.01	0.14	0.17	43.3%	35.2%					
71			135	2	0.30	0.00	0.00	0.01	0.23	0.23	77.9%	1.7%	0.13	0.00	0.00	0.00	0.09	0.11	43.3%	36.6%					
72			139	2	0.38	0.00	0.00	0.01	0.27	0.28	71.6%	2.9%	0.15	0.00	0.00	0.01	0.12	0.12	39.0%	32.6%					
73			140	2	0.70	0.01	0.00	0.00	0.41	0.55	58.2%	0.3%	0.34	0.01	0.00	0.00	0.21	0.26	48.3%	36.4%					
74			143	10	1.01	0.01	0.04	0.74	0.84	70.2%	0.9%	0.46	0.01	0.00	0.00	0.04	0.24	0.44	43.2%	36.4%					
75			145	5	1.28	0.02	0.00	0.01	0.83	0.99	65.1%	0.7%	0.68	0.02	0.00	0.01	0.49	0.57	53.3%	42.9%					
76			146	5	1.33	0.02	0.00	0.01	0.77	1.06	57.8%	0.4%	0.71	0.01	0.00	0.00	0.47	0.63	57.0%	47.6%					
77			145	5	1.31	0.02	0.00	0.02	0.92	1.04	70.4%	1.1%	0.70	0.02	0.00	0.01	0.53	0.61	53.3%	46.2%					
78			147	5	1.16	0.02	0.01	0.02	0.87	0.87	75.1%	1.3%	0.51	0.02	0.00	0.00	0.47	0.50	49.3%	47.6%					
79			153	5	1.23	0.02	0.00	0.03	0.86	0.97	70.1%	2.6%	0.58	0.02	0.00	0.02	0.49	0.53	47.5%	43.3%					
80			154	5	1.25	0.02	0.00	0.00	0.75	0.99	60.1%	0.3%	0.70	0.02	0.00	0.00	0.46	0.58	56.3%	46.3%					
81			155	5	1.47	0.02	0.00	0.01	0.93	1.17	63.4%	0.5%	0.81	0.02	0.00	0.01	0.56	0.70	55.5%	47.4%					
82			156	5	1.21	0.02	0.01	0.01	0.81	0.96	61.9%	0.9%	0.61	0.02	0.00	0.01	0.50	0.56	51.9%	44.9%					
83			0	128	2	0.55	0.00	0.01	0.01	0.20	0.46	41.9%	1.0%	0.18	0.00	0.01	0.00	0.10	0.19	38.8%	38.8%				
84			1	129	2	0.55	0.00	0.01	0.01	0.17	0.50	30.8%	2.2%	0.22	0.00	0.01	0.01	0.07	0.21	40.7%	39.0%				
85			2	130	2	0.55	0.00	0.00	0.02	0.19	0.51	34.8%	3.3%	0.22	0.00	0.00	0.01	0.07	0.22	40.7%	38.6%				
86			5	133	4	1.03	0.01	0.01	0.37	1.23	29.8%	2.3%	0.17	0.01	0.00	0.01	0.17	0.23	46.6%	46.6%					
87			6	134	4	1.02	0.01	0.01	0.01	0.37	0.99	36.5%	1.4%	0.47	0.01	0.00	0.01	0.18	0.49	47.5%	47.5%				
88			7	135	4	1.07	0.01	0.02	0.04	0.33	1.08	30.2%	3.4%	0.44	0.01	0.02	0.03	0.13	0.46	42.5%	42.5%				
89			11	139	4	0.96	0.01	0.01	0.02	0.36	0.92	39.5%	1.7%	0.41	0.01	0.01	0.01	0.17	0.45	49.4%	49.4%				
90			12	140	4	1.20	0.01	0.01	0.03	0.45	1.16	34.1%	2.1%	0.43	0.01	0.01	0.01	0.43	0.56	46.3%	46.3%				
91			15	143	10	2.86	0.03	0.01	0.14	0.96	2.50	33.5%	4.9%	1.29	0.02	0.01	0.10	0.55	1.39	48.4%	48.4%				
92			16	144	10	2.92	0.03	0.00	0.01	0.96	2.76	33.0%	0.5%	1.55	0.03	0.00	0.01	0.56	1.50	53.0%	53.0%				
93			17	145	10	2.97	0.02	0.00	0.03	0.92	2.74	31.0%	0.9%	1.67	0.02	0.00	0.02	0.54	1.58	56.2%	51.2%				
94			18	146	10	2.97	0.03	0.01	0.04	1.07	3.21	31.7%	1.1%	1.72	0.02	0.01	0.04	0.07	1.21	54.7%	54.6%				
95			19	147	10	2.96	0.03	0.03	0.04	1.10	3.02	36.4%	1.4%	1.47	0.03	0.02	0.03	0.60	1.56	51.7%	51.7%				
96			25	153	10	2.95	0.03	0.00	0.04	0.95	2.74	32.0%	1.5%	1.40	0.02	0.00	0.03	0.56	1.53	52.0%	52.0%				
97			26	154	10	2.90	0.03	0.00	0.02	0.91	2.74	31.4%	0.7%	1.61	0.02	0.00	0.02	0.54	1.54	53.0%	53.0%				
98			27	155	10	3.01	0.03	0.01	0.07	1.13	3.14	34.4%	1.8%	1.68	0.03	0.01	0.04	0.71	1.59	55.2%	54.2%				
99			28	156	10	3.13	0.03	0.02	0.06	1.10	3.18	34.6%	1.8%	1.62	0.02	0.02	0.04	0.62	1.60	53.3%	53.3%				

- L-patch Mid CH

						max ratio out of all beams												max ratio out of all beams			
						4cm2 PD(mW/cm2)				65.6%		6.3%		4cm2 PD(mW/cm2) at 10mm evaluation distance				58.6%		58.6%	
No.	Module	Type	Beam ID_1	Bema ID_2	Feed no.	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Fomt 2mm)/(worst-surface 2mm)	ratio (Bottom 2mm)/(worst-surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (back 10mm)/(worst-surface 2mm)
49	L	Patch	0	1	0.19	0.00	0.00	0.00	0.00	0.01	0.22	4.7%	0.9%	0.06	0.00	0.00	0.00	0.01	0.09	41.9%	41.9%
50			1	0.31	0.01	0.00	0.00	0.01	0.01	0.31	1.6%	0.12	0.12	0.00	0.00	0.00	0.01	0.13	42.1%	42.1%	
51			2	1	0.31	0.00	0.00	0.00	0.01	0.32	4.1%	3.2%	0.11	0.00	0.00	0.00	0.01	0.13	40.3%	40.3%	
52			5	2	0.78	0.00	0.00	0.00	0.02	0.05	0.78	5.8%	1.9%	0.03	0.00	0.00	0.01	0.02	0.38	48.5%	48.5%
53			6	2	0.42	0.01	0.00	0.01	0.02	0.49	3.2%	1.6%	0.18	0.00	0.00	0.00	0.01	0.01	0.25	50.9%	50.9%
54			7	0.57	0.00	0.04	0.00	0.00	0.00	0.61	5.9%	0.00	0.24	0.00	0.00	0.00	0.01	0.27	44.0%	44.0%	
55			11	2	0.43	0.00	0.00	0.00	0.00	0.02	0.47	4.4%	0.6%	0.19	0.00	0.00	0.00	0.01	0.24	50.8%	50.8%
56			12	2	0.38	0.01	0.00	0.00	0.02	0.02	0.46	3.2%	0.16	0.00	0.00	0.00	0.01	0.01	0.22	46.9%	46.9%
57			15	5	1.51	0.02	0.00	0.05	0.14	1.51	94%	3.2%	0.74	0.02	0.00	0.03	0.06	0.82	53.9%	53.9%	
58			16	5	1.56	0.02	0.00	0.00	0.10	1.55	6.5%	1.0%	0.76	0.02	0.00	0.00	0.01	0.10	0.87	55.5%	55.5%
59			17	5	1.55	0.02	0.00	0.00	0.02	0.10	1.55	6.1%	0.78	0.02	0.00	0.01	0.04	0.91	58.6%	58.6%	
60			18	5	1.54	0.02	0.00	0.00	0.02	0.10	1.63	6.0%	1.1%	0.71	0.01	0.00	0.01	0.04	0.90	55.0%	55.0%
61			19	5	1.28	0.02	0.02	0.01	0.11	1.48	7.2%	0.5%	0.59	0.02	0.01	0.01	0.04	0.72	48.4%	48.4%	
62			25	1.36	0.00	0.00	0.00	0.01	0.11	1.53	7.3%	0.75	0.02	0.05	0.00	0.01	0.13	0.63	55.3%	55.3%	
63			26	5	1.60	0.02	0.00	0.00	0.02	0.10	1.59	6.4%	1.2%	0.81	0.01	0.00	0.02	0.05	0.93	57.7%	57.7%
64			27	5	1.54	0.02	0.00	0.00	0.01	0.10	1.58	6.0%	0.77	0.02	0.00	0.01	0.04	0.90	57.1%	57.1%	
65			28	5	1.41	0.02	0.01	0.02	0.11	1.58	6.8%	1.1%	0.67	0.02	0.01	0.01	0.05	0.81	51.1%	51.1%	
66			128	0.26	0.00	0.00	0.00	0.00	0.16	0.19	62.3%	0.11	0.00	0.00	0.00	0.00	0.07	0.09	42.0%	42.0%	
67			129	1	0.22	0.00	0.00	0.01	0.13	0.19	57.7%	0.13	0.00	0.00	0.00	0.00	0.05	0.08	41.0%	41.0%	
68	130	1	0.23	0.00	0.00	0.00	0.00	0.15	0.17	65.6%	0.9%	0.10	0.00	0.00	0.00	0.06	0.08	44.9%	44.9%		
69	133	2	0.48	0.00	0.00	0.00	0.02	0.23	0.39	48.8%	3.1%	0.22	0.00	0.00	0.01	0.11	0.17	45.2%	33.0%		
70	134	10	0.49	0.00	0.00	0.01	0.13	0.29	0.38	59.4%	0.38	0.21	0.00	0.00	0.01	0.13	0.17	43.9%	33.8%		
71	135	2	0.32	0.00	0.00	0.00	0.01	0.20	0.27	63.6%	1.9%	0.14	0.00	0.00	0.00	0.08	0.12	42.0%	36.7%		
72	139	2	0.41	0.00	0.00	0.01	0.26	0.31	62.7%	2.9%	0.16	0.00	0.00	0.00	0.01	0.12	0.13	40.3%	31.7%		
73	140	2	0.68	0.00	0.00	0.00	0.36	0.53	53.4%	0.11	0.34	0.00	0.00	0.00	0.19	0.24	49.6%	35.7%			
74	143	108	5	1.08	0.01	0.00	0.08	0.28	0.36	60.2%	0.50	0.01	0.00	0.00	0.05	0.46	0.66	46.6%	43.8%		
75	144	5	1.26	0.02	0.00	0.00	0.01	0.72	1.00	57.3%	0.6%	0.68	0.02	0.00	0.00	0.44	0.55	54.6%	44.1%		
76	145	5	1.32	0.01	0.00	0.00	0.68	1.08	51.9%	0.3%	0.77	0.01	0.00	0.00	0.42	0.63	58.2%	48.0%			
77	146	5	1.31	0.02	0.00	0.00	0.78	1.08	59.0%	1.0%	0.73	0.01	0.00	0.01	0.45	0.61	55.4%	46.0%			
78	147	119	0.42	0.02	0.01	0.01	0.03	0.42	0.51	63.1%	0.61	0.11	0.00	0.00	0.01	0.53	0.51	43.3%	43.3%		
79	153	5	1.20	0.02	0.00	0.00	0.03	0.78	0.97	64.7%	2.1%	0.60	0.02	0.00	0.02	0.46	0.52	50.4%	43.3%		
80	154	5	1.25	0.02	0.00	0.00	0.65	1.03	51.8%	0.3%	0.72	0.01	0.00	0.00	0.41	0.59	57.3%	46.7%			
81	156	5	1.41	0.02	0.00	0.01	0.78	1.16	55.0%	0.5%	0.82	0.02	0.00	0.00	0.47	0.67	57.7%	47.0%			
82	155	5	1.67	0.02	0.01	0.01	0.77	1.01	61.9%	0.8%	1.06	0.01	0.00	0.00	0.47	0.68	53.8%	44.4%			
83	0	128	2	0.46	0.00	0.01	0.01	0.21	0.42	45.3%	3.3%	1.53	0.18	0.00	0.01	0.10	0.10	39.8%	38.5%		
84	0	129	2	0.58	0.00	0.01	0.01	0.15	0.52	26.6%	2.1%	0.24	0.00	0.00	0.01	0.07	0.21	40.6%	37.0%		
85	2	130	2	0.54	0.00	0.00	0.02	0.18	0.51	33.4%	3.5%	0.23	0.00	0.00	0.00	0.07	0.20	42.1%	36.9%		
86	5	133	4	0.34	0.01	0.01	0.03	0.30	0.51	23.1%	2.4%	0.58	0.01	0.01	0.02	0.14	0.58	44.5%	44.5%		
87	6	134	4	0.34	0.00	0.00	0.02	0.35	0.51	37.9%	2.8%	0.43	0.01	0.00	0.00	0.01	0.17	40.5%	48.2%		
88	7	135	4	0.38	0.01	0.02	0.04	0.28	1.13	24.7%	3.7%	0.45	0.01	0.01	0.03	0.11	0.45	48.0%	42.6%		
89	11	139	4	0.82	0.01	0.01	0.02	0.35	0.85	41.9%	2.3%	0.38	0.01	0.01	0.02	0.17	0.42	49.6%	49.6%		
90	140	4	0.81	0.01	0.01	0.03	0.26	0.36	2.2%	2.9%	0.51	0.01	0.01	0.01	0.02	0.23	0.21	47.2%	42.3%		
91	15	143	10	2.94	0.03	0.01	0.15	0.91	2.42	30.2%	1.4%	1.40	0.02	0.01	0.10	0.54	1.35	47.7%	54.6%		
92	16	144	10	2.92	0.03	0.00	0.01	0.83	2.60	28.5%	0.4%	1.55	0.02	0.00	0.01	0.51	1.40	53.1%	47.8%		
93	17	145	10	2.90	0.02	0.00	0.02	0.81	2.73	28.0%	0.8%	1.65	0.02	0.00	0.02	0.48	1.52	56.9%	52.4%		
94	18	146	10	3.10	0.02	0.01	0.04	0.87	3.06	27.9%	1.4%	1.69	0.02	0.01	0.03	0.48	1.69	54.4%	54.4%		
95	19	147	10	2.97	0.02	0.00	0.02	0.84	2.84	31.8%	0.7%	1.71	0.02	0.00	0.03	0.53	1.64	51.3%	51.3%		
96	25	153	10	2.90	0.03	0.01	0.04	0.94	2.52	32.2%	1.3%	1.48	0.02	0.00	0.02	0.56	1.43	50.9%	49.6%		
97	26	154	10	2.88	0.02	0.00	0.02	0.76	2.68	26.4%	0.8%	1.61	0.02	0.00	0.02	0.46	1.47	55.7%	51.5%		
98	27	155	10	3.11	0.03	0.00	0.02	0.91	3.00	29.3%	0.7%	1.78	0.02	0.00	0.01	0.54	1.67	57.1%	53.0%		
99	130	0.03	0.02	0.09	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		

- L-patch High CH

						max ratio out of all beams								max ratio out of all beams																
						4cm2 PD(mW/cm2)				64.2%				6.4%				4cm2 PD(mW/cm2) at 10mm evaluation distance				58.6%				58.6%				
						ratio				ratio				ratio				ratio				ratio								
No.	Module	Type	Beam ID_1	Berna ID_2	Feed no.	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	(Front 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(worst- surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	(Front 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(worst- surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	(Front 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(worst- surface 2mm)	
49			0		1	0.16	0.00	0.00	0.00	0.01	0.18	7.1%	1.1%	0.05	0.00	0.00	0.00	0.01	0.08	40.8%	40.8%									
50			1		1	0.29	0.00	0.00	0.00	0.01	0.29	4.5%	1.4%	0.11	0.00	0.00	0.00	0.01	0.12	42.8%	42.8%									
51			2		1	0.29	0.00	0.00	0.01	0.01	0.29	4.4%	3.1%	0.10	0.00	0.00	0.00	0.01	0.01	40.5%	40.5%									
52			5		2	0.72	0.00	0.00	0.01	0.04	0.70	5.7%	1.8%	0.31	0.00	0.00	0.00	0.01	0.02	48.8%	48.8%									
53			6		2	0.35	0.00	0.00	0.01	0.02	0.41	3.9%	2.0%	0.15	0.00	0.00	0.00	0.01	0.01	51.1%	51.1%									
54			7		2	0.53	0.00	0.01	0.02	0.03	0.57	5.8%	2.8%	0.23	0.00	0.00	0.01	0.01	0.01	45.2%	45.2%									
55			11		2	0.35	0.00	0.00	0.00	0.02	0.39	6.0%	0.8%	0.15	0.00	0.00	0.00	0.00	0.01	0.19	50.4%	50.4%								
56			12		2	0.33	0.00	0.00	0.01	0.01	0.40	3.5%	3.5%	0.14	0.00	0.00	0.00	0.01	0.01	46.5%	46.5%									
57			15		5	1.39	0.02	0.00	0.05	0.13	1.38	9.3%	3.2%	0.68	0.02	0.00	0.00	0.01	0.12	53.9%	53.9%									
58			16		5	1.40	0.02	0.00	0.01	0.10	1.38	6.8%	0.5%	0.68	0.01	0.00	0.01	0.04	0.77	55.4%	55.4%									
59			17		5	1.39	0.02	0.00	0.01	0.09	1.39	6.3%	0.9%	0.71	0.01	0.00	0.01	0.04	0.82	58.6%	58.6%									
60			18		5	1.39	0.02	0.00	0.02	0.09	1.46	6.3%	1.4%	0.69	0.01	0.00	0.02	0.04	0.81	55.5%	55.5%									
61			19		5	1.16	0.02	0.01	0.01	0.09	1.33	7.0%	0.6%	0.55	0.01	0.01	0.01	0.04	0.64	48.3%	48.3%									
62			25		5	1.42	0.02	0.00	0.01	0.11	1.39	7.6%	0.7%	0.70	0.01	0.00	0.01	0.05	0.78	52.5%	52.5%									
63			26		5	1.44	0.02	0.00	0.02	0.09	1.43	6.5%	1.2%	0.73	0.01	0.00	0.01	0.04	0.83	57.7%	57.7%									
64			27		5	1.38	0.02	0.00	0.01	0.09	1.41	6.3%	0.6%	0.70	0.02	0.00	0.01	0.04	0.81	57.6%	57.6%									
65			28		5	1.28	0.02	0.01	0.02	0.10	1.43	6.7%	1.3%	0.62	0.01	0.01	0.01	0.04	0.73	50.9%	50.9%									
66			128		1	0.27	0.00	0.00	0.00	0.16	0.19	58.5%	1.5%	0.11	0.00	0.00	0.00	0.07	0.99	41.1%	31.5%									
67			129		1	0.22	0.00	0.00	0.01	0.12	0.18	53.9%	3.2%	0.09	0.00	0.00	0.00	0.05	0.07	40.6%	33.8%									
68			130		1	0.22	0.00	0.00	0.00	0.14	0.16	64.1%	0.9%	0.10	0.00	0.00	0.00	0.06	0.07	43.9%	31.4%									
69			133		2	0.48	0.00	0.00	0.02	0.21	0.38	44.2%	3.1%	0.21	0.00	0.00	0.01	0.10	0.17	44.9%	34.0%									
70			134		2	0.48	0.00	0.00	0.01	0.28	0.36	58.1%	1.9%	0.21	0.00	0.00	0.01	0.13	0.16	44.6%	33.7%									
71			135		2	0.34	0.00	0.00	0.01	0.19	0.29	55.5%	1.5%	0.14	0.00	0.00	0.00	0.08	0.12	41.3%	35.8%									
72			139		4	0.50	0.00	0.00	0.01	0.25	0.30	61.9%	2.9%	0.17	0.00	0.00	0.01	0.12	0.13	41.0%	31.7%									
73			140		2	0.64	0.00	0.00	0.00	0.32	0.50	49.4%	0.3%	0.32	0.00	0.00	0.00	0.17	0.23	50.3%	35.7%									
74			143		5	1.02	0.01	0.01	0.07	0.61	0.85	59.7%	6.4%	0.48	0.01	0.00	0.05	0.36	0.45	47.1%	44.2%									
75			144		5	1.23	0.02	0.00	0.01	0.68	0.97	55.7%	0.7%	0.66	0.02	0.00	0.01	0.41	0.53	53.6%	42.9%									
76			145		5	1.28	0.01	0.00	0.00	0.66	1.05	51.1%	0.3%	0.75	0.01	0.00	0.00	0.41	0.61	58.0%	47.7%									
77			146		5	1.31	0.01	0.00	0.01	0.66	1.09	50.6%	0.8%	0.73	0.01	0.00	0.01	0.38	0.61	55.6%	46.6%									
78			147		5	1.23	0.01	0.01	0.01	0.65	0.98	53.0%	1.1%	0.64	0.01	0.01	0.01	0.37	0.53	52.0%	43.0%									
79			153		5	1.13	0.02	0.00	0.02	0.73	0.90	64.2%	1.8%	0.58	0.02	0.00	0.01	0.43	0.49	51.1%	43.1%									
80			154		5	1.24	0.01	0.00	0.01	0.63	1.01	50.7%	0.5%	0.71	0.01	0.00	0.01	0.40	0.57	56.8%	45.5%									
81			155		5	1.36	0.02	0.00	0.01	0.69	1.12	50.8%	0.7%	0.69	0.01	0.00	0.01	0.42	0.64	58.0%	47.8%									
82			156		5	1.26	0.01	0.01	0.01	0.65	1.04	51.6%	1.0%	0.69	0.01	0.00	0.01	0.37	0.57	54.5%	44.9%									
83			0	128	2	0.42	0.00	0.01	0.01	0.22	0.38	51.4%	1.9%	0.18	0.00	0.01	0.01	0.10	0.16	42.7%	36.7%									
84			1	129	2	0.59	0.00	0.00	0.01	0.16	0.53	26.5%	2.0%	0.24	0.00	0.00	0.01	0.07	0.22	41.0%	37.2%									
85			2	130	2	0.53	0.00	0.00	0.02	0.18	0.49	33.6%	3.4%	0.23	0.00	0.00	0.01	0.08	0.19	42.2%	36.9%									
86			5	133	4	1.25	0.01	0.01	0.03	0.28	1.12	22.7%	2.5%	0.58	0.00	0.01	0.02	0.13	0.53	46.1%	42.5%									
87			6	134	4	0.82	0.01	0.00	0.02	0.36	0.77	44.5%	2.1%	0.40	0.01	0.00	0.01	0.18	0.38	49.4%	46.6%									
88			7	135	4	1.05	0.01	0.01	0.04	0.25	1.12	22.5%	3.4%	0.45	0.00	0.01	0.03	0.10	0.48	42.9%	42.9%									
89			11	139	4	0.78	0.01	0.01	0.02	0.36	0.73	46.7%	2.6%	0.36	0.01	0.01	0.02	0.18	0.36	46.7%	45.6%									
90			12	140	4	1.10	0.01	0.01	0.02	0.41	0.99	37.0%	2.2%	0.54	0.01	0.01	0.02	0.23	0.46	41.4%	44.8%									
91			15	143	10	2.83	0.02	0.01	0.14	0.85	2.27	30.0%	4.9%	1.37	0.02	0.01	0.10	0.52	1.25	48.5%	44.3%									
92			16	144	10	2.85	0.03	0.00	0.01	0.84	2.50	29.5%	6.0%	1.53	0.02	0.00	0.01	0.51	1.33	53.9%	52.8%									
93			17	145	10	2.83	0.02	0.00	0.02	0.82	2.64	28.8%	0.7%	1.63	0.02	0.00	0.02	0.49	1.47	57.7%	46.6%									
94			18	146	10	2.95	0.02	0.01	0.05	0.81	2.89	27.5%	1.7%	1.62	0.02	0.01	0.04	0.43	1.59	55.1%	54.0%									
95			19	147	10	2.81	0.02	0.02	0.04	0.81	2.84	28.4%	1.4%	1.47	0.02	0.02	0.03	0.45	1.47	51.7%	51.7%									
96			25	153	5	0.89	0.03	0.01	0.03	0.94	1.27	33.5%	1.2%	1.47	0.02	0.01	0.02	0.56	1.29	52.3%	46.0%									
97			26	154	10	2.84	0.02	0.00	0.02	0.76	2.61	26.6%	0.8%	1.60	0.02	0.00	0.02	0.46	1.43	56.4%	50.5%									
98			27	155	10	2.91	0.02	0.00	0.02	0.82	2.82	29.6%	0.8%	1.71	0.02	0.00	0.02	0.47	1.52	53.7%	53.0%									
99			28	156	10	2.89	0.02	0.02	0.06	0.78	2.90	27.0%	2.1%	1.55	0.02	0.01	0.05	0.43	1.54	53.3%	50.5%									

Table 6. PD of Ant L – patch antenna (39GHz – n260)

- L-patch Low CH

						max ratio out of all beams								max ratio out of all beams								
						4cm2 PD(mW/cm2)				100.0%		9.7%		4cm2 PD(mW/cm2) at 10mm evaluation distance				64.1%		64.1%		
No.	Module	Type	Beam ID_1	Bema ID_2	Feed no.	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Front 2mm)/(worst- surface 2mm)	ratio (Bottom 2mm)/(worst- surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (back 10mm)/(worst- surface 2mm)	
55			0		1	0.11	0.00	0.00	0.00	0.05	0.07	44.7%	1.8%	0.05	0.00	0.00	0.00	0.03	0.03	42.6%	23.7%	
56			1		1	0.10	0.00	0.00	0.00	0.08	0.06	81.2%	1.0%	0.04	0.00	0.00	0.00	0.04	0.03	42.6%	24.8%	
57			2		1	0.09	0.00	0.00	0.01	0.08	0.06	85.6%	6.7%	0.04	0.00	0.00	0.01	0.03	0.02	42.6%	23.3%	
58			3		1	0.08	0.00	0.00	0.00	0.09	0.05	100.0%	3.4%	0.03	0.00	0.00	0.00	0.03	0.02	37.1%	21.3%	
59			6		2	0.19	0.00	0.00	0.03	0.19	0.12	97.9%	8.9%	0.09	0.00	0.00	0.01	0.09	0.05	46.6%	24.9%	
60			9		2	0.19	0.00	0.00	0.00	0.06	0.13	30.6%	1.6%	0.09	0.00	0.00	0.00	0.02	0.06	46.6%	32.8%	
61			10		2	0.29	0.00	0.00	0.00	0.17	0.15	58.7%	1.0%	0.10	0.00	0.00	0.00	0.08	0.06	35.1%	22.2%	
62			14		2	0.21	0.00	0.00	0.00	0.19	0.12	88.6%	0.5%	0.09	0.00	0.00	0.00	0.08	0.05	40.8%	22.7%	
63			15		2	0.27	0.00	0.00	0.01	0.16	0.16	42.9%	1.1%	0.11	0.00	0.00	0.00	0.06	0.07	41.2%	27.8%	
64			18		5	0.46	0.01	0.01	0.03	0.26	0.36	56.7%	6.3%	0.19	0.01	0.01	0.02	0.17	0.17	41.3%	36.1%	
65			19		5	0.35	0.01	0.00	0.01	0.39	0.26	100.0%	1.3%	0.18	0.01	0.00	0.00	0.21	0.13	52.7%	33.0%	
66			20		5	0.35	0.01	0.00	0.01	0.26	0.20	73.9%	1.7%	0.20	0.01	0.00	0.01	0.15	0.08	58.6%	24.3%	
67			21		5	0.40	0.01	0.00	0.04	0.26	0.31	58.8%	7.4%	0.23	0.00	0.00	0.03	0.12	0.16	44.2%	34.1%	
68			22		5	0.41	0.01	0.01	0.02	0.36	0.27	88.1%	5.1%	0.16	0.01	0.01	0.02	0.17	0.13	42.1%	30.9%	
69			28		5	0.44	0.01	0.01	0.03	0.33	0.30	76.3%	5.9%	0.17	0.01	0.01	0.02	0.16	0.13	39.0%	29.7%	
70			29		5	0.30	0.01	0.00	0.00	0.27	0.18	88.7%	1.3%	0.18	0.01	0.00	0.00	0.15	0.08	60.1%	26.2%	
71			30		4	0.41	0.01	0.00	0.03	0.30	0.28	70.2%	4.2%	0.22	0.01	0.00	0.01	0.14	0.13	52.1%	32.1%	
72			31		5	0.46	0.01	0.01	0.03	0.33	0.30	72.4%	5.5%	0.18	0.01	0.01	0.02	0.15	0.14	39.5%	29.6%	
73			128		1	0.25	0.00	0.00	0.00	0.07	0.21	26.2%	1.6%	0.09	0.00	0.00	0.00	0.04	0.09	36.9%	34.1%	
74			129		1	0.18	0.00	0.00	0.00	0.04	0.19	22.1%	1.6%	0.06	0.00	0.00	0.00	0.02	0.08	40.9%	40.9%	
75			130		1	0.23	0.00	0.00	0.01	0.06	0.22	27.6%	2.6%	0.08	0.00	0.00	0.01	0.03	0.09	38.6%	38.6%	
76			131		1	0.16	0.00	0.00	0.00	0.05	0.16	31.7%	2.4%	0.05	0.00	0.00	0.00	0.03	0.07	40.9%	40.9%	
77			136		2	0.43	0.01	0.01	0.01	0.11	0.39	25.4%	2.3%	0.17	0.00	0.00	0.01	0.05	0.16	39.4%	36.6%	
78			137		2	0.47	0.00	0.00	0.01	0.10	0.43	20.3%	1.3%	0.20	0.00	0.00	0.00	0.05	0.23	49.6%	49.6%	
79			138		2	0.41	0.00	0.01	0.09	0.42	0.20	20.5%	1.3%	0.13	0.00	0.00	0.01	0.03	0.18	43.1%	43.1%	
80			142		2	0.40	0.00	0.01	0.01	0.08	0.42	19.5%	1.2%	0.14	0.00	0.01	0.00	0.04	0.20	48.1%	48.1%	
81			143		2	0.43	0.00	0.01	0.01	0.10	0.40	24.2%	2.4%	0.16	0.00	0.01	0.01	0.04	0.15	37.9%	35.1%	
82			146		5	0.66	0.00	0.02	0.07	0.13	0.69	18.3%	9.7%	0.28	0.01	0.01	0.06	0.06	0.33	47.7%	47.9%	
83			147		0.93	0.07	0.01	0.01	0.01	0.20	0.85	21.5%	4.5%	0.31	0.00	0.00	0.01	0.11	0.39	62.2%	62.2%	
84			148		5	0.80	0.01	0.00	0.02	0.29	0.70	36.0%	2.0%	0.38	0.01	0.00	0.01	0.17	0.38	48.3%	48.3%	
85			149		5	0.84	0.01	0.01	0.05	0.15	0.77	18.0%	5.8%	0.38	0.01	0.01	0.04	0.07	0.37	44.8%	43.6%	
86			150		5	0.60	0.00	0.02	0.04	0.17	0.70	24.5%	6.3%	0.25	0.00	0.02	0.04	0.09	0.34	48.9%	48.9%	
87			156		0.01	0.77	0.00	0.01	0.16	0.83	19.0%	1.3%	0.36	0.00	0.00	0.01	0.03	0.46	55.4%	55.4%		
88			157		5	0.89	0.01	0.01	0.01	0.27	0.87	30.5%	0.8%	0.43	0.01	0.00	0.01	0.16	0.53	59.3%	59.3%	
89			158		5	0.91	0.02	0.00	0.03	0.22	0.81	24.4%	3.2%	0.46	0.01	0.00	0.02	0.13	0.45	50.7%	49.5%	
90			159		5	0.65	0.01	0.02	0.05	0.12	0.64	18.7%	7.4%	0.26	0.01	0.02	0.04	0.06	0.28	43.1%	43.1%	
91			128		2	0.46	0.00	0.01	0.01	0.17	0.36	35.3%	1.5%	0.17	0.00	0.00	0.01	0.09	0.16	34.0%	34.0%	
92			129		2	0.38	0.00	0.00	0.00	0.19	0.29	49.1%	1.3%	0.14	0.00	0.00	0.00	0.10	0.13	37.1%	34.7%	
93			130		2	0.44	0.00	0.00	0.00	0.20	0.35	45.1%	3.0%	0.17	0.00	0.00	0.00	0.18	0.15	38.9%	34.3%	
94			131		2	0.33	0.00	0.00	0.00	0.21	0.25	62.3%	2.1%	0.13	0.00	0.00	0.01	0.08	0.11	39.2%	32.3%	
95			136		4	0.63	0.01	0.01	0.03	0.33	0.52	44.1%	1.2%	0.27	0.00	0.01	0.02	0.13	0.26	42.5%	41.6%	
96			137		4	0.81	0.01	0.00	0.01	0.16	0.66	19.2%	1.7%	0.34	0.00	0.00	0.01	0.08	0.35	42.7%	42.7%	
97			138		4	0.93	0.01	0.02	0.02	0.40	0.68	42.7%	1.7%	0.34	0.01	0.01	0.01	0.18	0.26	36.1%	27.6%	
98			142		4	0.72	0.01	0.02	0.01	0.42	0.60	51.7%	1.2%	0.25	0.01	0.01	0.01	0.17	0.32	44.4%	44.4%	
99			143		4	0.99	0.01	0.01	0.02	0.41	0.73	34.7%	1.0%	0.41	0.01	0.00	0.01	0.32	0.16	41.6%	35.2%	
100			146		10	1.21	0.02	0.03	0.11	0.66	1.24	47.8%	2.8%	0.55	0.02	0.03	0.09	0.51	0.25	42.3%	37.2%	
101			19		147	1.66	0.03	0.01	0.02	0.68	1.65	40.8%	1.3%	0.78	0.02	0.01	0.02	0.34	1.06	64.1%	64.1%	
102			20		148	1.71	0.03	0.00	0.03	0.70	1.28	40.0%	1.9%	0.87	0.02	0.00	0.03	0.42	1.01	50.6%	41.8%	
103			149		20	1.91	0.02	0.02	0.11	1.47	1.87	28.5%	5.6%	0.66	0.07	0.03	0.08	0.38	0.75	46.5%	39.8%	
104			22		150	1.39	0.02	0.04	0.09	0.82	1.35	59.2%	2.5%	0.82	0.02	0.04	0.01	0.40	0.72	51.4%	51.4%	
105			28		156	1.0	0.13	0.02	0.03	0.12	0.76	1.56	48.9%	7.4%	0.62	0.02	0.03	0.08	0.38	0.87	55.8%	55.8%
106			29		157	1.0	0.16	0.04	0.01	0.02	0.69	1.29	46.9%	1.1%	0.72	0.03	0.01	0.01	0.40	0.80	54.9%	54.9%
107			30		158	1.0	0.03	0.00	0.05	0.66	1.61	33.1%	2.4%	1.06	0.03	0.00	0.04	0.39	0.88	53.0%	44.9%	
108			159		10	1.0	0.04	0.00	0.01	1.21	1.01	45.9%	0.9%	0.61	0.02	0.00	0.09	0.34	0.51	40.9%	37.2%	

- L-patch Mid CH

						max ratio out of all beams										max ratio out of all beams									
						4cm2 PD(mW/cm2)						100.0%		7.9%		4cm2 PD(mW/cm2) at 10mm evaluation distance						59.5%		53.9%	
No.	Module	Type	Beam ID_1	Berna ID_2	Feed no.	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Front 2mm)/(worst-surface 2mm)	ratio (Bottom 2mm)/(worst-surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (back 10mm)/(worst-surface 2mm)				
55	L	Patch	0	1	0.09	0.00	0.00	0.00	0.03	0.07	33.0%	1.1%	0.03	0.00	0.00	0.00	0.01	0.03	33.0%	33.0%					
56			1	1	0.12	0.00	0.00	0.00	0.05	0.07	44.3%	1.6%	0.05	0.00	0.00	0.00	0.03	0.02	44.3%	19.7%					
57			2	1	0.15	0.00	0.00	0.01	0.10	0.10	66.9%	4.0%	0.07	0.00	0.00	0.01	0.05	0.03	46.4%	21.9%					
58			3	1	0.11	0.00	0.00	0.00	0.08	0.07	79.2%	3.8%	0.05	0.00	0.00	0.00	0.03	0.03	47.2%	27.4%					
59			8	2	0.19	0.01	0.00	0.02	0.23	0.15	100.0%	7.5%	0.05	0.00	0.00	0.01	0.11	0.06	46.9%	27.9%					
60			9	2	0.18	0.00	0.00	0.00	0.08	0.14	44.0%	2.3%	0.08	0.00	0.00	0.00	0.02	0.07	42.9%	41.1%					
61			10	2	0.23	0.00	0.00	0.00	0.09	0.15	38.4%	1.7%	0.09	0.00	0.00	0.00	0.04	0.05	39.3%	21.8%					
62			14	2	0.20	0.00	0.00	0.00	0.09	0.11	45.1%	1.0%	0.09	0.00	0.00	0.00	0.04	0.05	47.7%	25.6%					
63			15	2	0.22	0.00	0.00	0.01	0.08	0.16	37.8%	2.3%	0.09	0.00	0.00	0.00	0.03	0.07	39.6%	30.4%					
64			18	5	0.43	0.01	0.01	0.03	0.27	0.37	62.4%	5.9%	0.16	0.01	0.01	0.02	0.13	0.22	51.6%	51.6%					
65			19	5	0.37	0.01	0.00	0.02	0.39	0.26	100.0%	3.8%	0.21	0.01	0.00	0.01	0.18	0.11	52.7%	29.0%					
66			20	5	0.70	0.01	0.00	0.01	0.30	0.43	43.1%	0.7%	0.40	0.01	0.00	0.00	0.14	0.23	56.8%	33.2%					
67			21	5	0.42	0.01	0.00	0.03	0.24	0.32	58.3%	7.9%	0.18	0.01	0.00	0.03	0.13	0.19	45.1%	45.1%					
68			22	5	0.45	0.01	0.01	0.02	0.33	0.35	74.0%	4.3%	0.15	0.01	0.01	0.02	0.16	0.14	36.5%	32.1%					
69			28	5	0.46	0.01	0.01	0.02	0.30	0.39	64.9%	4.6%	0.16	0.01	0.01	0.02	0.15	0.19	40.1%	40.1%					
70			29	5	0.62	0.01	0.00	0.00	0.35	0.35	56.4%	0.5%	0.37	0.01	0.00	0.00	0.17	0.20	59.5%	32.1%					
71			30	5	0.35	0.01	0.00	0.01	0.24	0.24	68.4%	3.5%	0.18	0.01	0.00	0.01	0.12	0.13	51.6%	37.4%					
72			31	5	0.47	0.01	0.01	0.02	0.28	0.38	59.7%	5.1%	0.17	0.01	0.01	0.02	0.13	0.19	39.6%	39.6%					
73			128	1	0.25	0.00	0.00	0.00	0.09	0.19	35.4%	0.4%	0.09	0.00	0.00	0.00	0.05	0.08	36.6%	29.9%					
74			129	1	0.20	0.00	0.00	0.00	0.06	0.18	31.2%	2.0%	0.08	0.00	0.00	0.00	0.03	0.07	38.1%	36.6%					
75			130	1	0.22	0.00	0.00	0.00	0.07	0.20	33.9%	1.8%	0.10	0.00	0.00	0.00	0.04	0.08	44.0%	37.2%					
76			131	1	0.16	0.00	0.00	0.00	0.07	0.15	42.0%	1.9%	0.07	0.00	0.00	0.00	0.03	0.06	41.4%	39.5%					
77			136	2	0.44	0.00	0.00	0.01	0.14	0.36	31.4%	1.6%	0.18	0.00	0.00	0.01	0.07	0.18	41.1%	41.1%					
78			137	2	0.50	0.01	0.00	0.00	0.12	0.43	23.2%	0.6%	0.25	0.00	0.00	0.00	0.05	0.22	50.1%	44.3%					
79			138	2	0.42	0.00	0.01	0.01	0.12	0.34	27.8%	1.4%	0.14	0.00	0.01	0.01	0.05	0.12	34.1%	32.9%					
80			142	2	0.40	0.00	0.01	0.01	0.12	0.34	29.0%	1.5%	0.14	0.00	0.01	0.00	0.05	0.14	35.2%	35.2%					
81			143	2	0.44	0.00	0.01	0.01	0.13	0.36	30.4%	1.6%	0.17	0.00	0.00	0.01	0.06	0.18	40.2%	40.2%					
82			146	5	0.70	0.01	0.01	0.05	0.23	0.55	32.4%	7.2%	0.32	0.01	0.01	0.04	0.11	0.26	45.3%	37.1%					
83			147	5	0.88	0.01	0.00	0.07	0.35	0.82	29.0%	1.0%	0.45	0.01	0.00	0.01	0.14	0.47	53.9%	53.9%					
84			148	5	0.81	0.02	0.00	0.01	0.33	0.70	40.2%	1.4%	0.41	0.01	0.00	0.01	0.19	0.38	50.9%	46.1%					
85			149	5	0.88	0.01	0.01	0.04	0.24	0.73	27.4%	4.3%	0.39	0.01	0.01	0.03	0.12	0.36	44.3%	41.0%					
86			150	5	0.56	0.01	0.01	0.01	0.19	0.53	23.8%	6.7%	0.31	0.00	0.01	0.03	0.10	0.24	40.6%	40.6%					
87			156	5	0.66	0.01	0.01	0.04	0.19	0.66	28.5%	6.5%	0.31	0.00	0.01	0.03	0.09	0.33	49.7%	49.7%					
88			157	5	0.89	0.01	0.01	0.00	0.32	0.77	36.3%	0.4%	0.48	0.01	0.01	0.00	0.20	0.46	53.5%	51.3%					
89			158	5	0.88	0.02	0.00	0.02	0.28	0.78	32.2%	1.7%	0.45	0.01	0.00	0.01	0.16	0.42	51.6%	48.1%					
90			159	5	0.68	0.01	0.02	0.04	0.21	0.55	31.3%	6.3%	0.29	0.01	0.01	0.03	0.10	0.26	42.7%	37.8%					
91			0 128	2	0.46	0.01	0.01	0.00	0.14	0.32	30.4%	0.9%	0.15	0.00	0.01	0.00	0.08	0.16	35.2%	35.2%					
92			1 129	2	0.44	0.00	0.00	0.01	0.17	0.31	38.4%	2.0%	0.18	0.00	0.00	0.01	0.08	0.12	40.0%	27.8%					
93			2 130	2	0.59	0.01	0.00	0.01	0.23	0.40	38.8%	1.7%	0.25	0.00	0.00	0.01	0.11	0.17	42.7%	29.3%					
94			3 131	2	0.37	0.00	0.00	0.01	0.20	0.29	52.9%	2.1%	0.16	0.00	0.00	0.01	0.08	0.12	41.7%	31.8%					
95			8 136	4	0.75	0.01	0.01	0.02	0.27	0.66	36.5%	3.1%	0.32	0.01	0.01	0.02	0.13	0.33	44.4%	44.4%					
96			9 137	4	0.78	0.01	0.00	0.01	0.19	0.63	24.5%	0.9%	0.37	0.01	0.00	0.01	0.09	0.31	47.4%	39.8%					
97			10 138	4	0.87	0.01	0.01	0.02	0.33	0.59	38.3%	2.0%	0.32	0.01	0.01	0.01	0.16	0.24	36.8%	27.7%					
98			14 142	4	0.77	0.01	0.02	0.01	0.33	0.51	42.5%	1.3%	0.28	0.00	0.01	0.01	0.14	0.26	36.1%	33.1%					
99			15 143	4	0.87	0.01	0.01	0.02	0.32	0.63	36.8%	2.3%	0.36	0.01	0.01	0.02	0.17	0.31	40.8%	35.8%					
100			18 146	10	1.67	0.03	0.03	0.12	0.72	1.24	42.8%	6.9%	0.76	0.02	0.03	0.09	0.35	0.63	45.5%	37.9%					
101			19 147	10	1.57	0.03	0.01	0.04	0.85	1.27	54.3%	2.2%	0.85	0.02	0.01	0.03	0.42	0.78	54.1%	49.6%					
102			20 148	10	2.08	0.03	0.01	0.06	0.67	1.49	32.0%	1.0%	1.08	0.02	0.01	0.02	0.33	0.86	52.0%	41.2%					
103			21 149	10	2.03	0.03	0.02	0.10	0.81	1.56	39.7%	5.0%	0.97	0.03	0.02	0.08	0.41	0.81	47.3%	39.6%					
104			22 150	10	1.61	0.02	0.05	0.07	0.80	1.14	49.5%	4.6%	0.60	0.01	0.05	0.06	0.38	0.55	37.1%	34.1%					
105			28 156	10	1.49	0.02	0.04	0.10	0.70	1.37	46.7%	6.5%	0.59	0.02	0.04	0.07	0.35	0.72	47.9%	47.9%					
106			29 157	10	2.18	0.03	0.02	0.01	0.80	1.53	36.8%	0.5%	0.49	0.02	0.00	0.01	0.44	0.95	54.0%	44.3%					
107			30 158	10	1.81	0.03	0.01	0.03	0.72	1.35	39.8%	1.9%	0.40	0.03	0.00	0.03	0.40	0.80	49.8%	44.3%					
108			31 159	10	1.83	0.02	0.05	0.10	0.69	1.27	37.4%	5.4%	0.79	0.02	0.04	0.08	0.33	0.60	43.3%	32.5%					

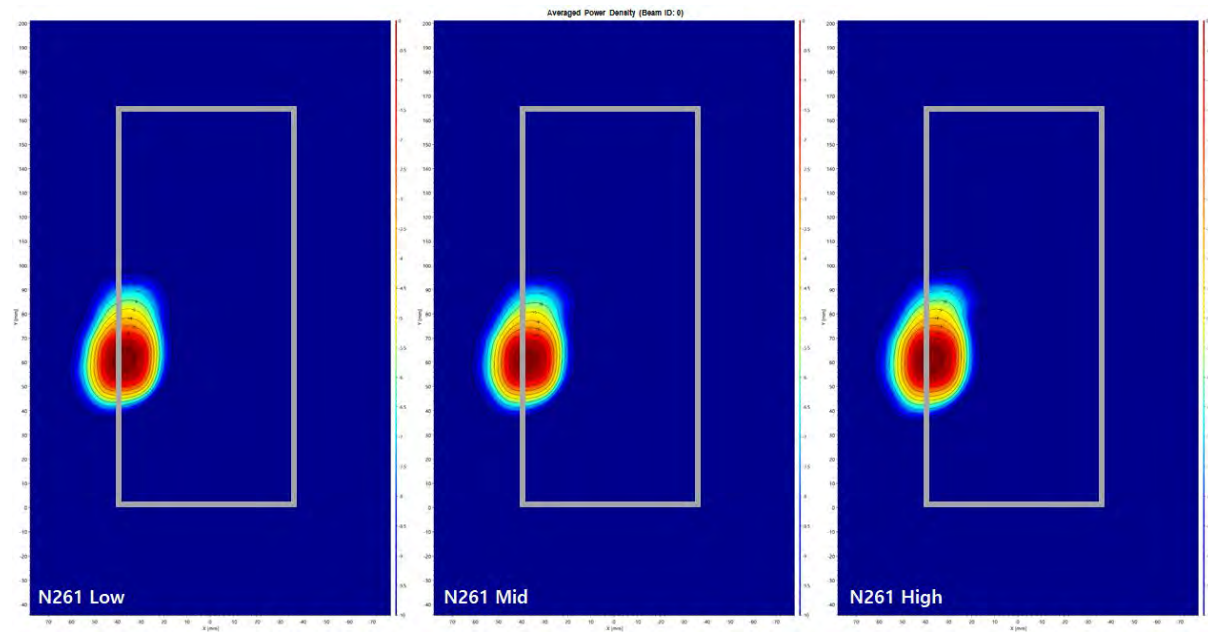
- L-patch High CH

						max ratio out of all beams										max ratio out of all beams									
No.	Module	Type	Beam ID_1	Berna ID_2	Feed no.	4cm2 PD(mW/cm2)						69.9%		7.4%		4cm2 PD(mW/cm2) at 10mm evaluation distance						54.5%		49.7%	
						S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio (Front 2mm)/(worst-surface 2mm)	ratio (Bottom 2mm)/(worst-surface 2mm)	S4(Right)	S3(Left)	S5(Top)	S6(Bottom)	S1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (back 10mm)/(worst-surface 2mm)				
55	L	Patch	0	1	0.09	0.00	0.00	0.00	0.04	0.07	42.4%	1.1%	0.03	0.00	0.01	0.03	33.7%	28.3%							
56			1	0.12	0.00	0.00	0.00	0.05	0.08	44.3%	0.8%	0.05	0.00	0.00	0.00	0.02	0.03	42.6%	27.9%						
57			2	0.23	0.00	0.00	0.01	0.09	0.13	39.1%	2.6%	0.10	0.00	0.00	0.01	0.04	0.06	44.6%	23.9%						
58			3	0.20	0.00	0.00	0.00	0.09	0.12	43.4%	0.6%	0.09	0.00	0.00	0.00	0.03	0.05	43.3%	26.3%						
59			8	2	0.35	0.01	0.00	0.02	0.18	0.19	51.0%	4.3%	0.13	0.00	0.00	0.01	0.09	0.06	38.0%	18.6%					
60			9	2	0.21	0.00	0.00	0.00	0.12	0.16	53.7%	1.9%	0.10	0.00	0.00	0.00	0.04	0.07	47.7%	33.2%					
61			10	2	0.24	0.00	0.00	0.00	0.09	0.17	39.3%	0.8%	0.10	0.00	0.00	0.00	0.03	0.07	41.0%	29.1%					
62			14	2	0.17	0.00	0.00	0.00	0.08	0.11	44.4%	1.2%	0.06	0.00	0.00	0.00	0.03	0.09	43.0%	30.0%					
63			15	2	0.25	0.11	0.00	0.00	0.11	0.19	46.3%	1.6%	0.12	0.00	0.00	0.00	0.04	0.08	44.3%	32.6%					
64			18	5	0.43	0.01	0.01	0.03	0.30	0.30	69.9%	5.9%	0.18	0.01	0.01	0.02	0.14	0.16	41.2%	37.4%					
65			18	5	0.66	0.01	0.01	0.01	0.40	0.39	60.9%	2.1%	0.32	0.01	0.01	0.01	0.17	0.19	48.8%	29.8%					
66			20	5	0.89	0.01	0.00	0.00	0.62	0.57	44.9%	0.7%	0.45	0.01	0.00	0.01	0.22	0.24	52.9%	38.0%					
67			21	5	0.52	0.01	0.00	0.02	0.27	0.31	51.1%	2.0%	0.27	0.01	0.00	0.02	0.12	0.16	48.4%	31.4%					
68			22	5	0.48	0.01	0.01	0.02	0.27	0.33	55.4%	4.0%	0.23	0.01	0.01	0.02	0.13	0.16	33.3%	31.4%					
69			28	5	0.47	0.01	0.01	0.02	0.26	0.34	56.3%	3.3%	0.20	0.01	0.01	0.02	0.12	0.18	42.2%	38.5%					
70			29	5	0.88	0.01	0.01	0.01	0.41	0.54	46.9%	0.6%	0.47	0.01	0.00	0.00	0.23	0.31	53.7%	35.3%					
71			30	5	0.80	0.01	0.00	0.02	0.34	0.47	42.0%	2.2%	0.42	0.01	0.00	0.01	0.16	0.24	36.2%	28.0%					
72			31	5	0.49	0.01	0.01	0.02	0.26	0.32	52.1%	4.1%	0.19	0.01	0.01	0.02	0.11	0.18	37.8%	36.0%					
73			128	1	0.19	0.00	0.00	0.00	0.09	0.13	50.5%	2.2%	0.07	0.00	0.00	0.00	0.05	0.06	38.2%	30.1%					
74			129	1	0.21	0.00	0.00	0.01	0.07	0.17	33.5%	2.4%	0.09	0.00	0.00	0.00	0.04	0.07	43.4%	32.1%					
75			130	2	0.20	0.00	0.00	0.00	0.10	0.18	48.3%	1.5%	0.20	0.00	0.00	0.00	0.05	0.08	37.5%	37.5%					
76			131	1	0.15	0.00	0.00	0.00	0.08	0.14	51.3%	1.3%	0.06	0.00	0.00	0.00	0.04	0.06	41.6%	36.4%					
77			136	2	0.41	0.00	0.00	0.02	0.15	0.32	31.6%	3.9%	0.15	0.00	0.00	0.01	0.07	0.11	37.3%	26.8%					
78			137	2	0.47	0.01	0.00	0.00	0.15	0.41	36.9%	0.6%	0.25	0.00	0.00	0.00	0.08	0.20	53.8%	43.0%					
79			138	2	0.37	0.00	0.00	0.01	0.18	0.30	30.8%	0.8%	0.13	0.00	0.00	0.01	0.10	0.12	36.2%	32.4%					
80			142	2	0.35	0.00	0.01	0.01	0.11	0.29	32.3%	3.1%	0.14	0.00	0.01	0.01	0.04	0.12	39.9%	35.4%					
81			143	2	0.40	0.00	0.00	0.02	0.14	0.31	34.7%	4.0%	0.14	0.00	0.00	0.01	0.07	0.10	35.0%	25.6%					
82			146	5	0.62	0.01	0.01	0.05	0.27	0.53	42.8%	7.4%	0.28	0.01	0.01	0.04	0.12	0.24	44.4%	40.1%					
83			147	0.07	0.31	0.07	0.01	0.17	0.16	35.2%	0.3%	0.46	0.01	0.01	0.01	0.19	0.43	52.7%	49.2%						
84			148	0.04	0.02	0.00	0.01	0.38	0.71	45.3%	0.9%	0.44	0.01	0.00	0.01	0.22	0.37	51.5%	43.5%						
85	149	5	0.73	0.01	0.01	0.03	0.26	0.56	36.2%	0.4%	0.36	0.01	0.01	0.03	0.12	0.26	49.7%	35.7%							
86	150	5	0.60	0.01	0.00	0.03	0.24	0.56	39.0%	5.5%	0.38	0.01	0.01	0.03	0.11	0.27	46.6%	37.9%							
87	156	5	0.69	0.01	0.00	0.06	0.24	0.67	34.0%	0.7%	0.24	0.01	0.01	0.03	0.13	0.25	49.1%	40.9%							
88	157	5	0.88	0.02	0.01	0.01	0.37	0.75	42.5%	0.6%	0.48	0.01	0.00	0.00	0.22	0.41	54.5%	46.9%							
89	158	5	0.90	0.02	0.00	0.02	0.32	0.76	35.2%	2.4%	0.47	0.02	0.00	0.02	0.19	0.40	52.5%	44.3%							
90	159	5	0.63	0.01	0.01	0.04	0.25	0.53	38.7%	6.6%	0.25	0.01	0.01	0.03	0.11	0.23	38.9%	36.2%							
91	0	128	1	0.42	0.00	0.00	0.01	0.17	0.24	39.6%	0.7%	0.14	0.00	0.00	0.01	0.07	37.4%	28.3%							
92	1	129	2	0.49	0.00	0.00	0.01	0.16	0.34	33.1%	1.6%	0.19	0.00	0.00	0.01	0.07	0.15	39.7%	30.1%						
93	2	130	2	0.57	0.01	0.00	0.01	0.21	0.37	36.8%	2.1%	0.24	0.00	0.00	0.01	0.10	0.16	42.3%	28.2%						
94	3	131	2	0.45	0.00	0.00	0.01	0.19	0.29	42.2%	2.0%	0.19	0.00	0.01	0.00	0.13	0.23	42.2%	29.7%						
95	4	136	4	0.79	0.01	0.01	0.03	0.29	0.55	37.4%	0.1%	0.42	0.01	0.00	0.01	0.16	0.18	40.0%	40.0%						
96	9	137	4	0.82	0.01	0.00	0.01	0.30	0.63	37.0%	1.2%	0.42	0.01	0.00	0.01	0.12	0.33	51.6%	39.8%						
97	10	138	4	0.82	0.01	0.02	0.02	0.26	0.58	31.8%	2.7%	0.31	0.01	0.01	0.02	0.13	0.20	37.7%	24.8%						
98	14	142	4	0.73	0.01	0.02	0.01	0.23	0.51	31.8%	1.7%	0.22	0.00	0.02	0.01	0.10	0.25	33.7%	33.7%						
99	143	0.01	0.63	0.01	0.00	0.03	0.32	0.60	36.1%	0.1%	0.39	0.01	0.01	0.01	0.12	0.23	43.2%	40.2%							
100	18	146	0	1.65	0.04	0.04	0.10	0.92	1.19	55.8%	1.1%	0.77	0.03	0.03	0.08	0.44	0.54	46.8%	28.0%						
101	19	147	10	1.96	0.03	0.02	0.04	0.97	1.46	49.2%	2.0%	1.05	0.02	0.02	0.03	0.51	0.87	53.3%	44.5%						
102	20	148	10	2.06	0.04	0.01	0.01	0.77	1.50	37.5%	0.7%	1.10	0.03	0.01	0.01	0.26	0.86	53.1%	41.6%						
103	21	149	10	1.90	0.03	0.02	0.02	0.99	1.23	39.8%	4.3%	0.79	0.03	0.01	0.01	0.40	0.76	51.3%	33.2%						
104	22	150	10	1.70	0.02	0.05	0.06	0.68	1.06	39.8%	3.3%	0.68	0.02	0.05	0.05	0.31	0.54	40.0%	32.1%						
105	28	156	10	1.56	0.03	0.04	0.07	0.73	1.27	47.7%	4.2%	0.71	0.02	0.04	0.05	0.36	0.66	45.6%	42.3%						
106	29	157	10	1.26	0.04	0.02	0.02	0.91	1.55	40.0%	0.8%	1.22	0.03	0.02	0.01	0.45	0.95	53.8%	42.1%						
107	35	158	0	2.47	0.01	0.00	0.08	0.85	1.05	35.8%	0.2%	0.74	0.02	0.01	0.01	0.35	0.58	52.5%	35.9%						
108	31	159	10	1.71	0.03	0.04	0.08	0.84	1.08	48.9%	0.8%	0.77	0.03	0.03	0.07	0.40	0.51	45.5%	29.6%						

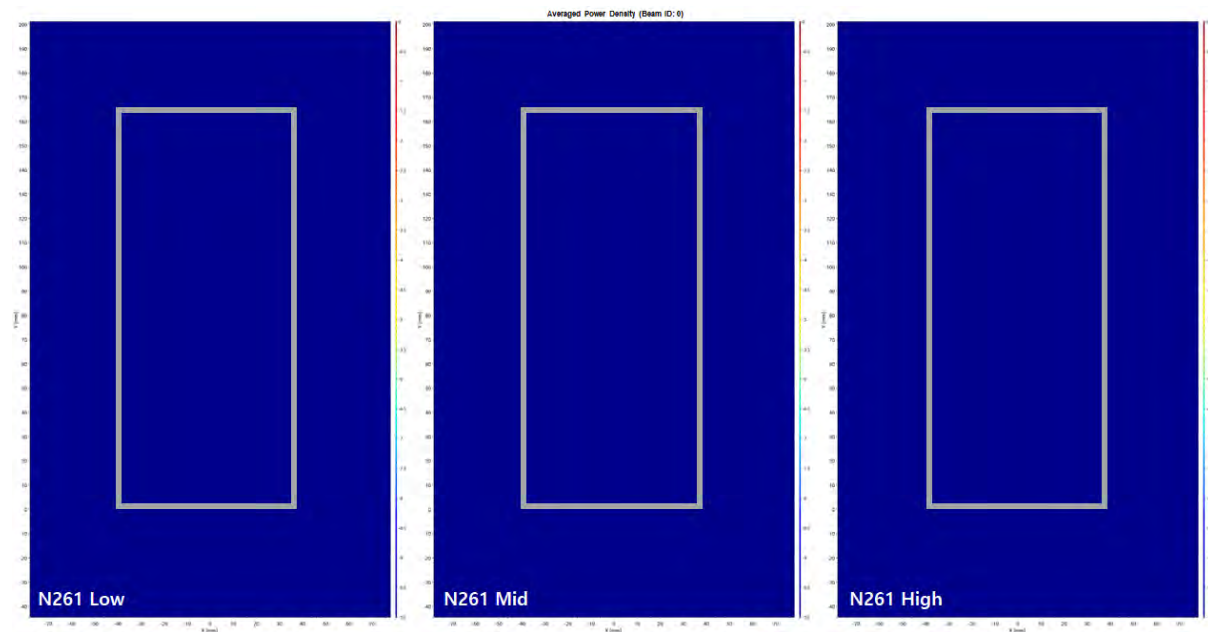
Appendix A – Simulated PD Distributions for Ant. L for simultaneous transmission analysis

This section shows the 4cm^2 10 PD simulation plots with 10 dB contour for each beam IDs, channels of Ant. L (Back /Front surfaces). These figures are normalized to peak 4cm^2 PD values of each beam ID. For the front surface, if the ratio of (2mm front PD)/(2mm worst surface PD) below 10%, then nothing will be shown in the PD distribution.

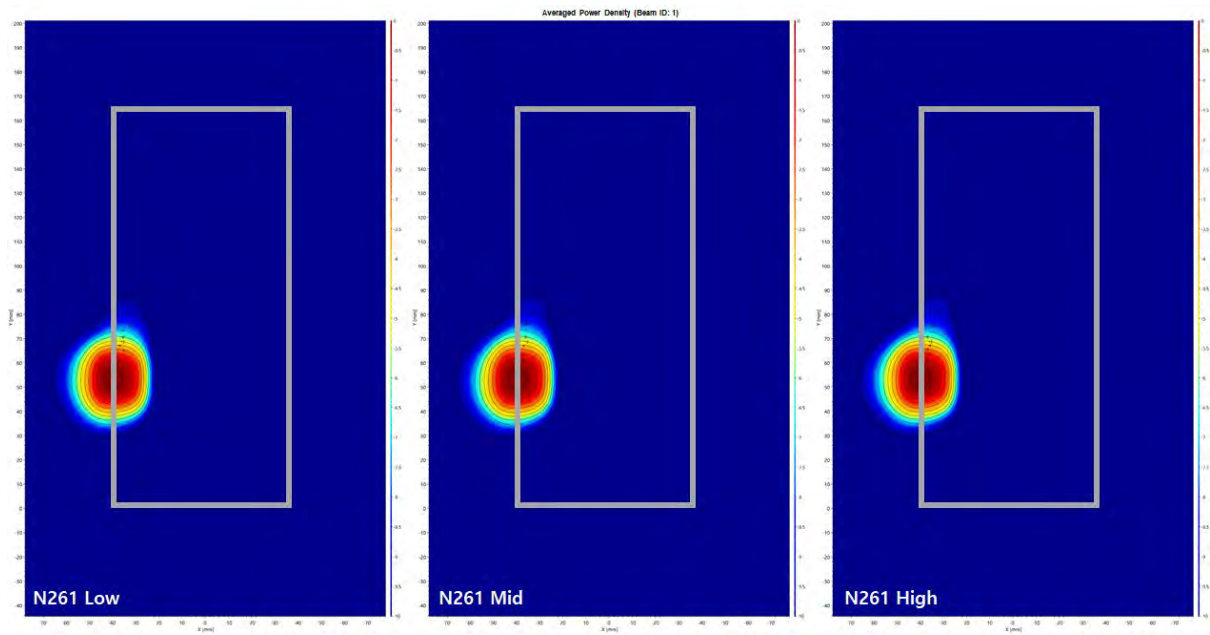
- n261 / Beam ID: 0 / Back surface



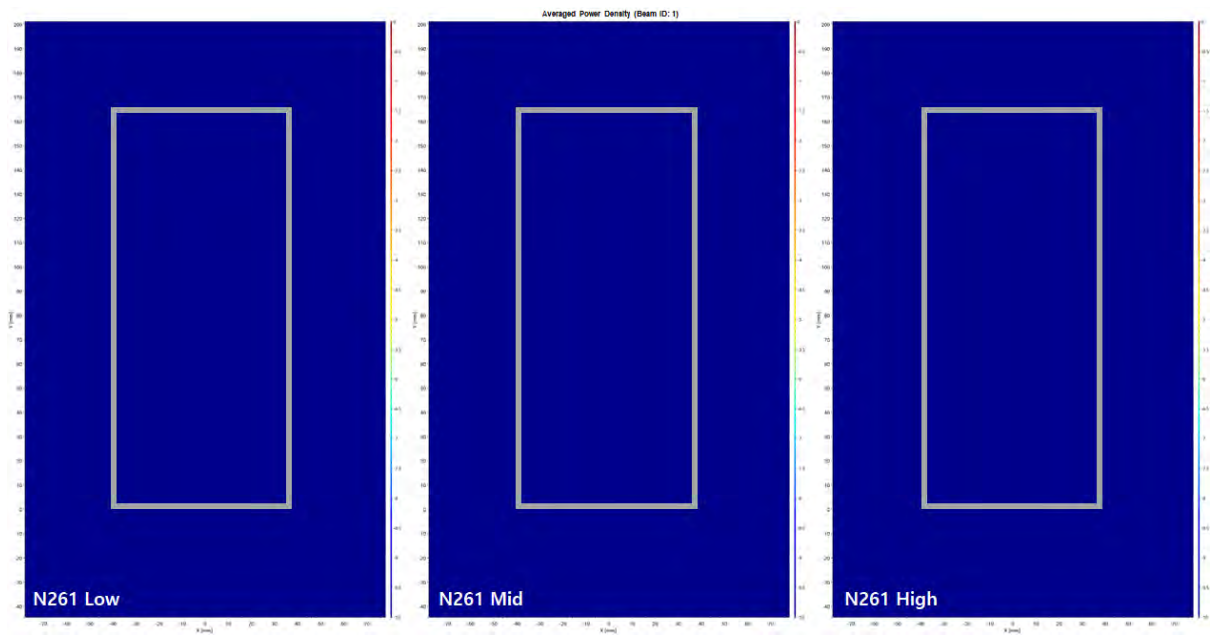
- n261 / Beam ID: 0 / Front surface



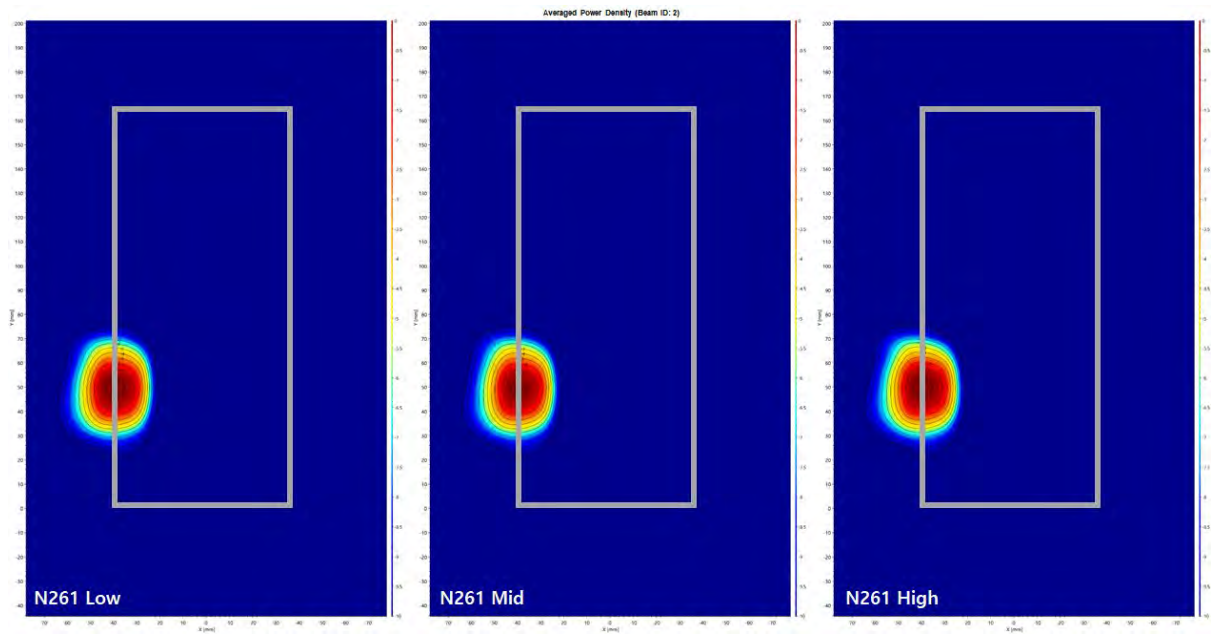
- n261 / Beam ID: 1 / Back surface



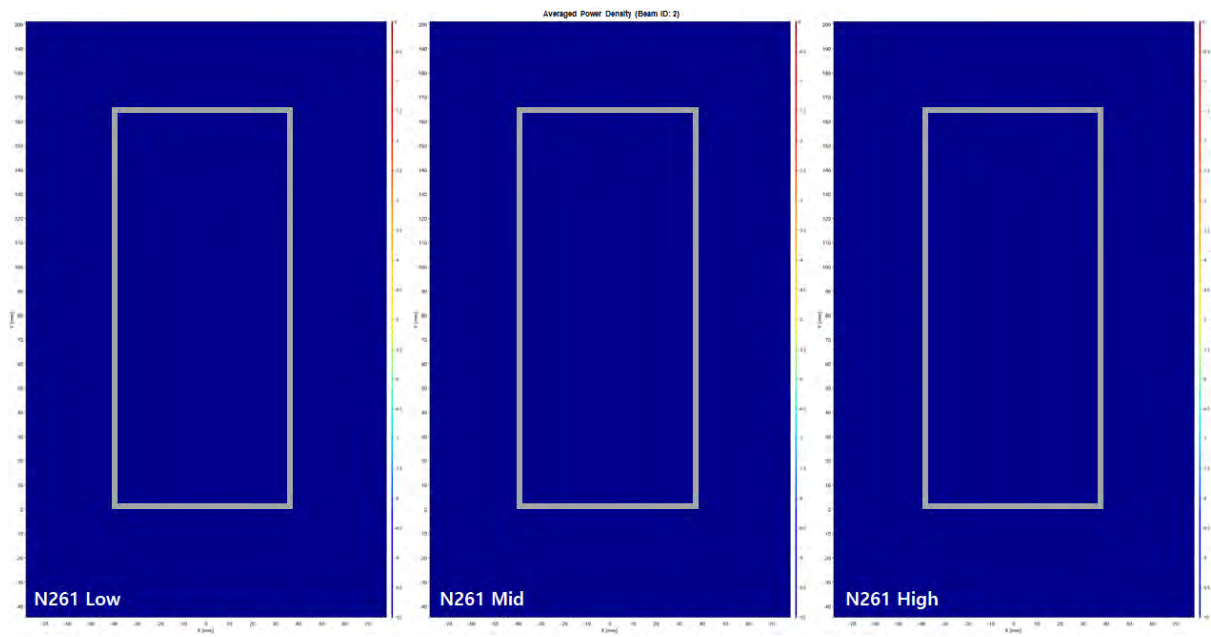
- n261 / Beam ID: 1 / Front surface



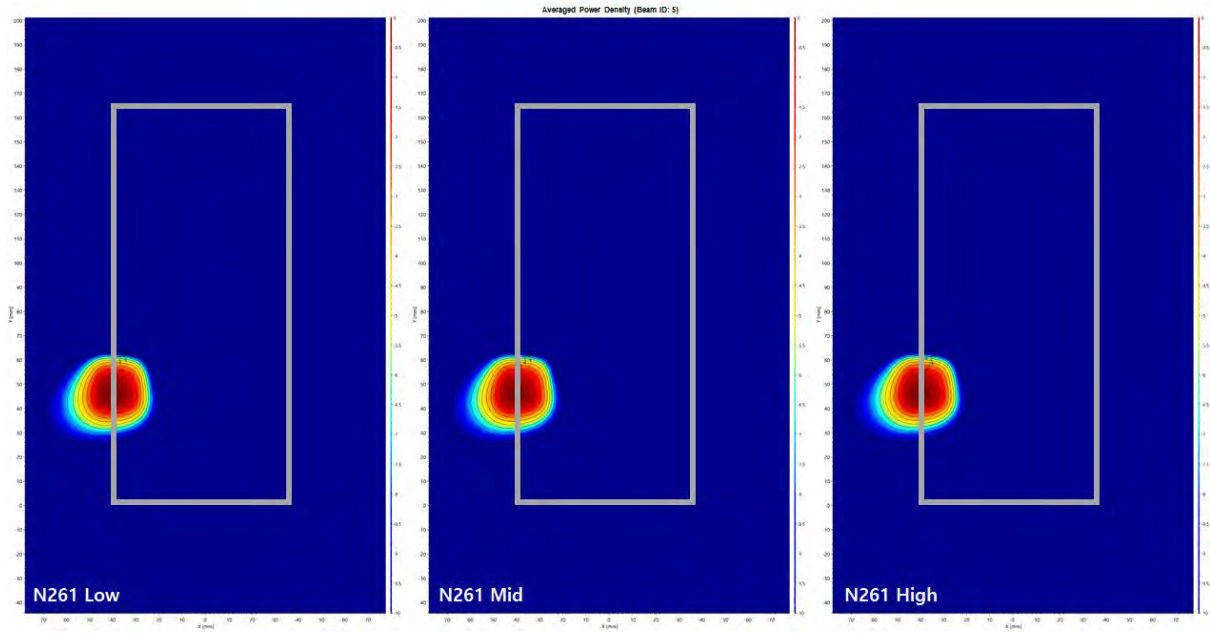
- n261 / Beam ID: 2 / Back surface



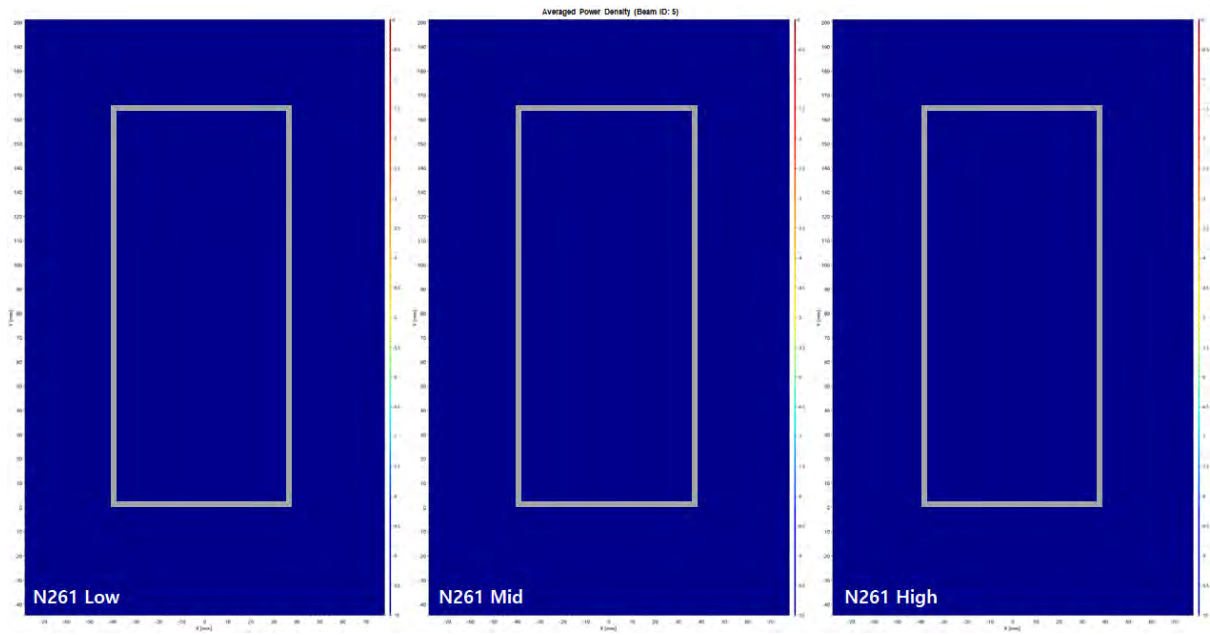
- n261 / Beam ID: 2 / Front surface



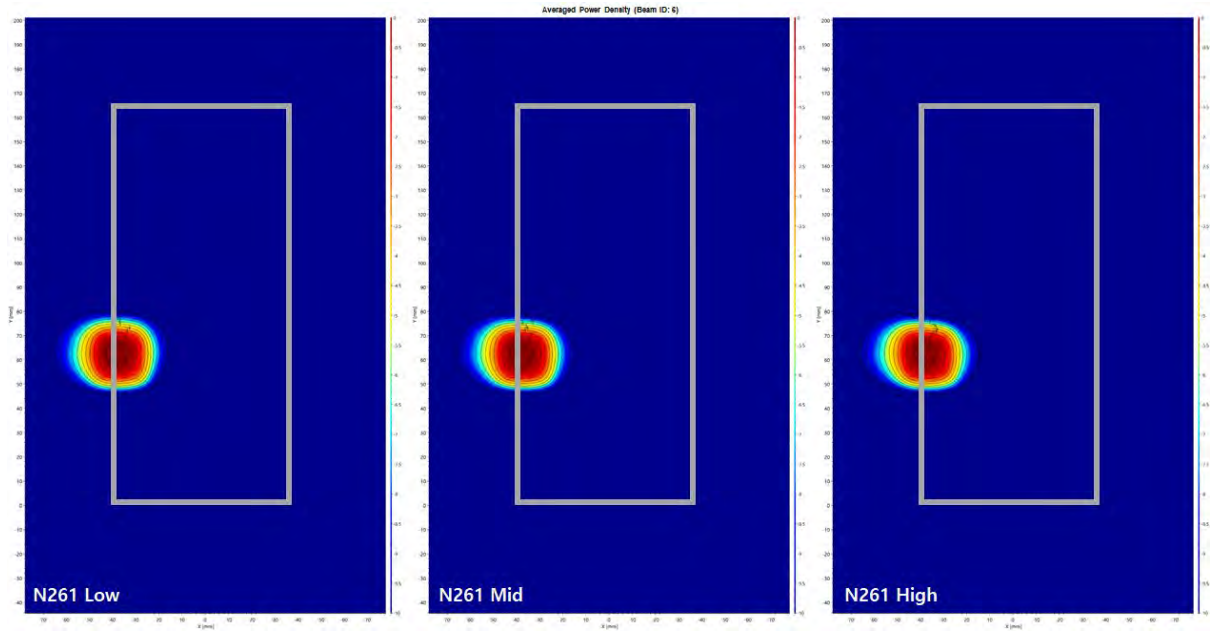
- n261 / Beam ID: 5 / Back surface



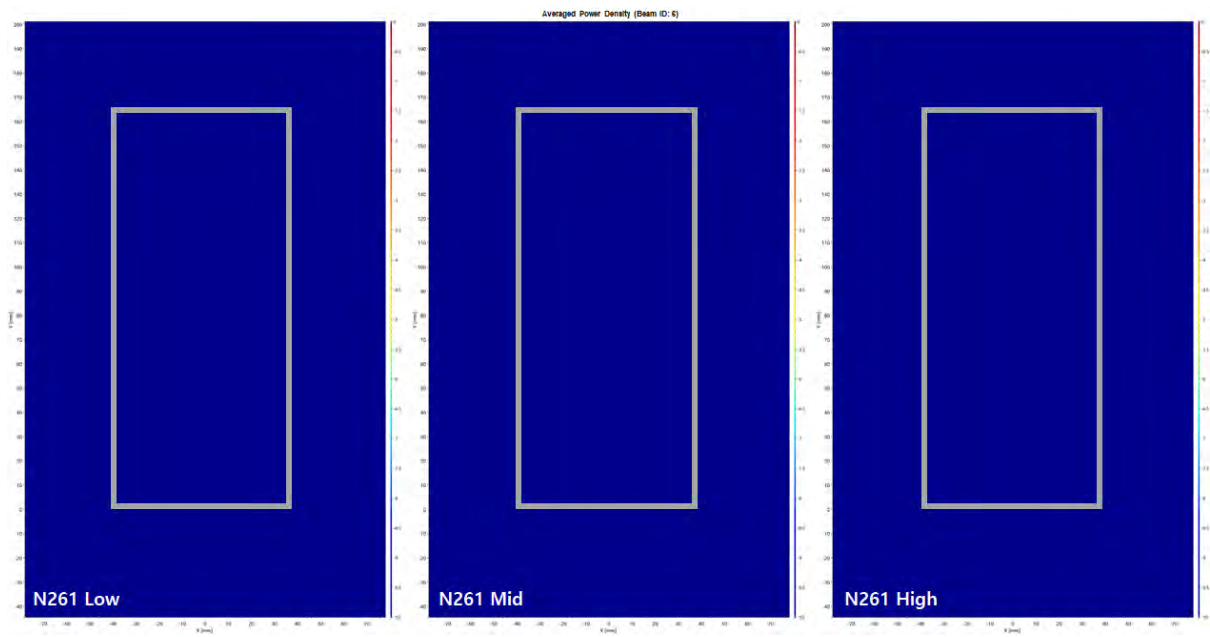
- n261 / Beam ID: 5 / Front surface



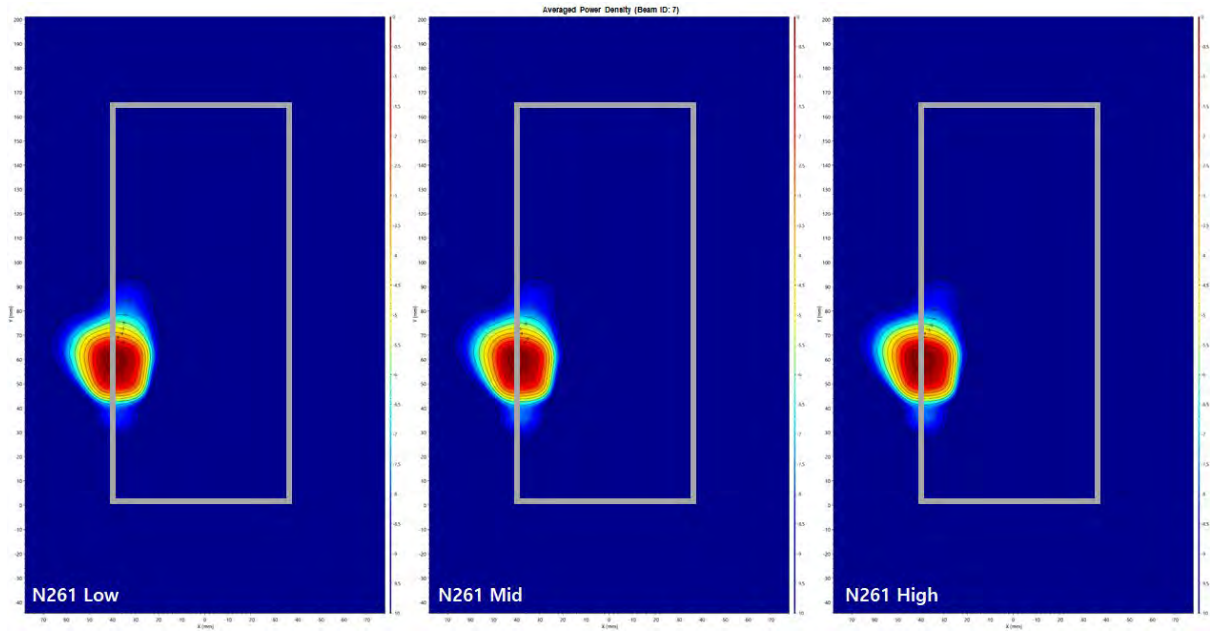
- n261 / Beam ID: 6 / Back surface



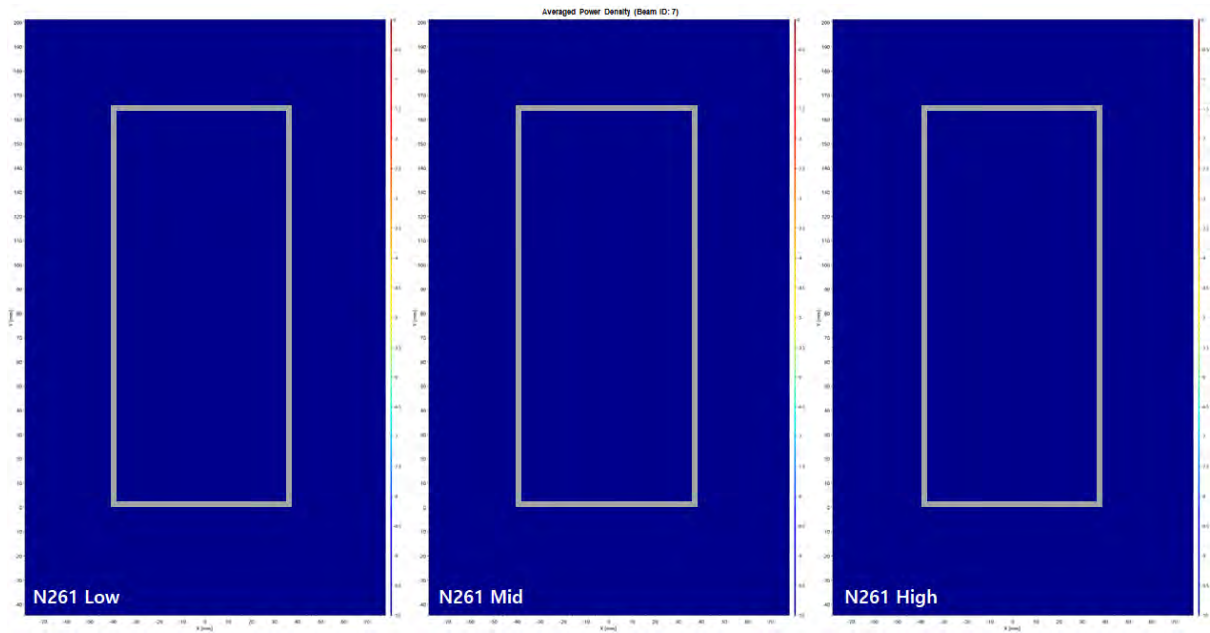
- n261 / Beam ID: 6 / Front surface



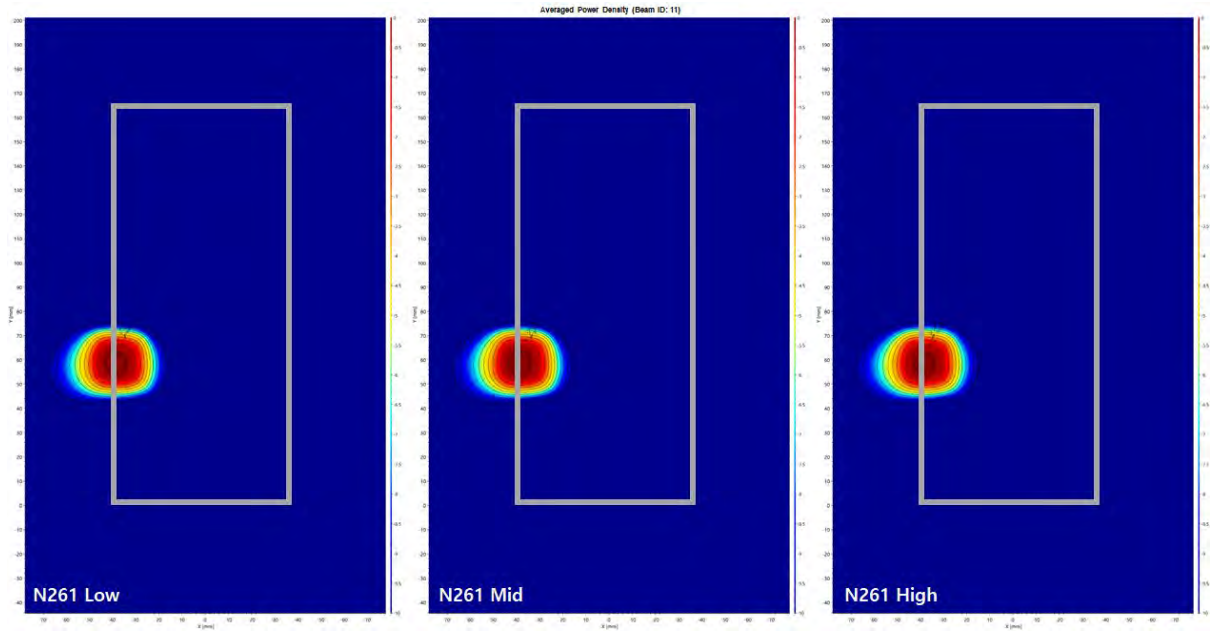
- n261 / Beam ID: 7 / Back surface



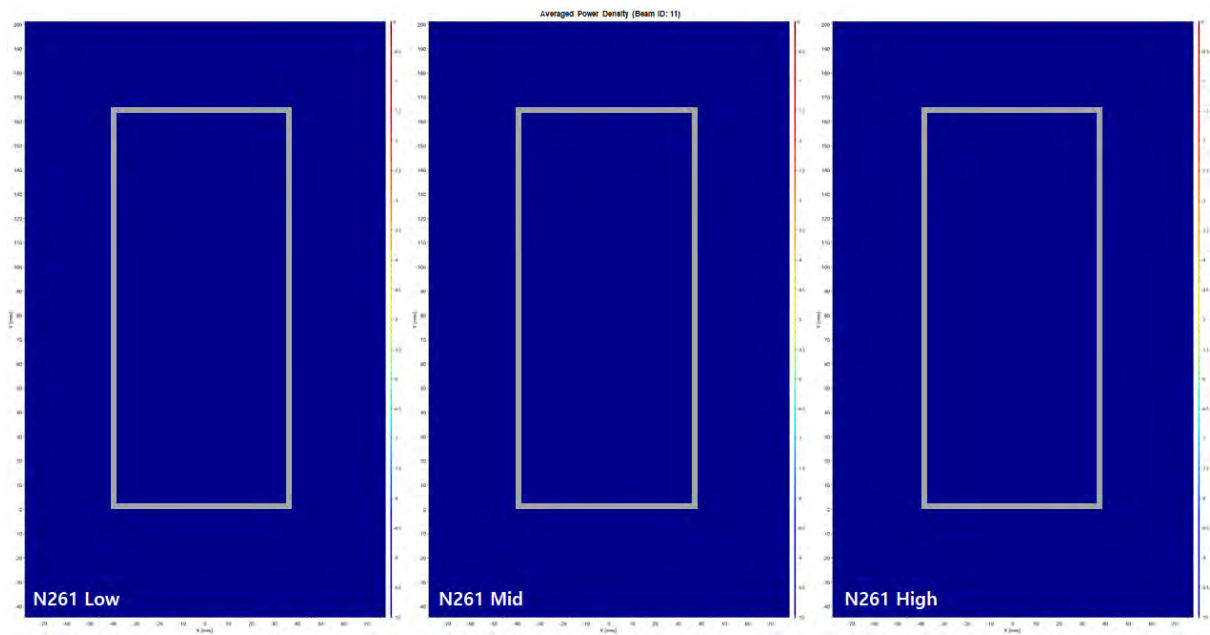
- n261 / Beam ID: 7 / Front surface



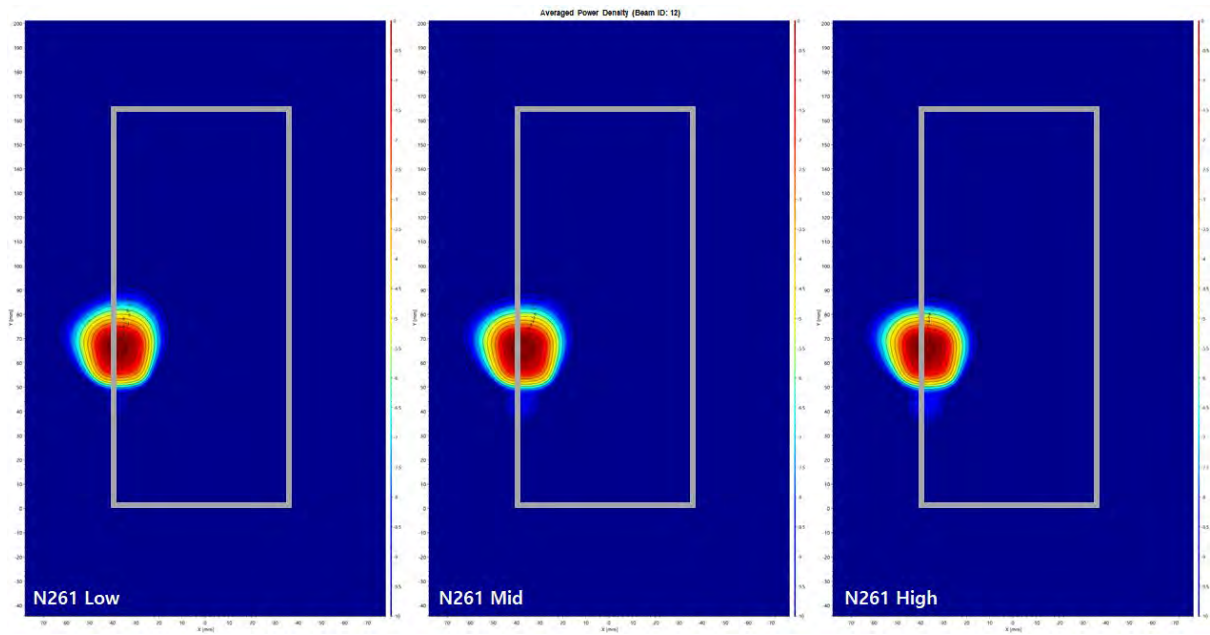
- n261 / Beam ID: 11 / Back surface



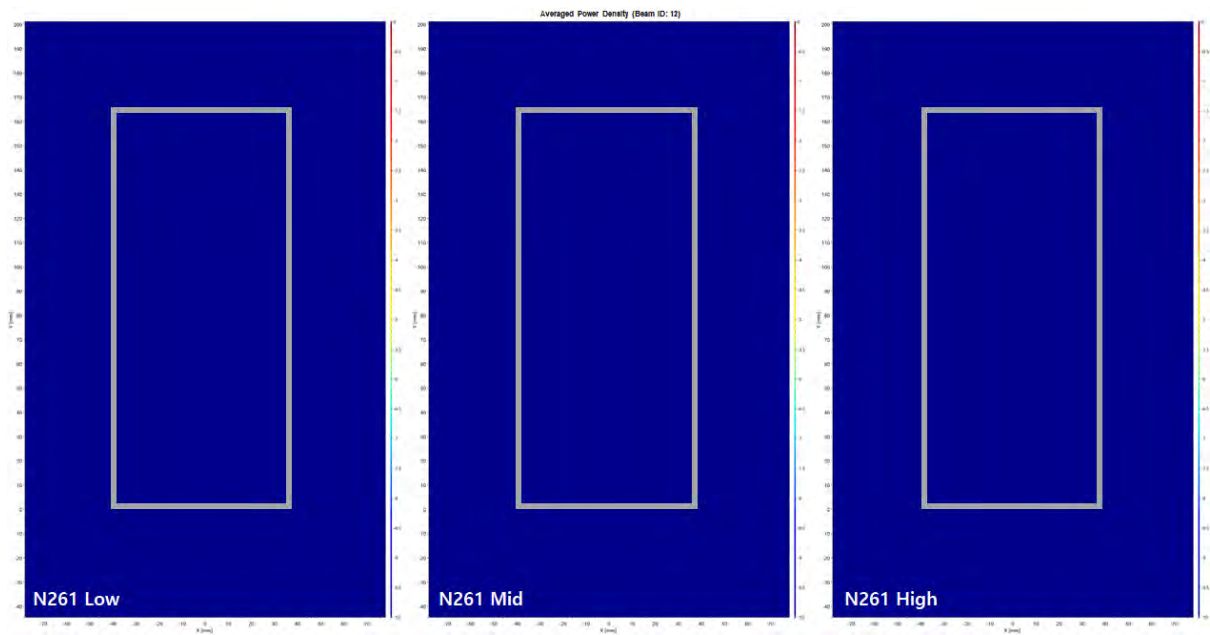
- n261 / Beam ID: 11 / Front surface



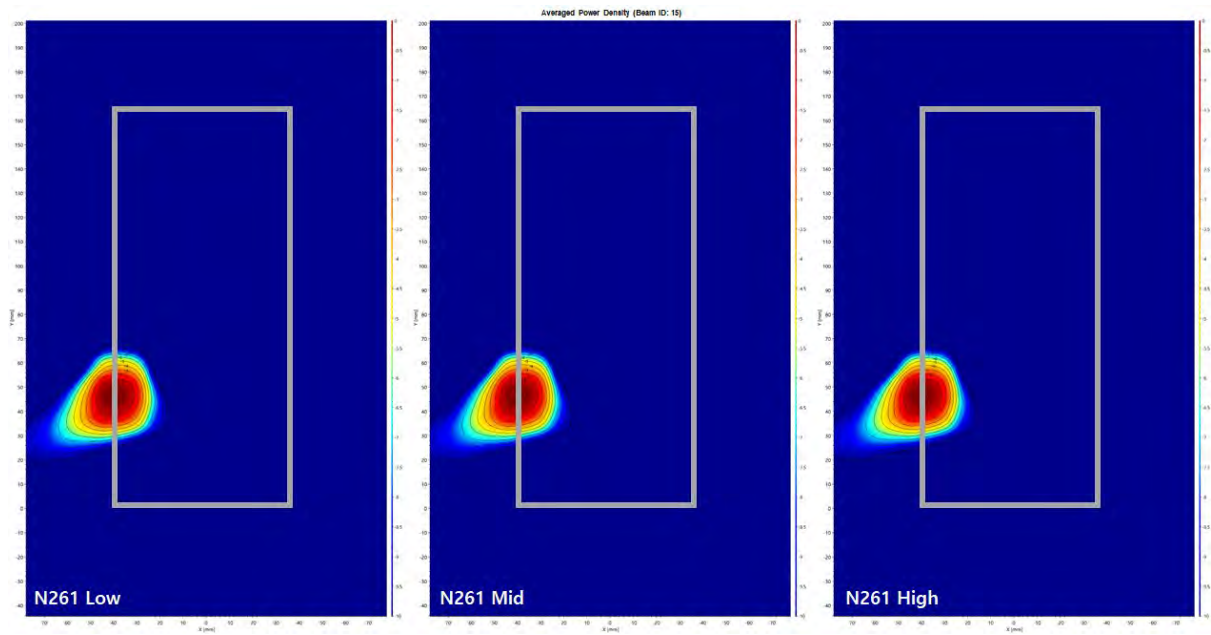
- n261 / Beam ID: 12 / Back surface



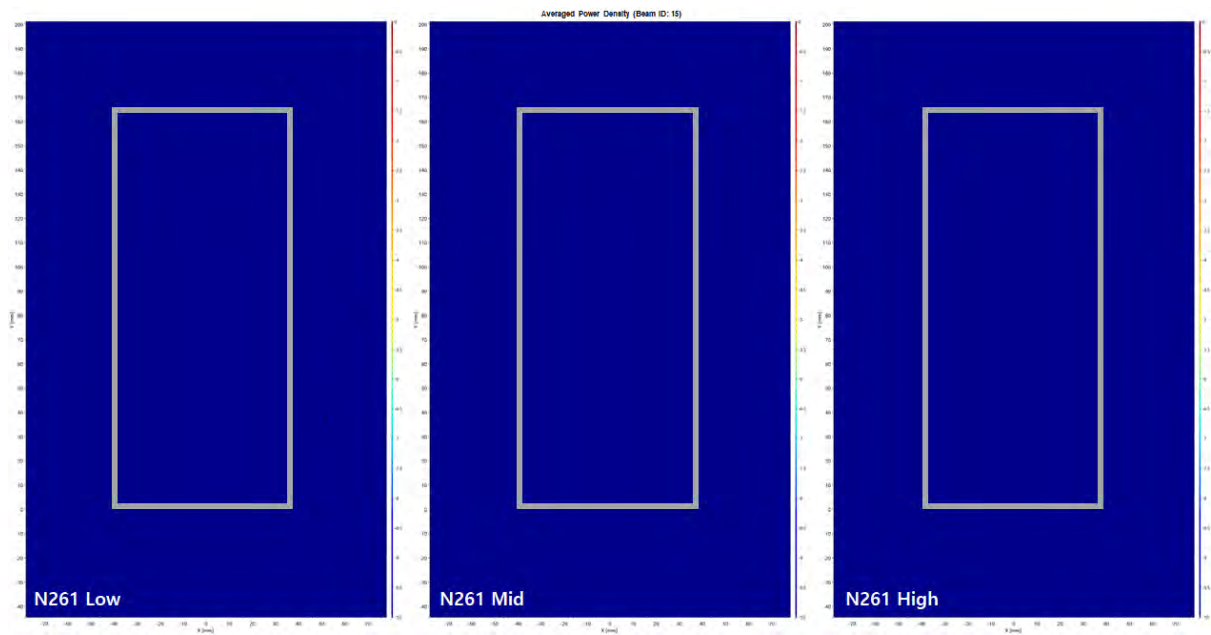
- n261 / Beam ID: 12 / Front surface



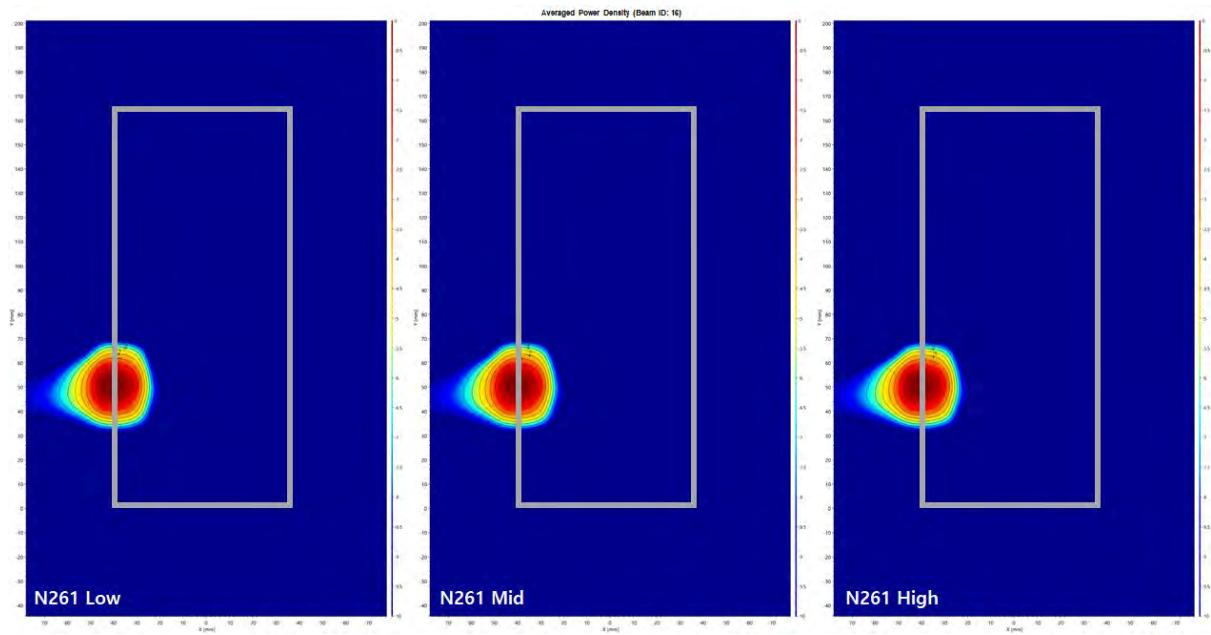
- n261 / Beam ID: 15 / Back surface



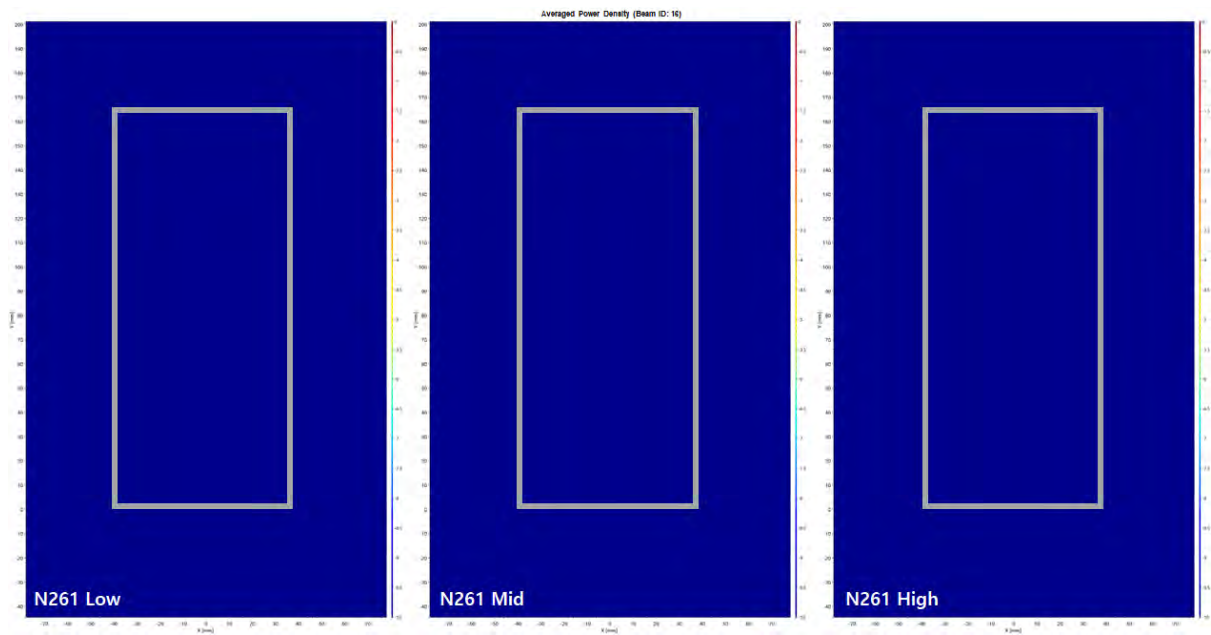
- n261 / Beam ID: 15 / Front surface



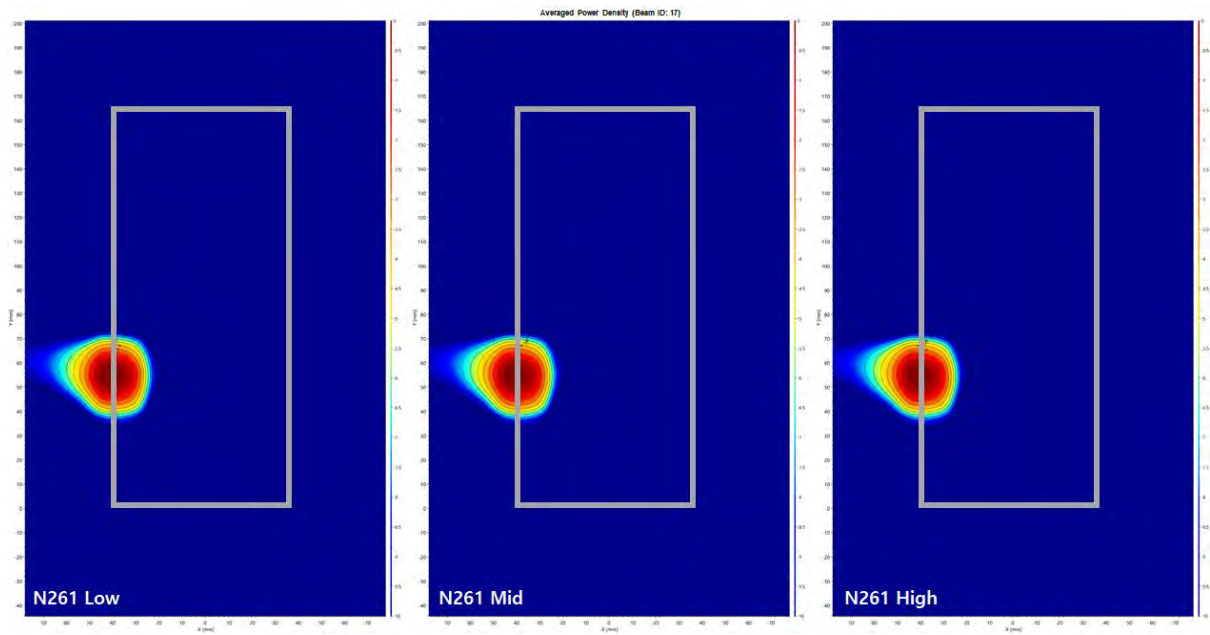
- n261 / Beam ID: 16 / Back surface



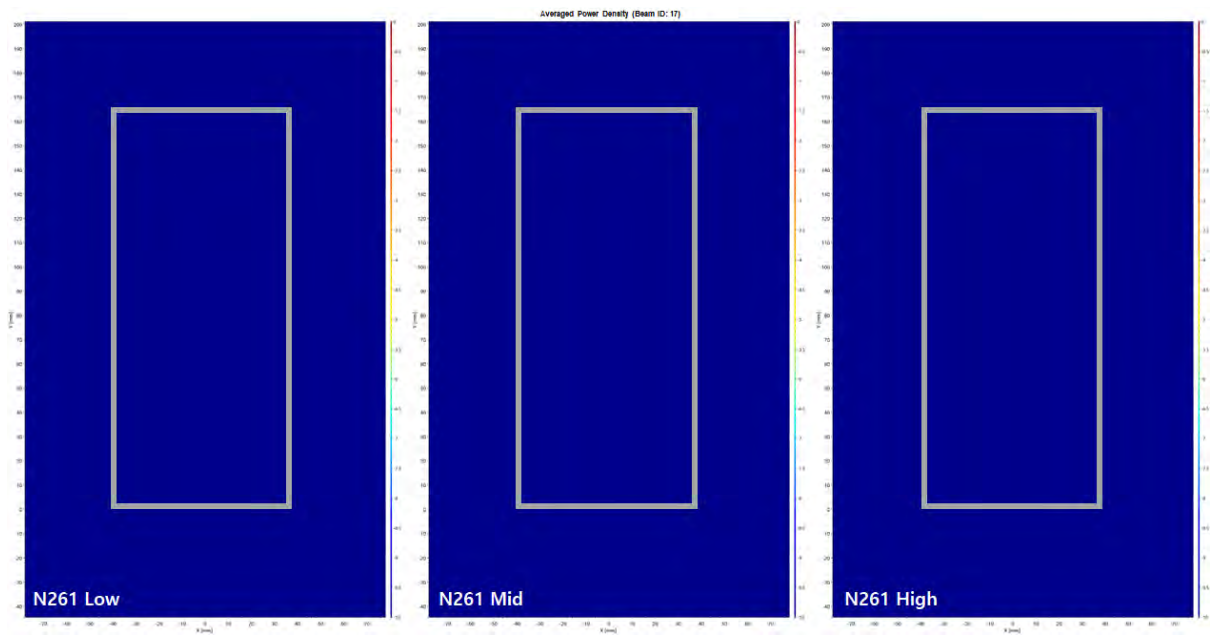
- n261 / Beam ID: 16 / Front surface



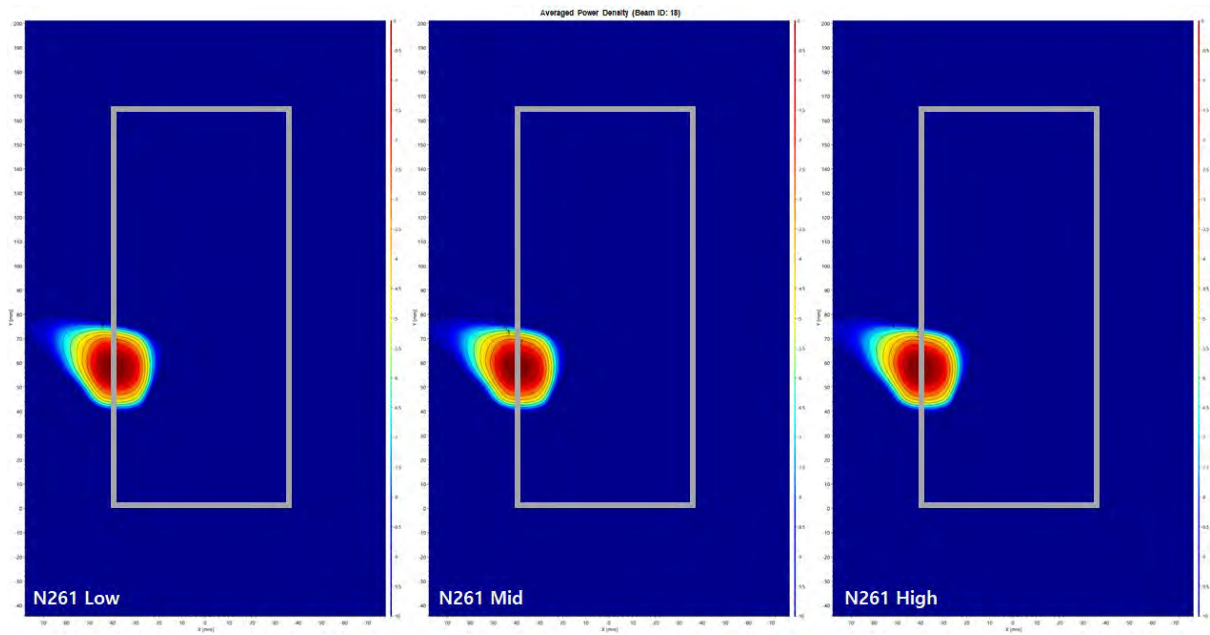
- n261 / Beam ID: 17 / Back surface



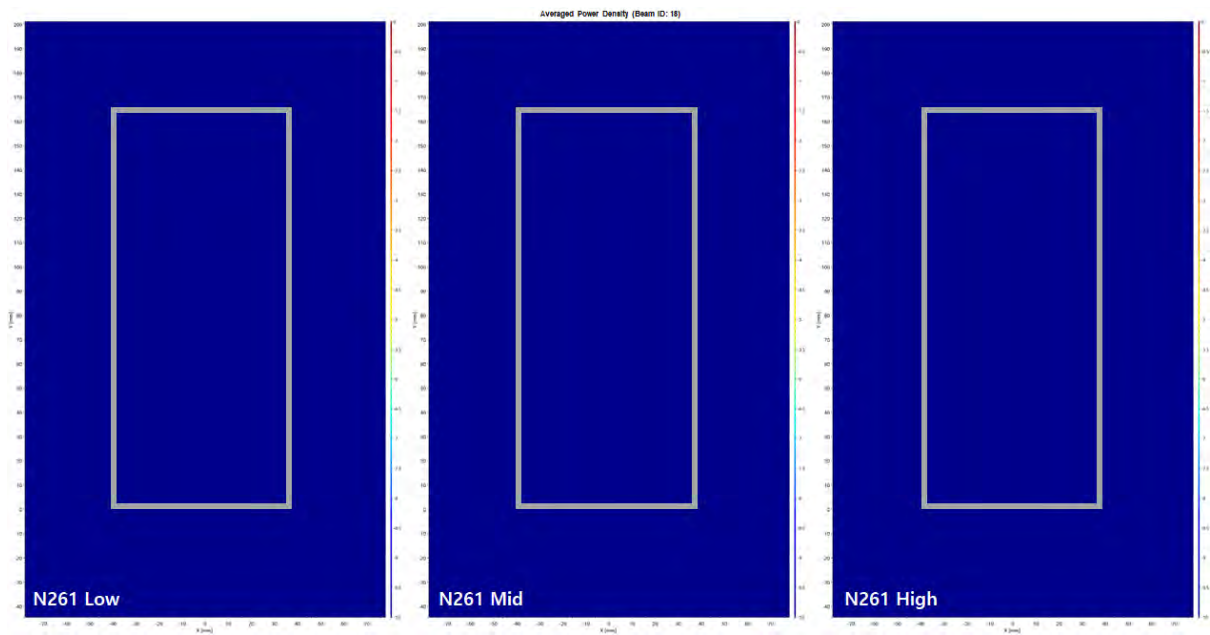
- n261 / Beam ID: 17 / Front surface



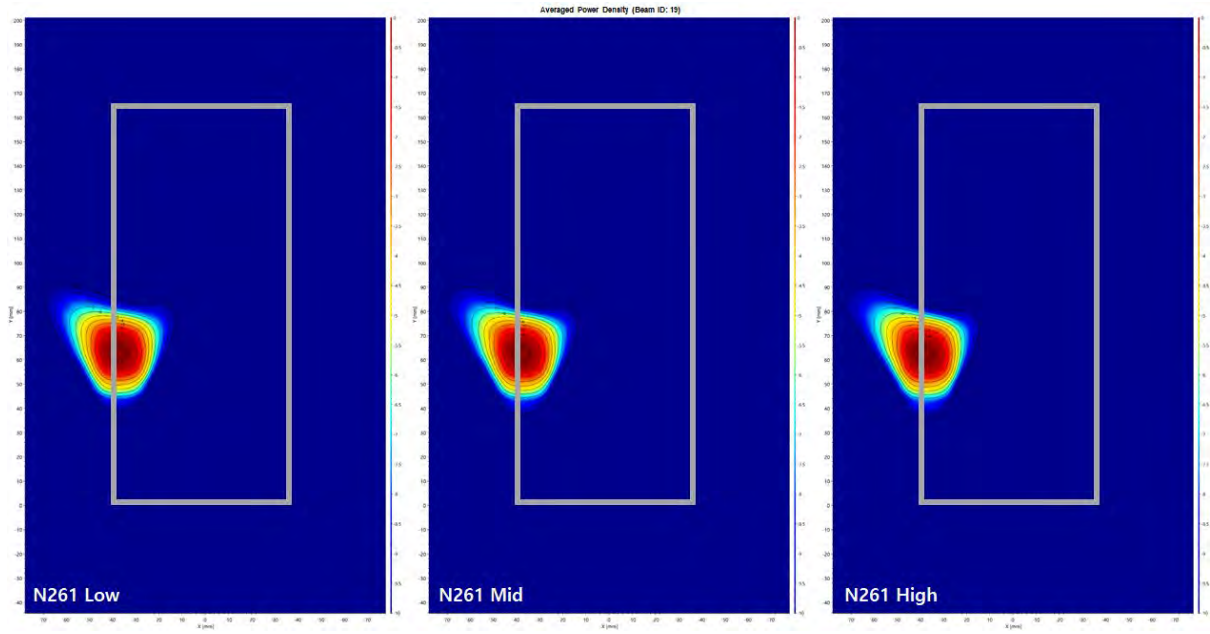
- n261 / Beam ID: 18 / Back surface



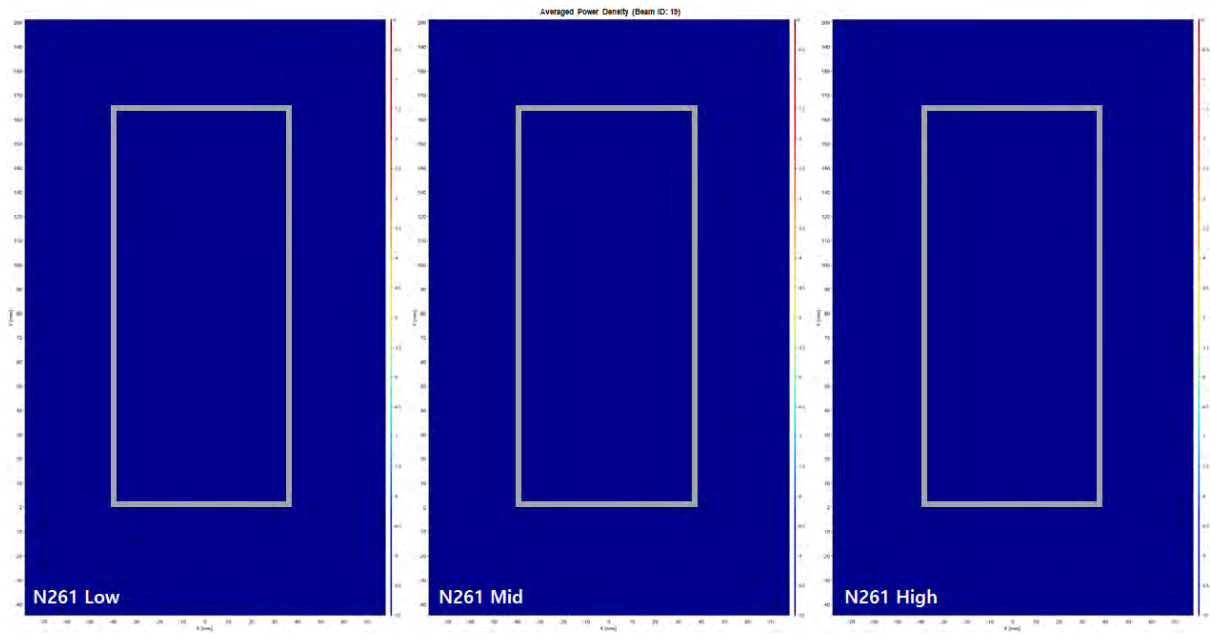
- n261 / Beam ID: 18 / Front surface



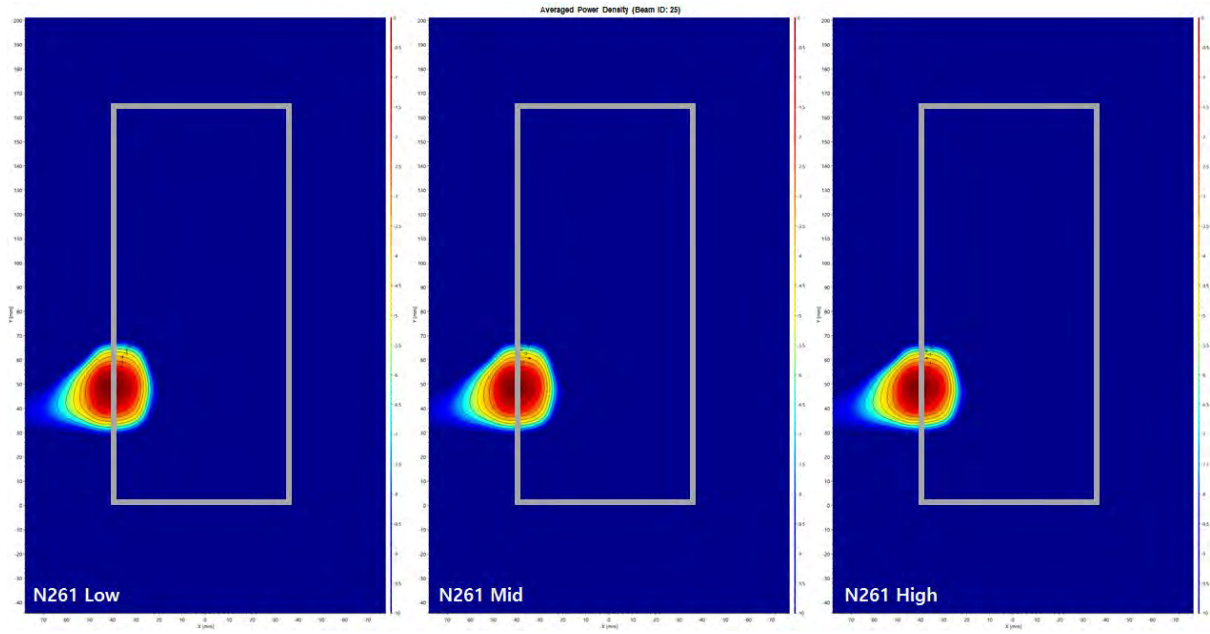
- n261 / Beam ID: 19 / Back surface



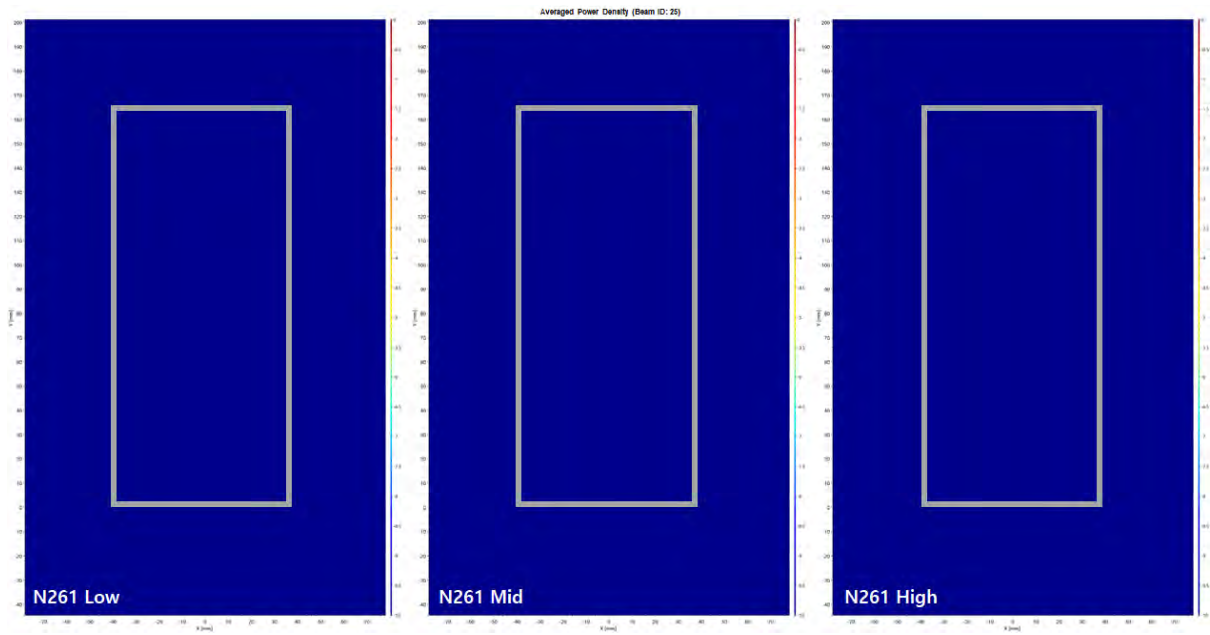
- n261 / Beam ID: 19 / Front surface



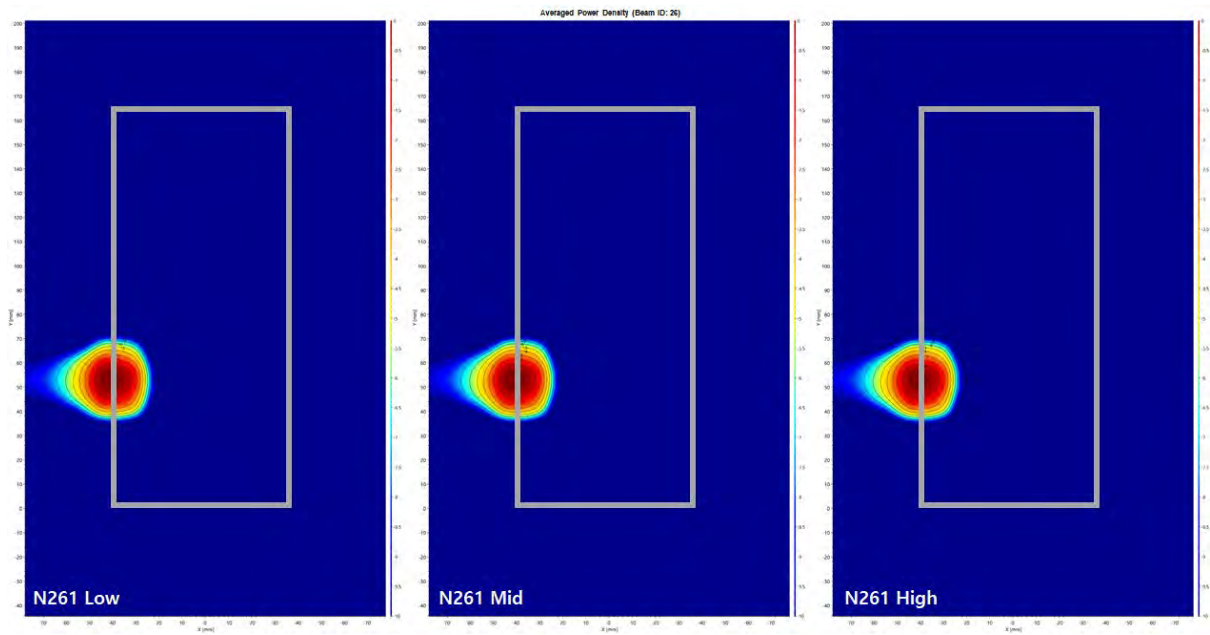
- n261 / Beam ID: 25 / Back surface



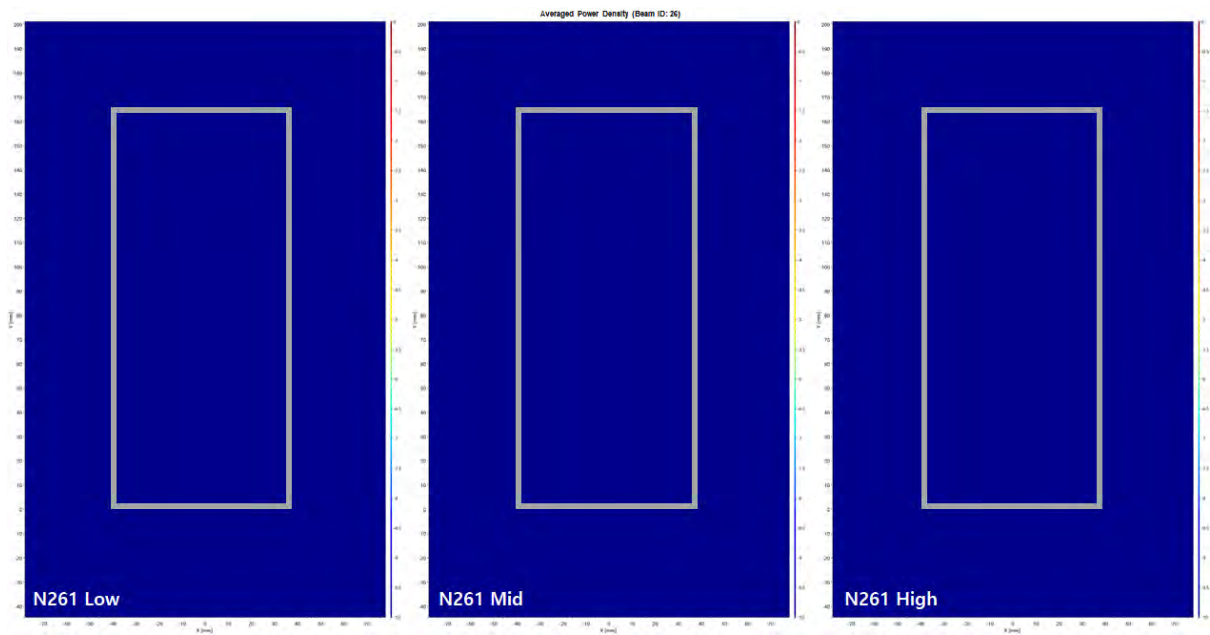
- n261 / Beam ID: 25 / Front surface



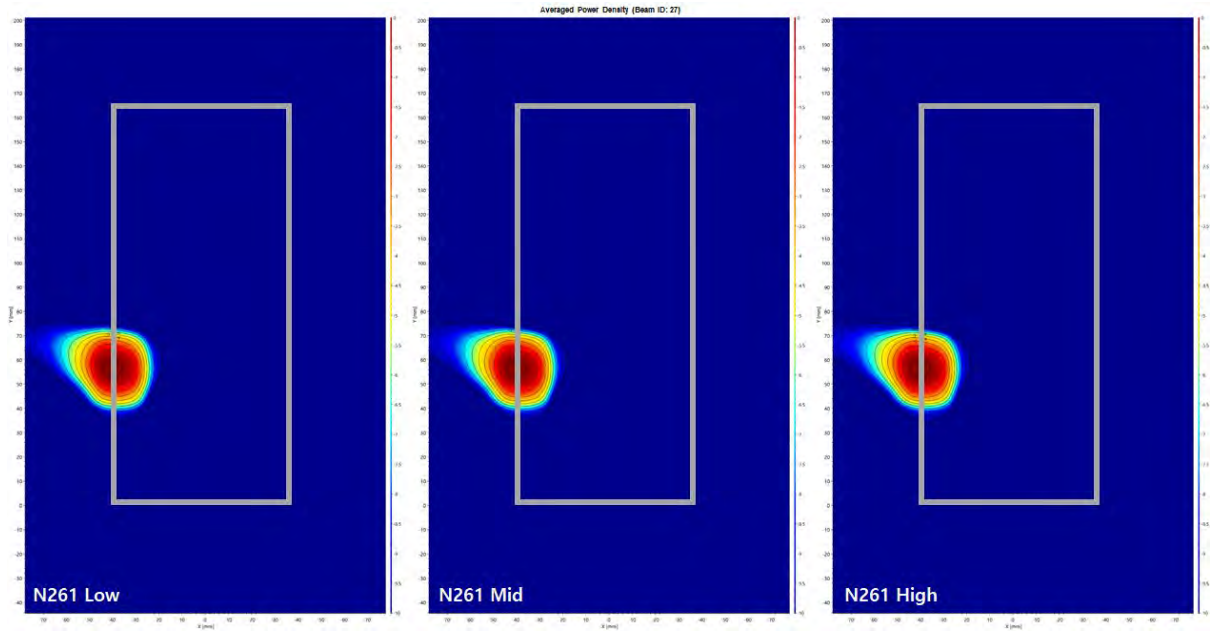
- n261 / Beam ID: 26 / Back surface



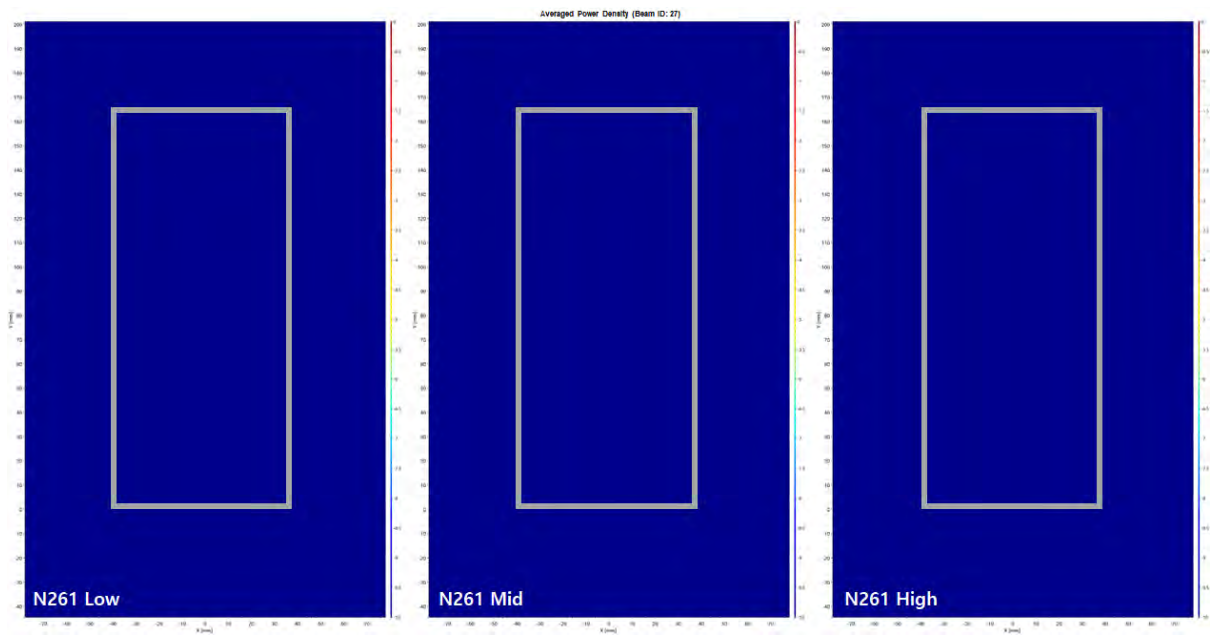
- n261 / Beam ID: 26 / Front surface



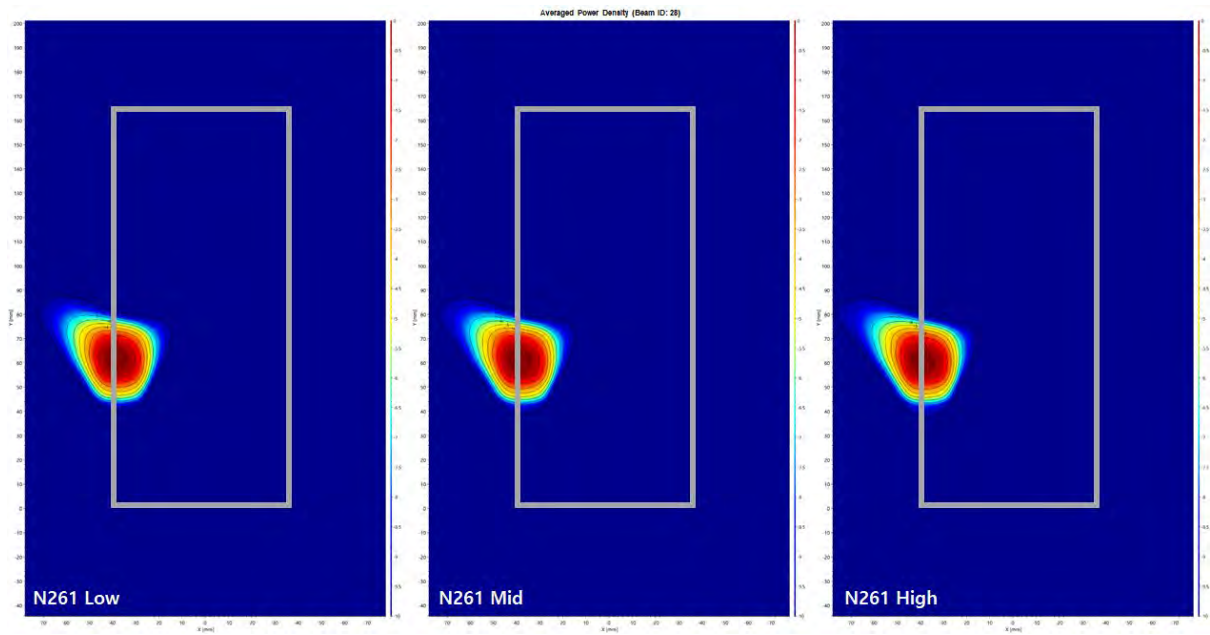
- n261 / Beam ID: 27 / Back surface



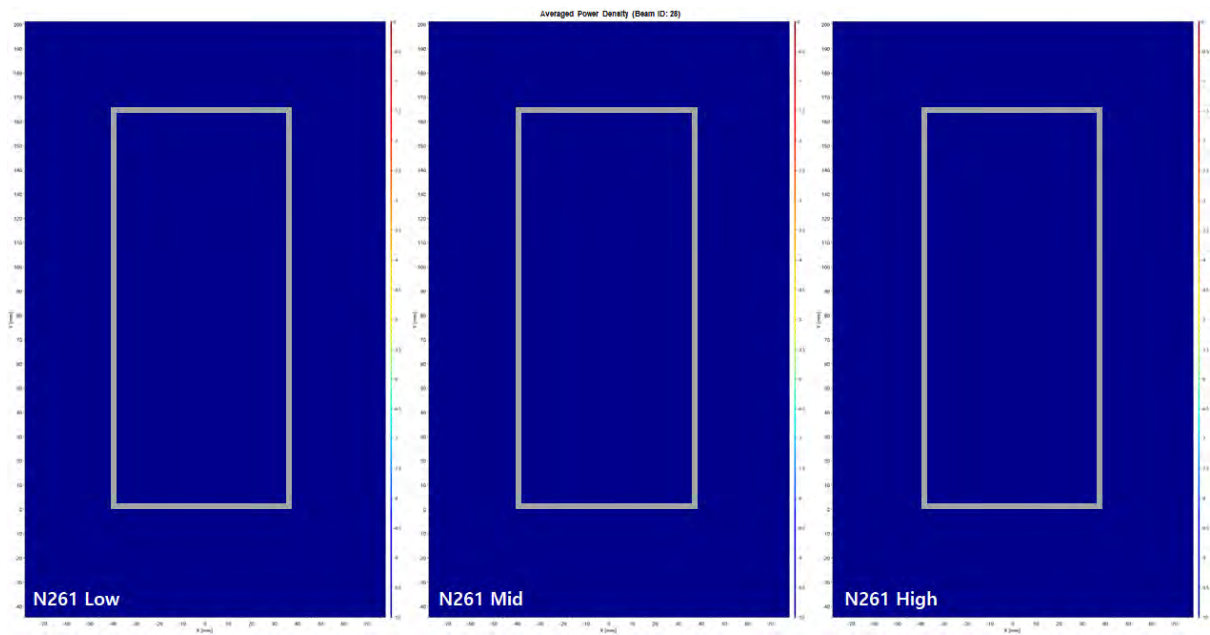
- n261 / Beam ID: 27 / Front surface



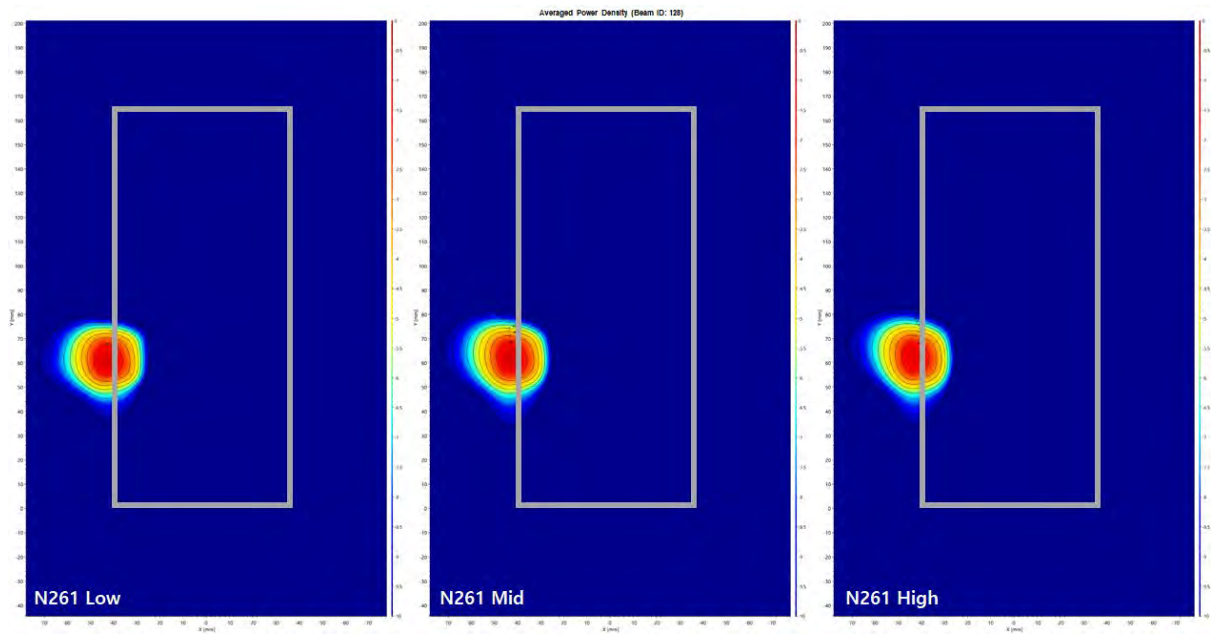
- n261 / Beam ID: 28 / Back surface



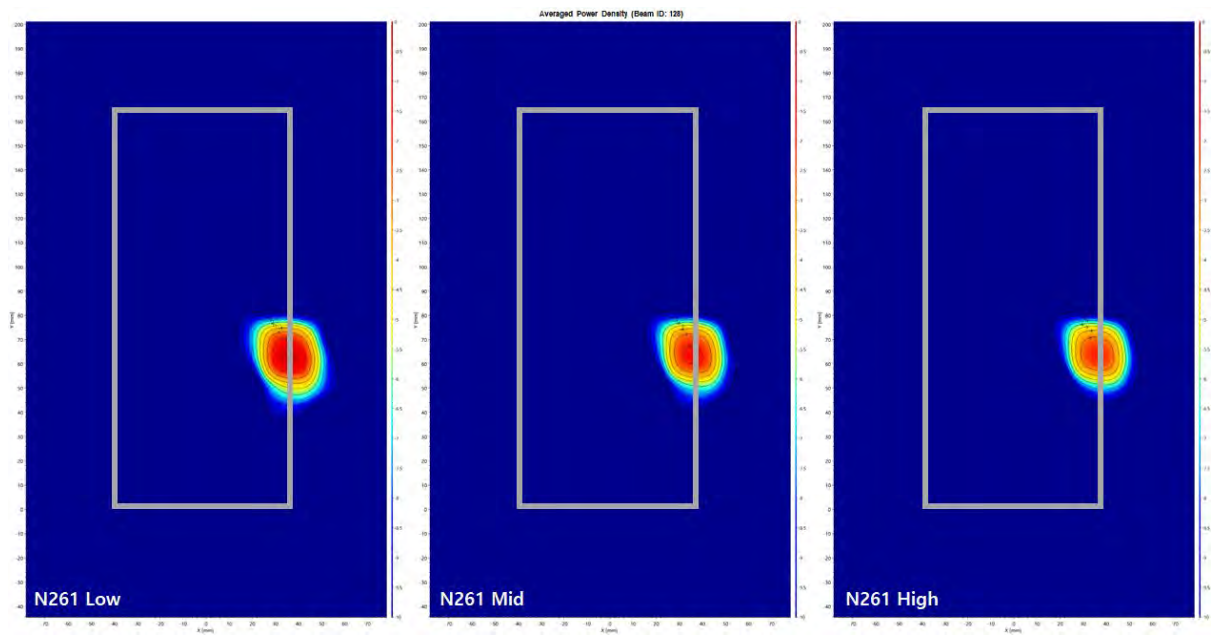
- n261 / Beam ID: 28 / Front surface



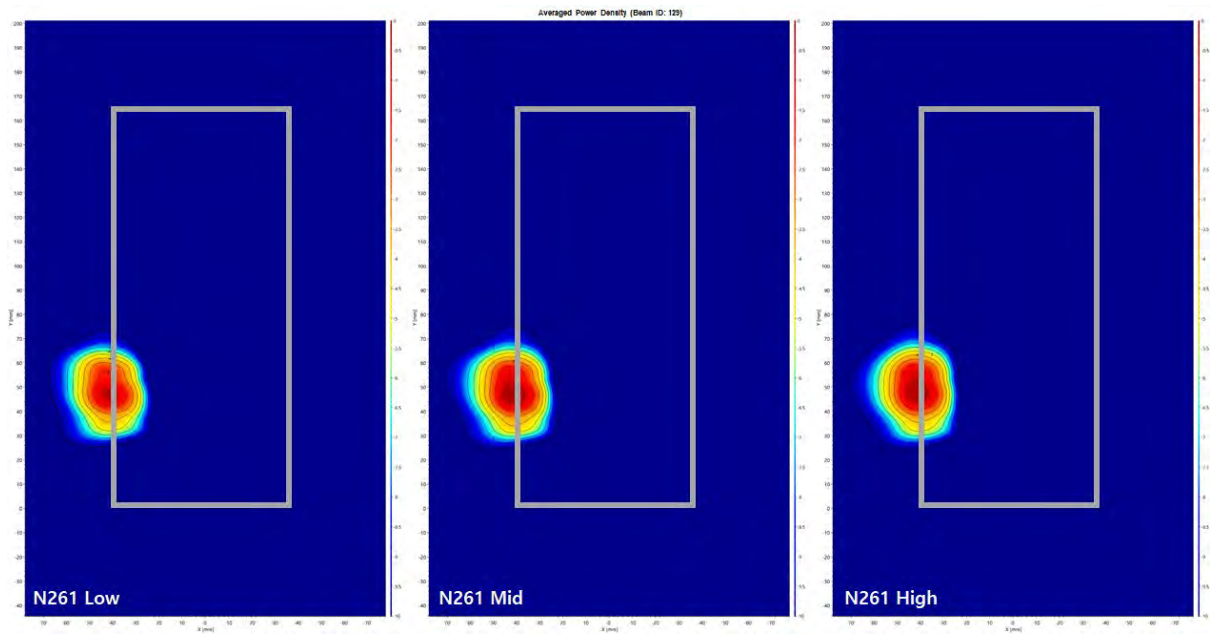
- n261 / Beam ID: 128 / Back surface



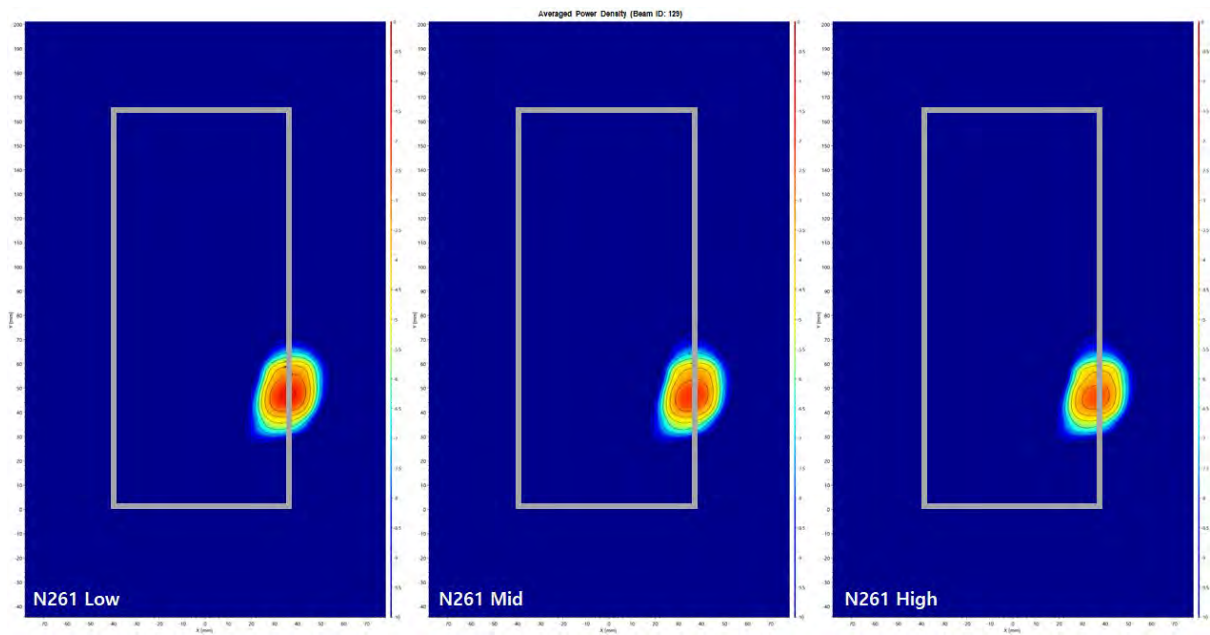
- n261 / Beam ID: 128 / Front surface



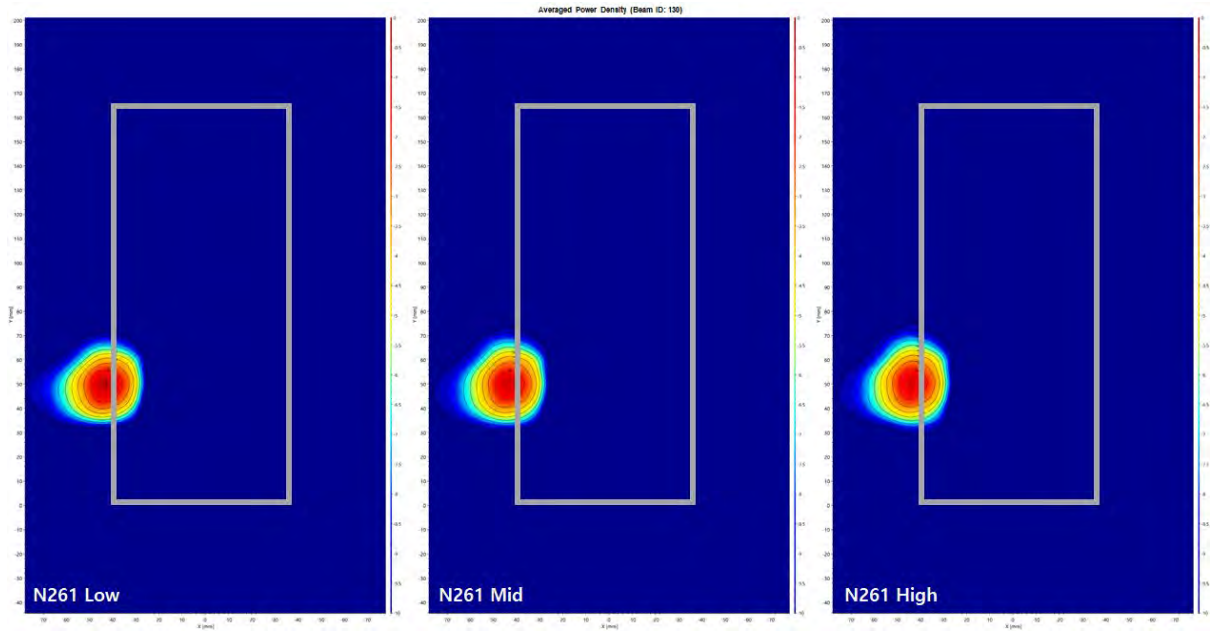
- n261 / Beam ID: 129 / Back surface



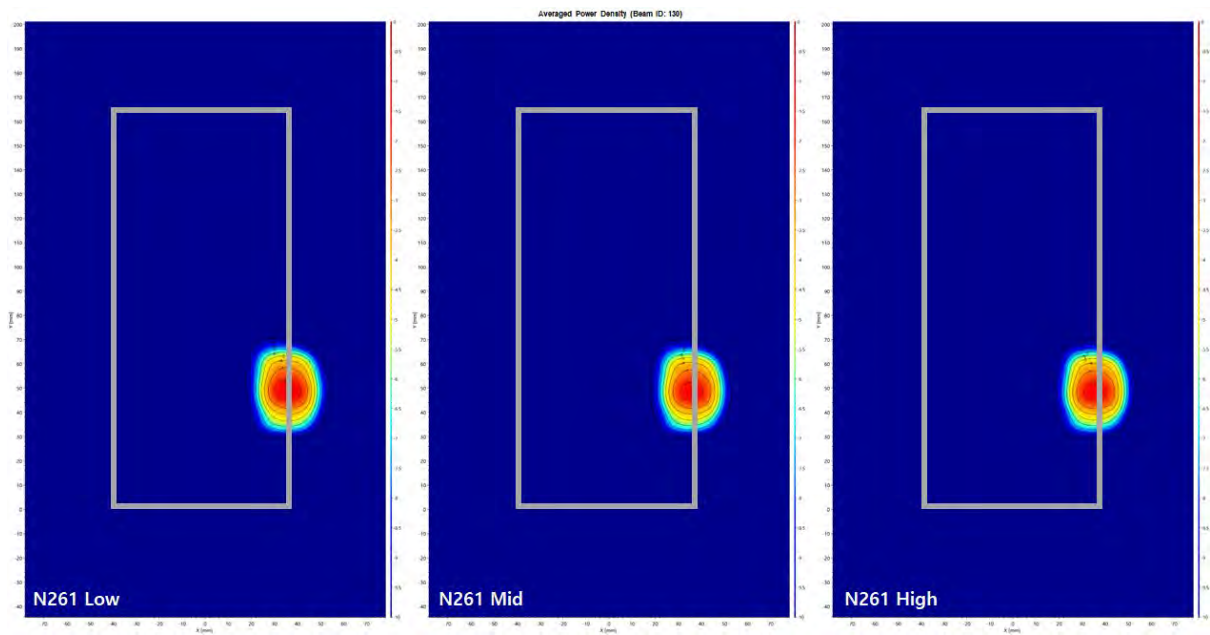
- n261 / Beam ID: 129 / Front surface



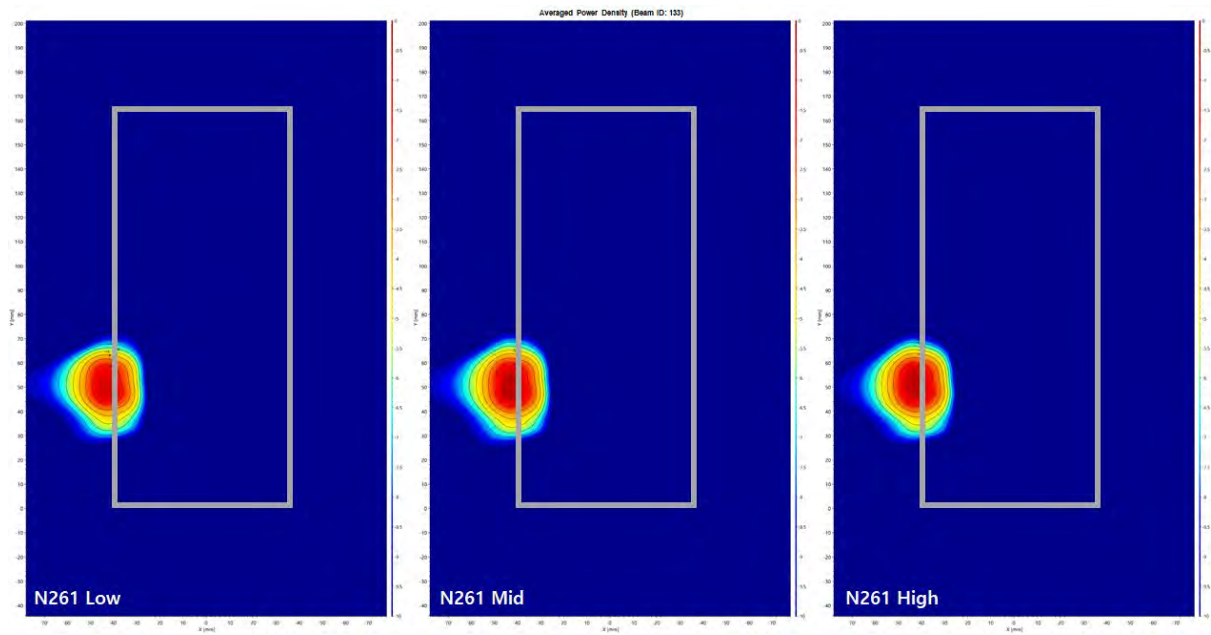
- n261 / Beam ID: 130 / Back surface



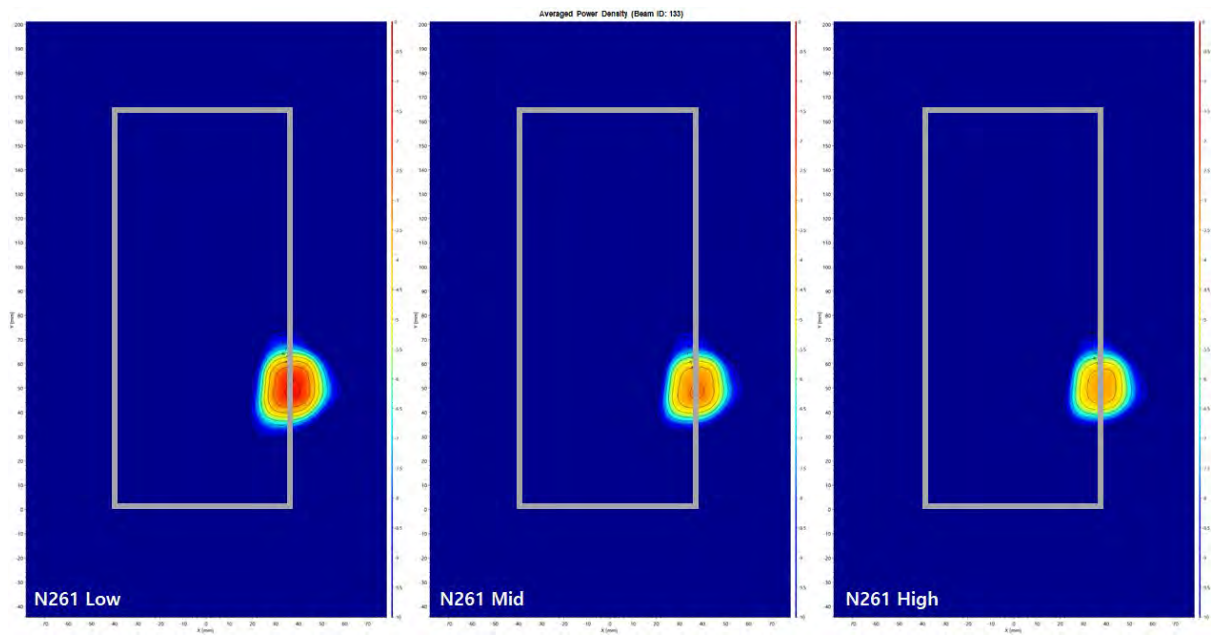
- n261 / Beam ID: 130 / Front surface



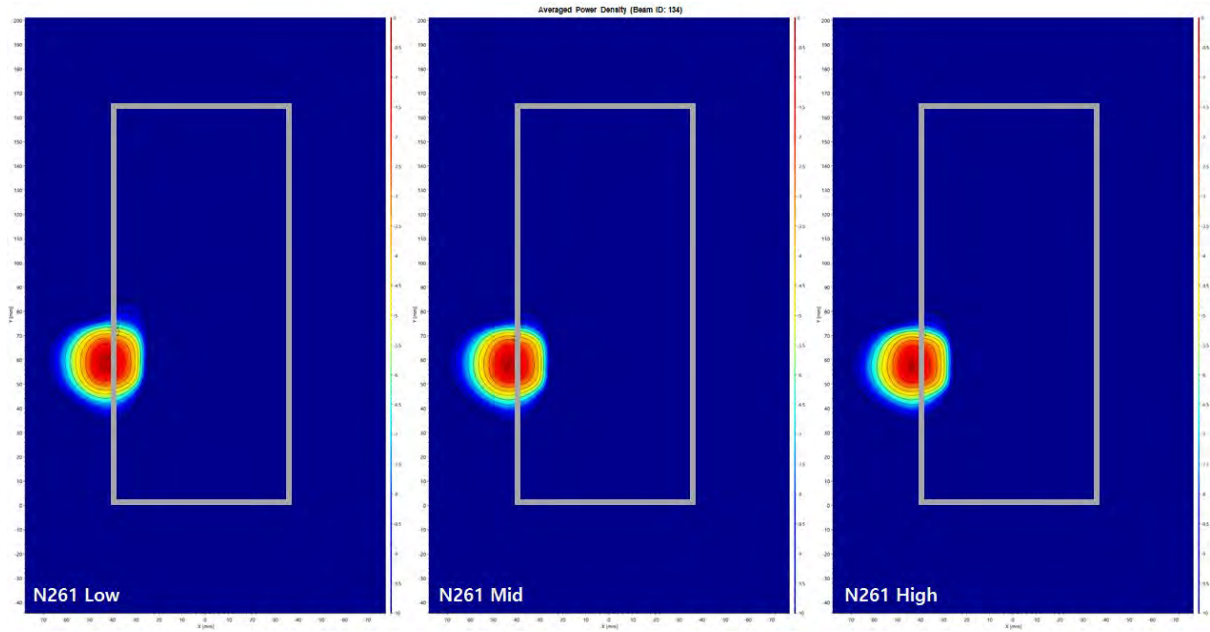
- n261 / Beam ID: 133 / Back surface



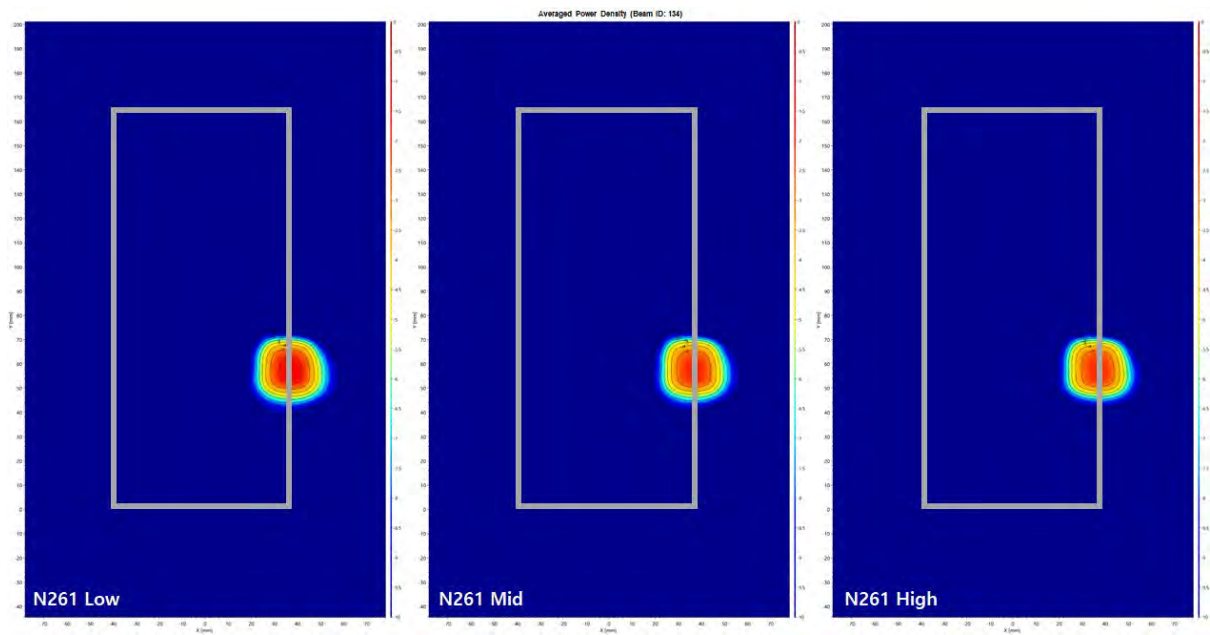
- n261 / Beam ID: 133 / Front surface



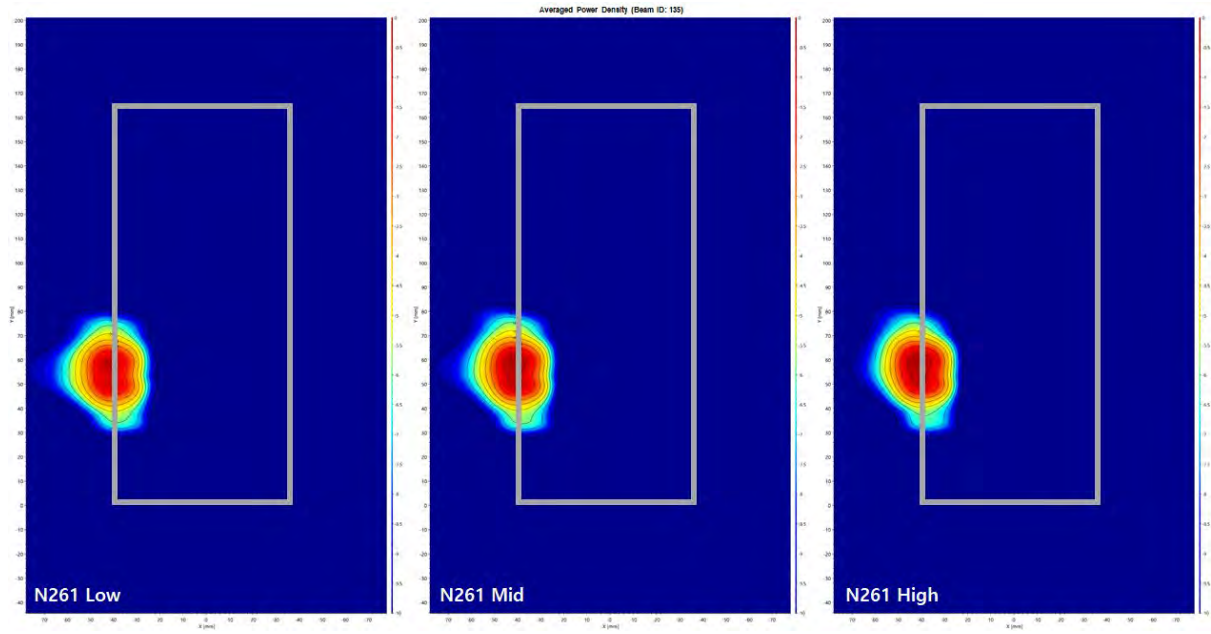
- n261 / Beam ID: 134 / Back surface



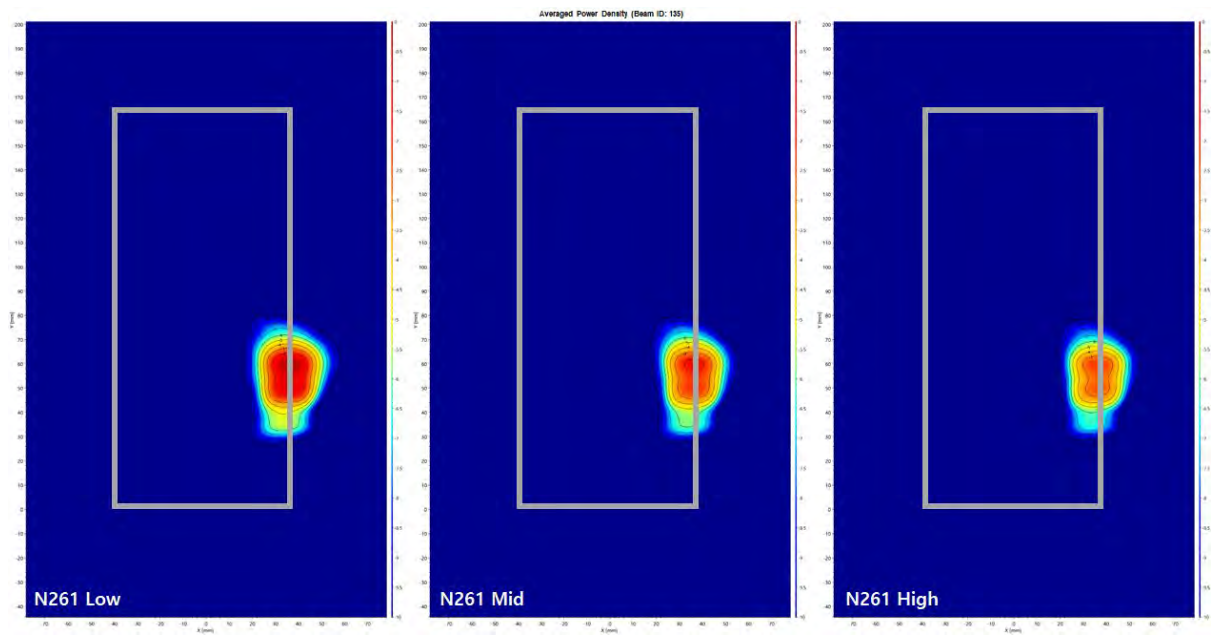
- n261 / Beam ID: 134 / Front surface



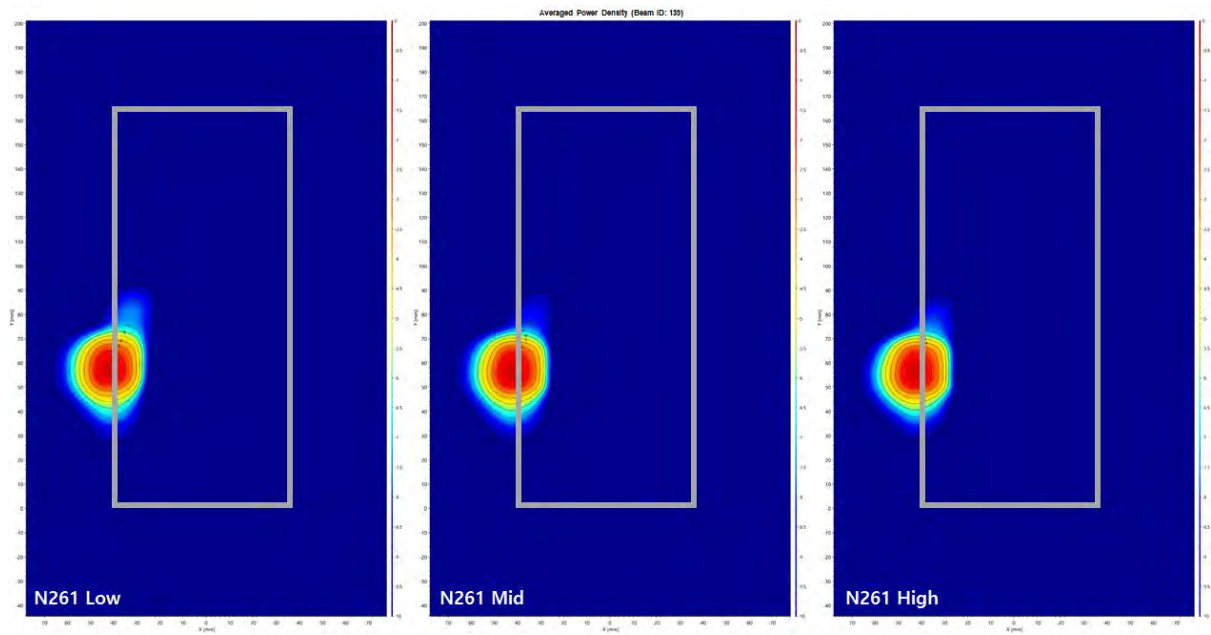
- n261 / Beam ID: 135 / Back surface



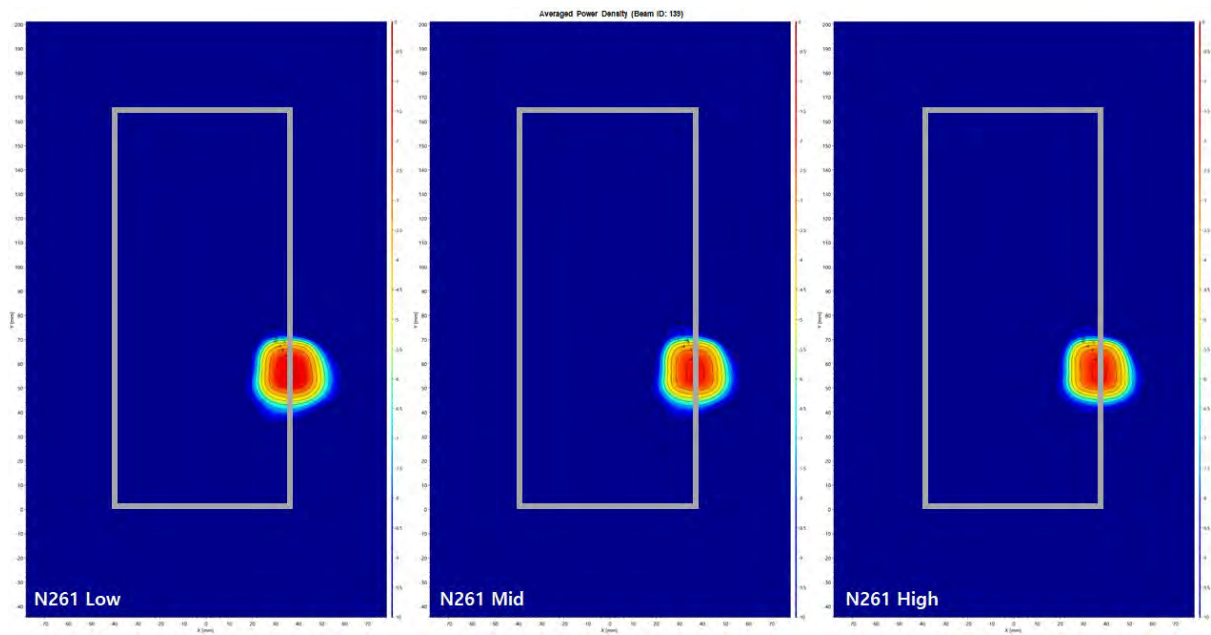
- n261 / Beam ID: 135 / Front surface



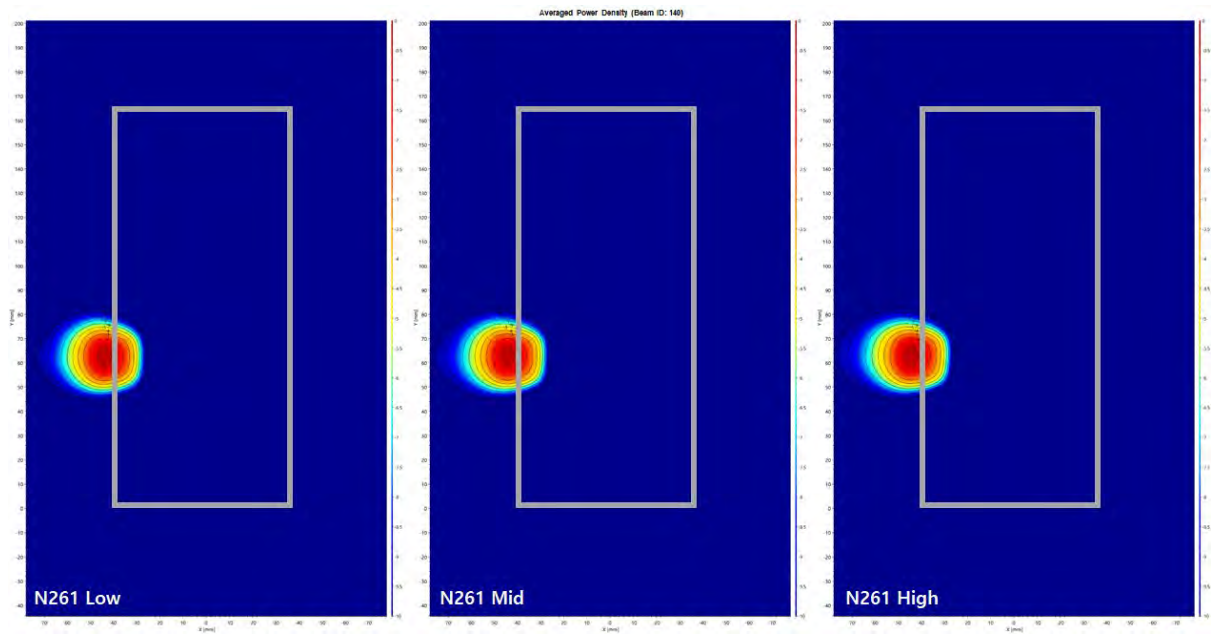
- n261 / Beam ID: 139 / Back surface



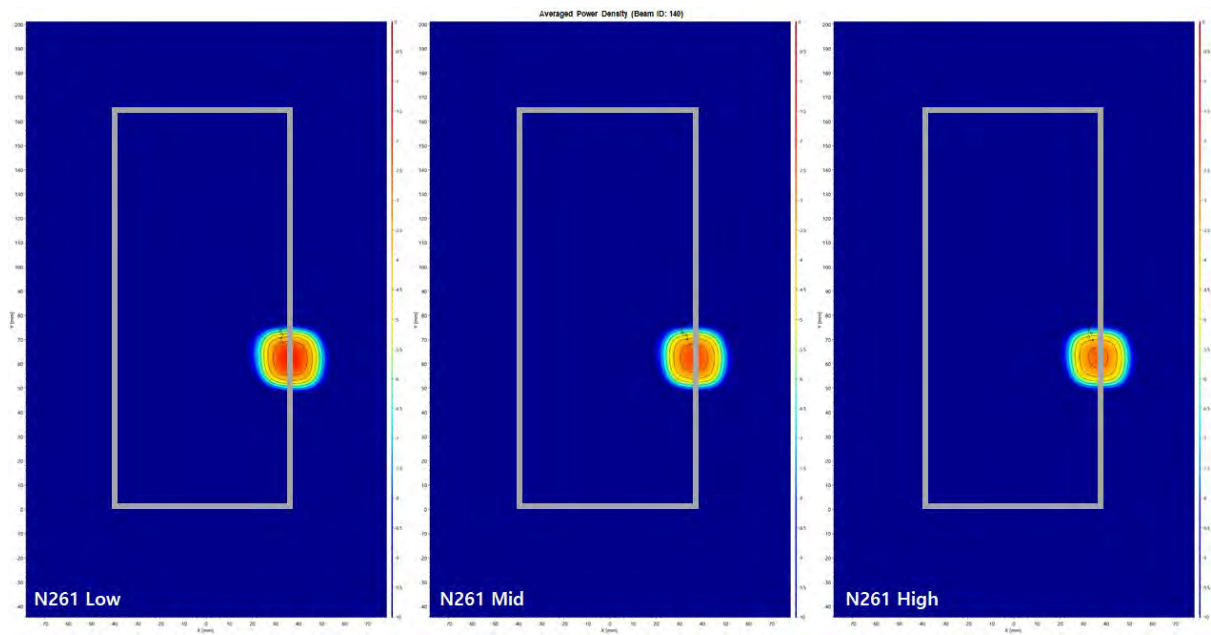
- n261 / Beam ID: 139 / Front surface



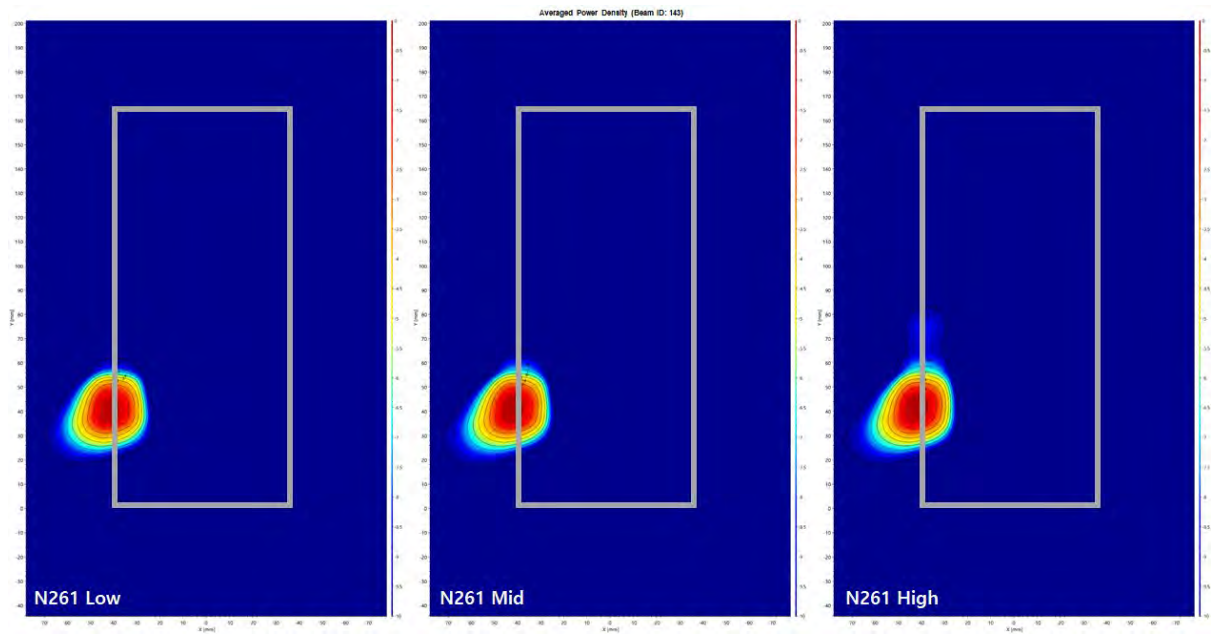
- n261 / Beam ID: 140 / Back surface



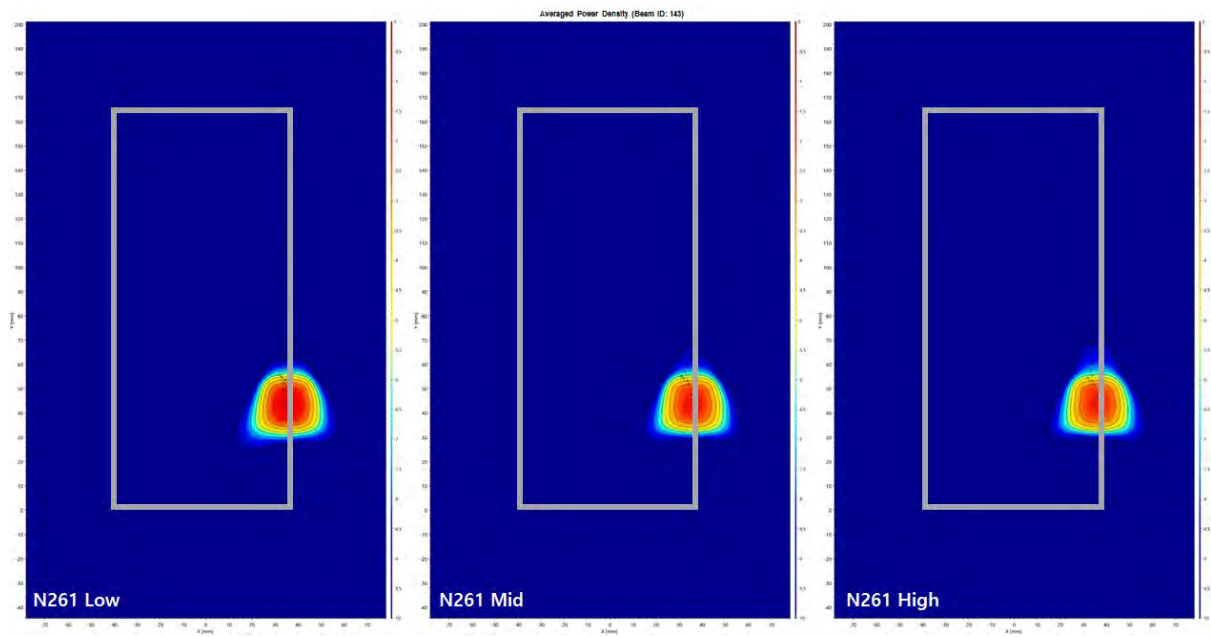
- n261 / Beam ID: 140 / Front surface



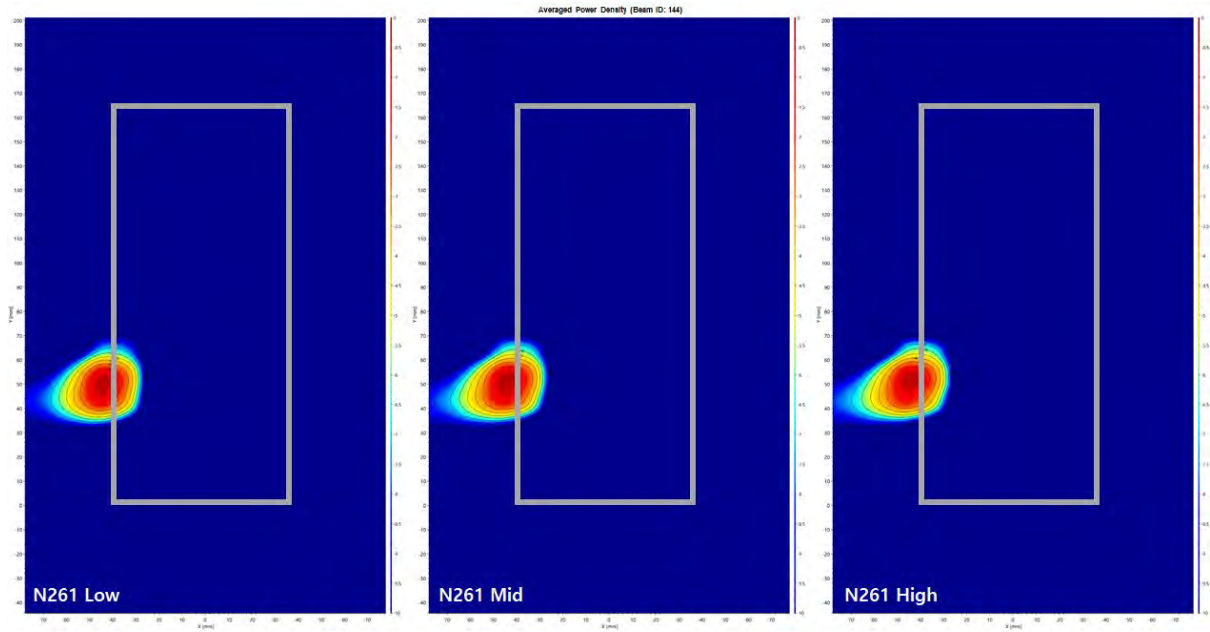
- n261 / Beam ID: 143 / Back surface



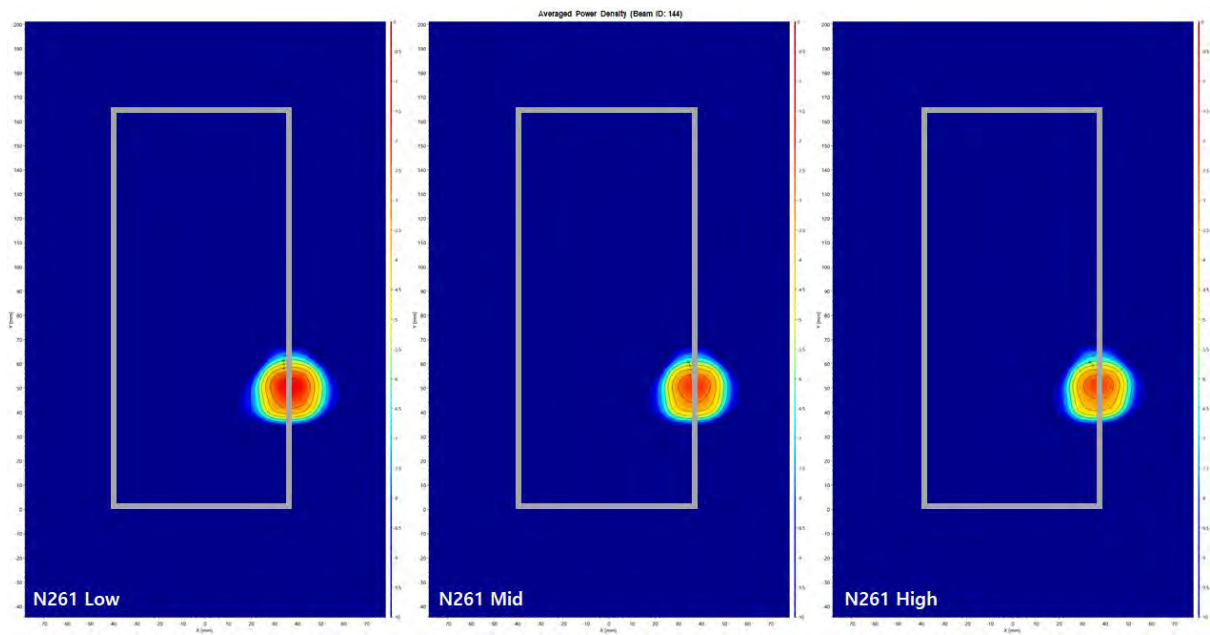
- n261 / Beam ID: 143 / Front surface



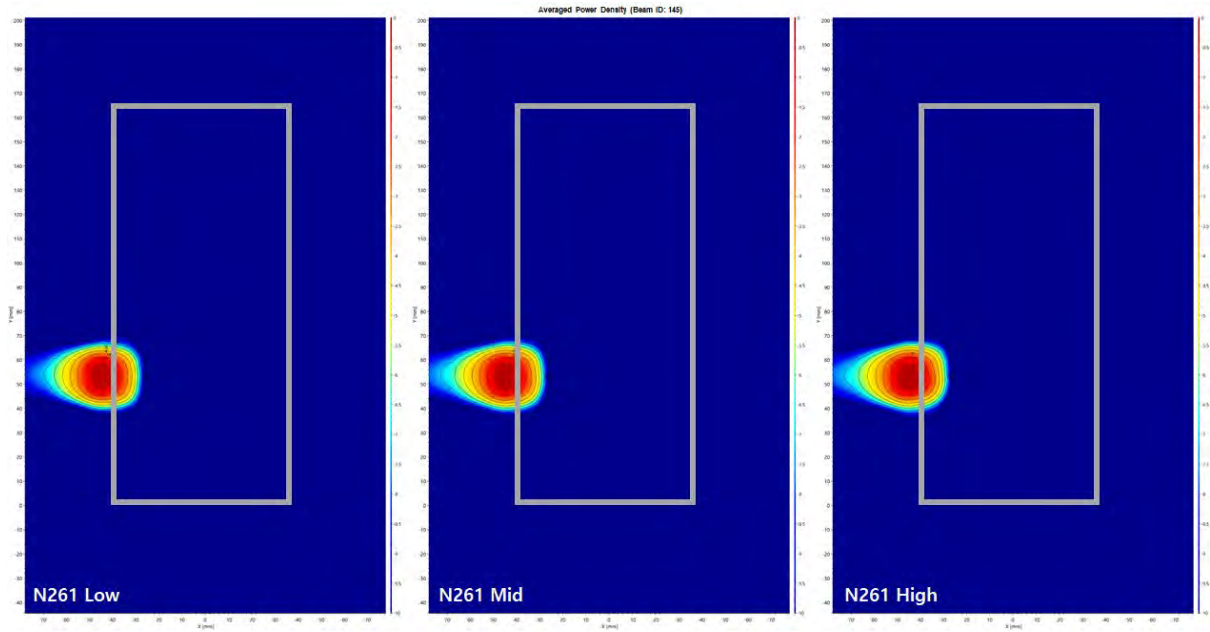
- n261 / Beam ID: 144 / Back surface



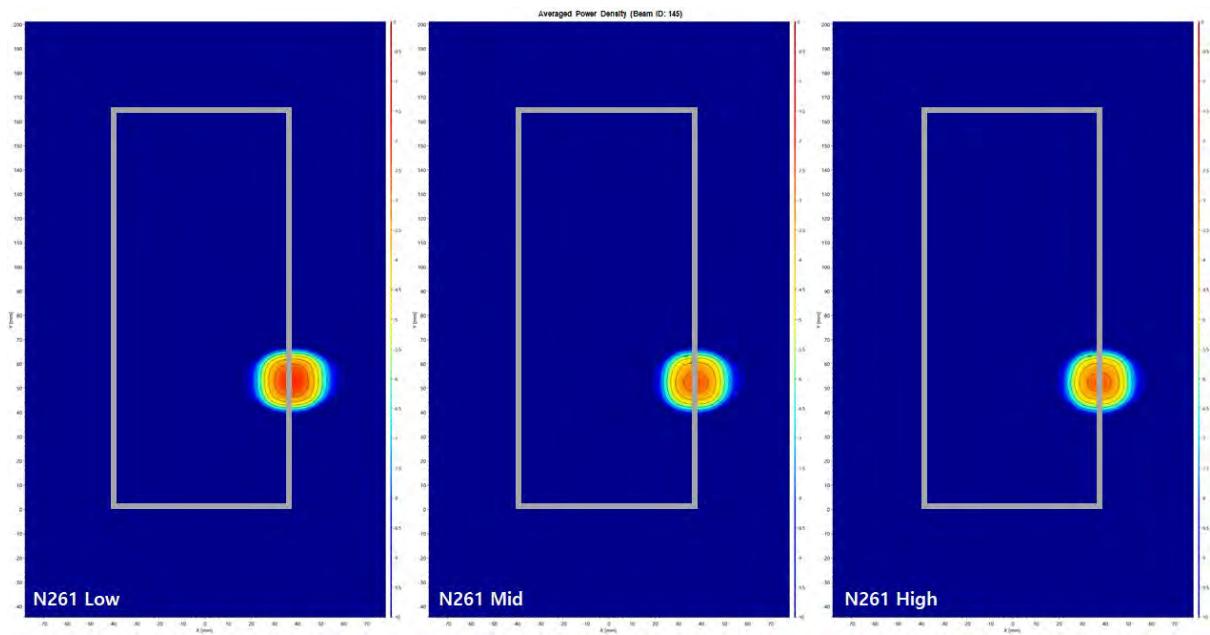
- n261 / Beam ID: 144 / Front surface



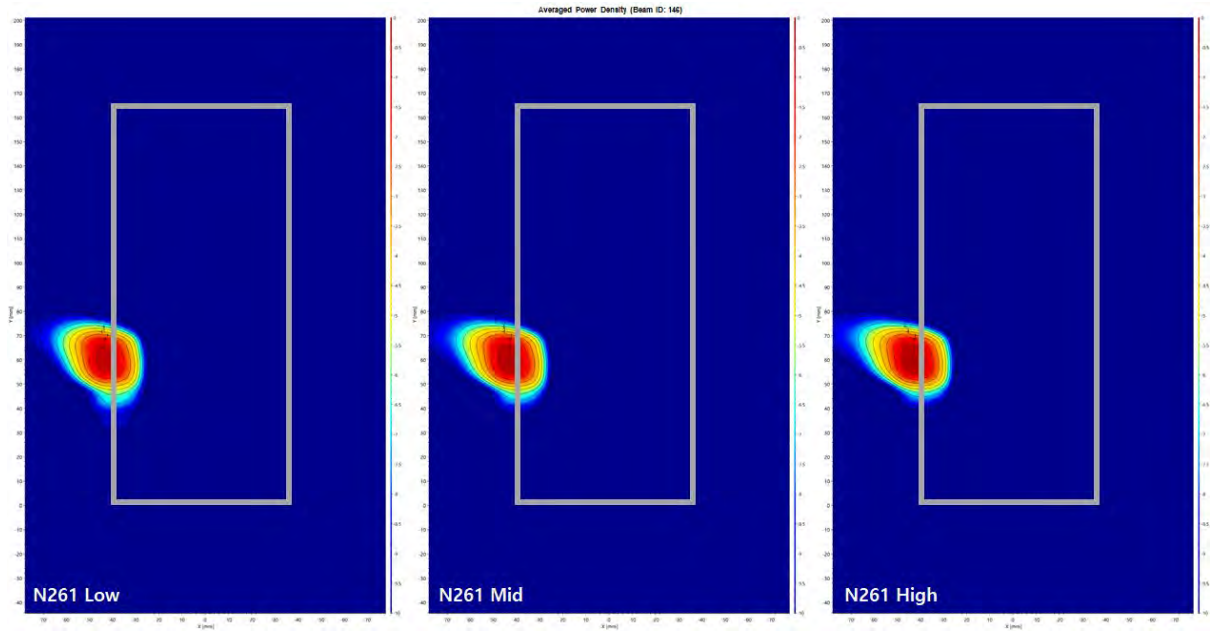
- n261 / Beam ID: 145 / Back surface



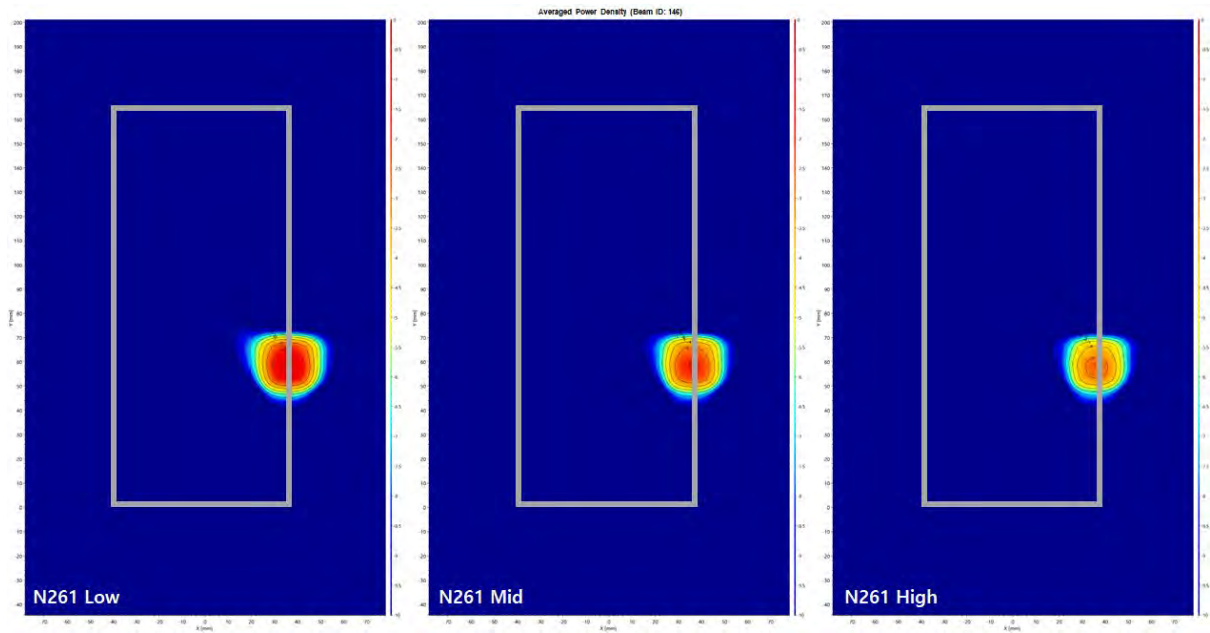
- n261 / Beam ID: 145 / Front surface



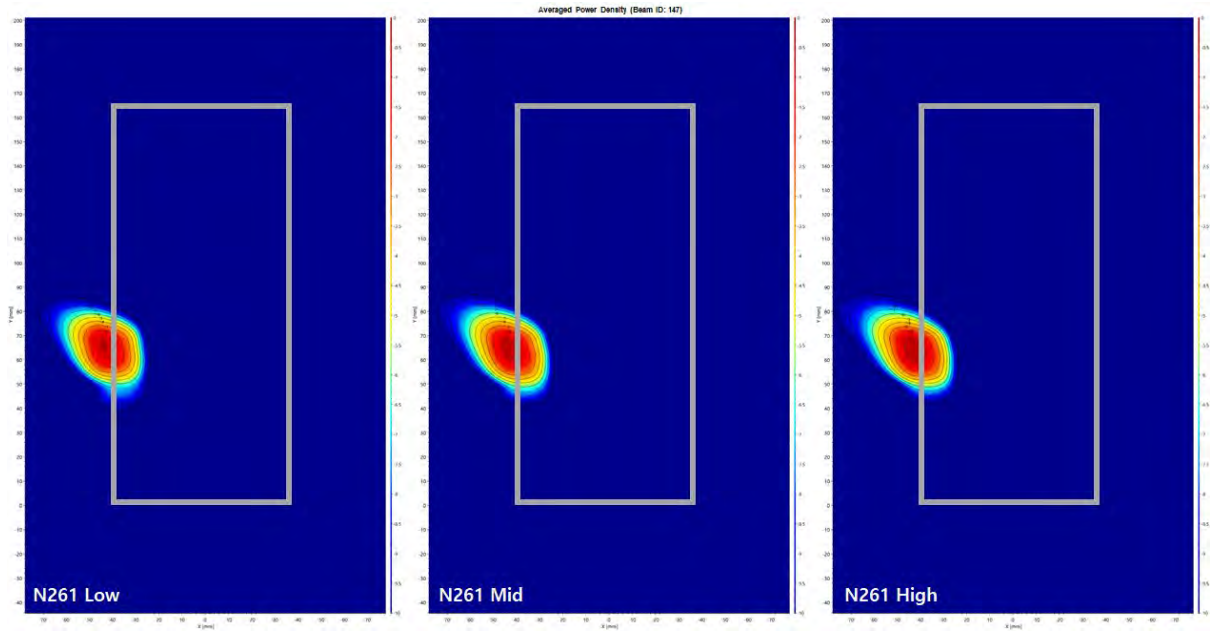
- n261 / Beam ID: 146 / Back surface



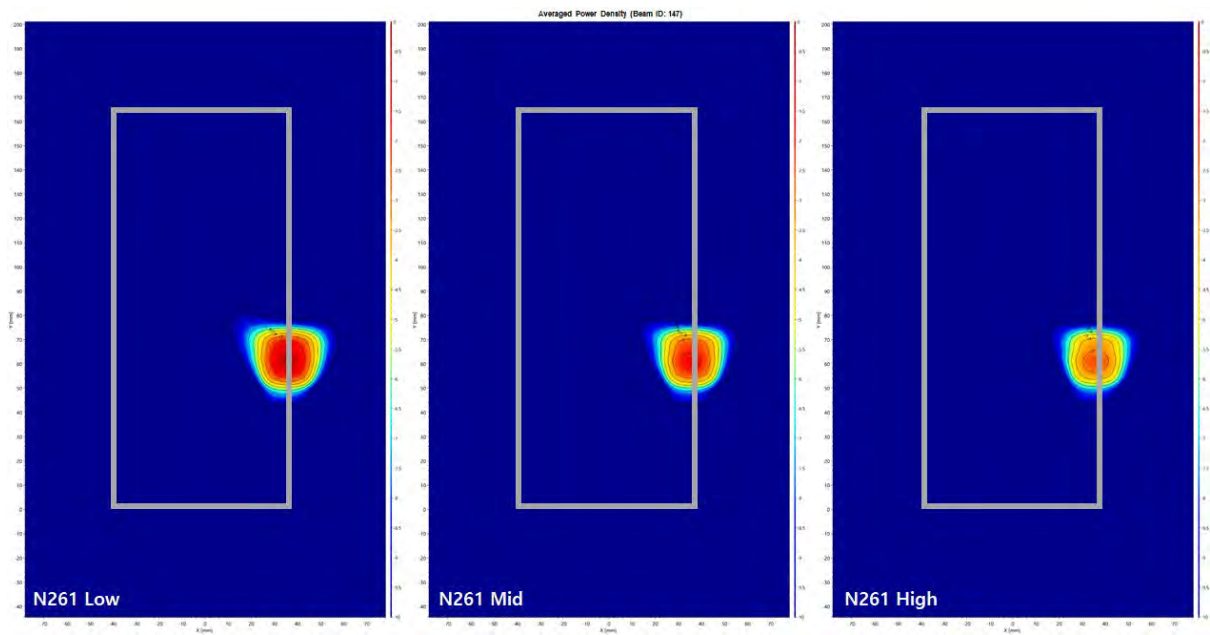
- n261 / Beam ID: 146 / Front surface



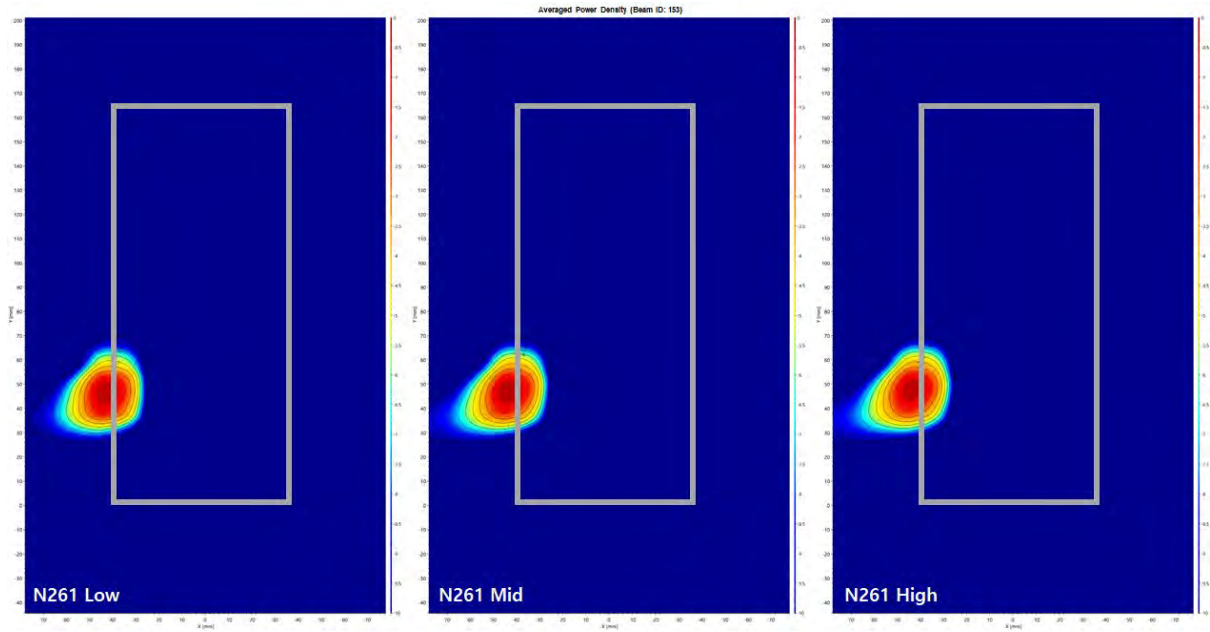
- n261 / Beam ID: 147 / Back surface



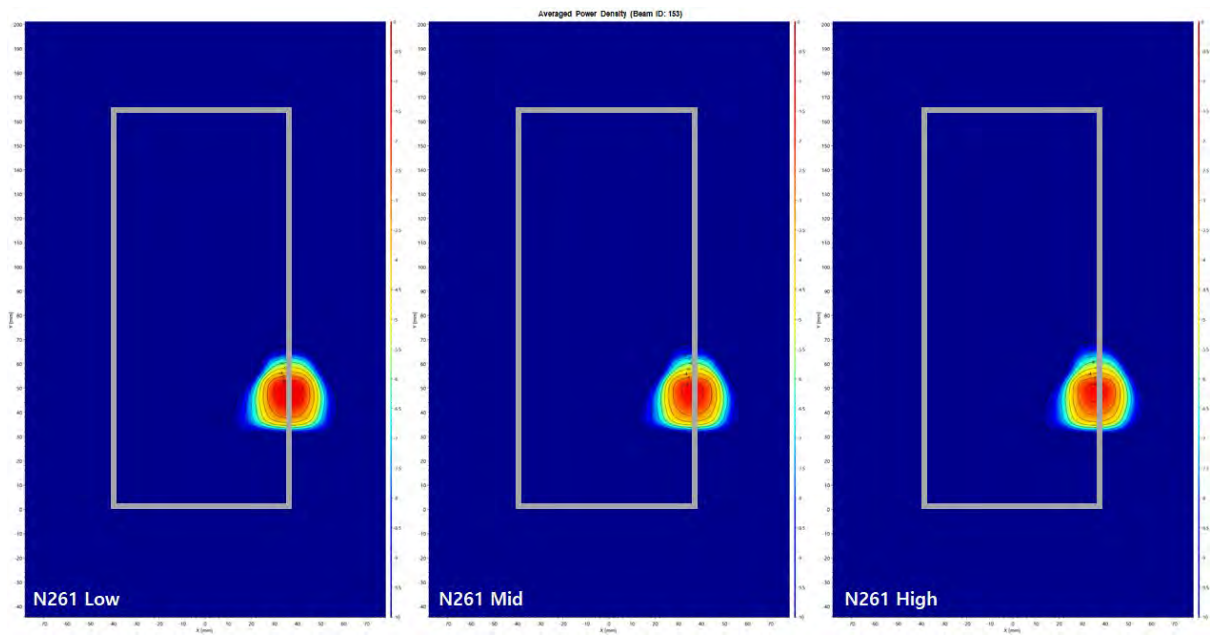
- n261 / Beam ID: 147 / Front surface



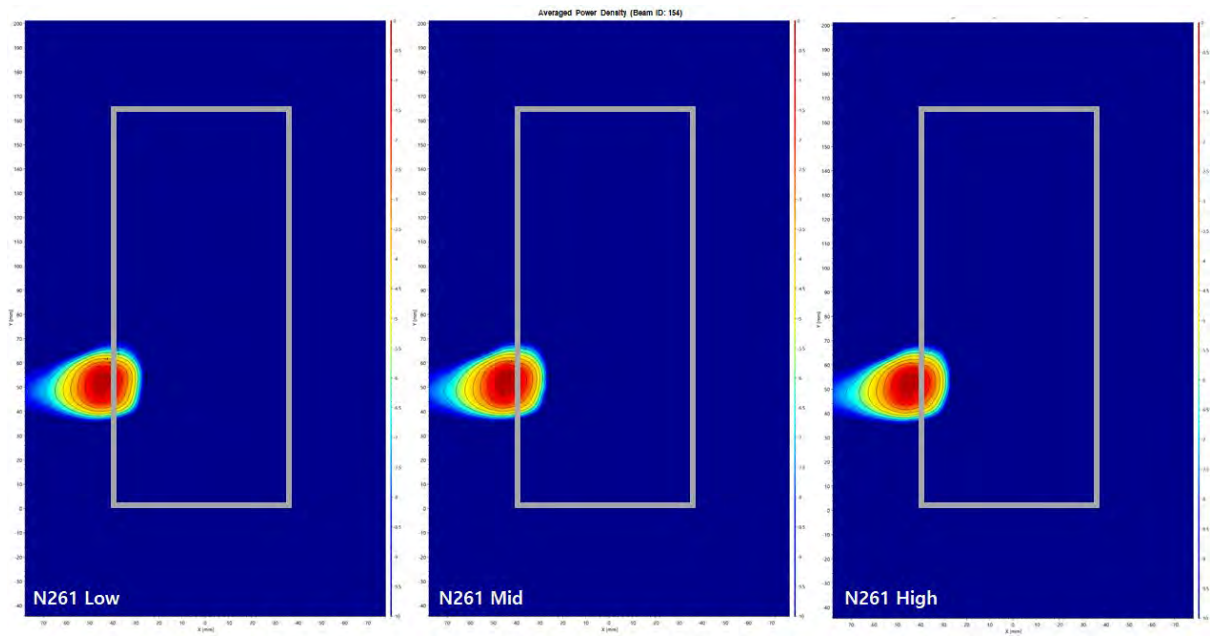
- n261 / Beam ID: 153 / Back surface



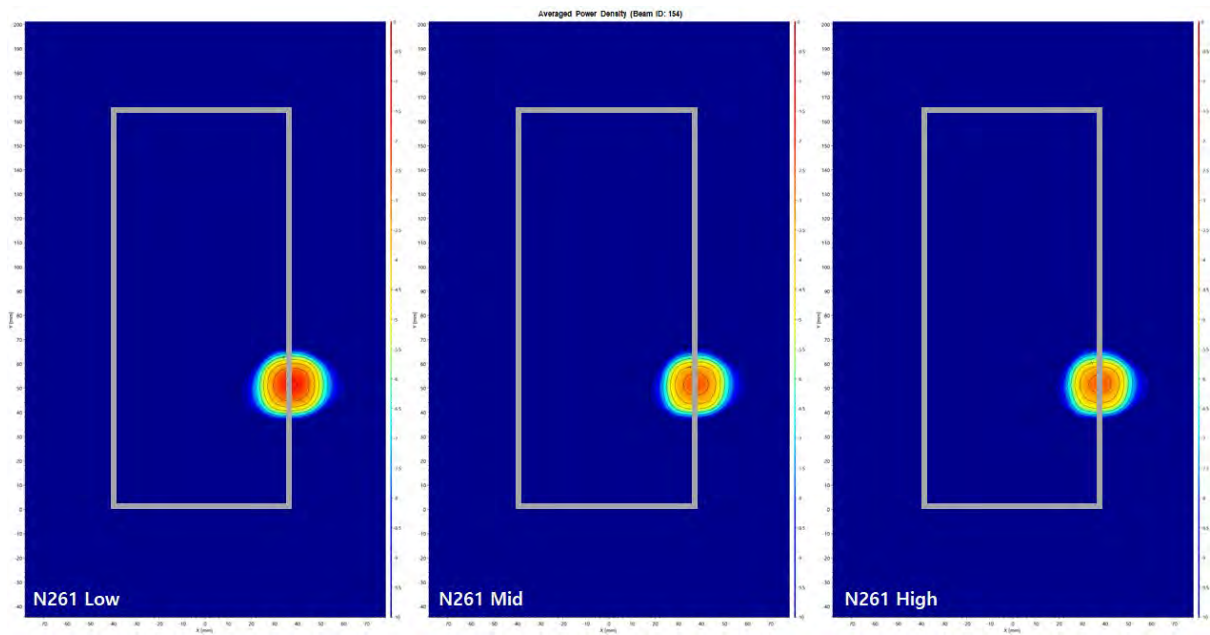
- n261 / Beam ID: 153 / Front surface



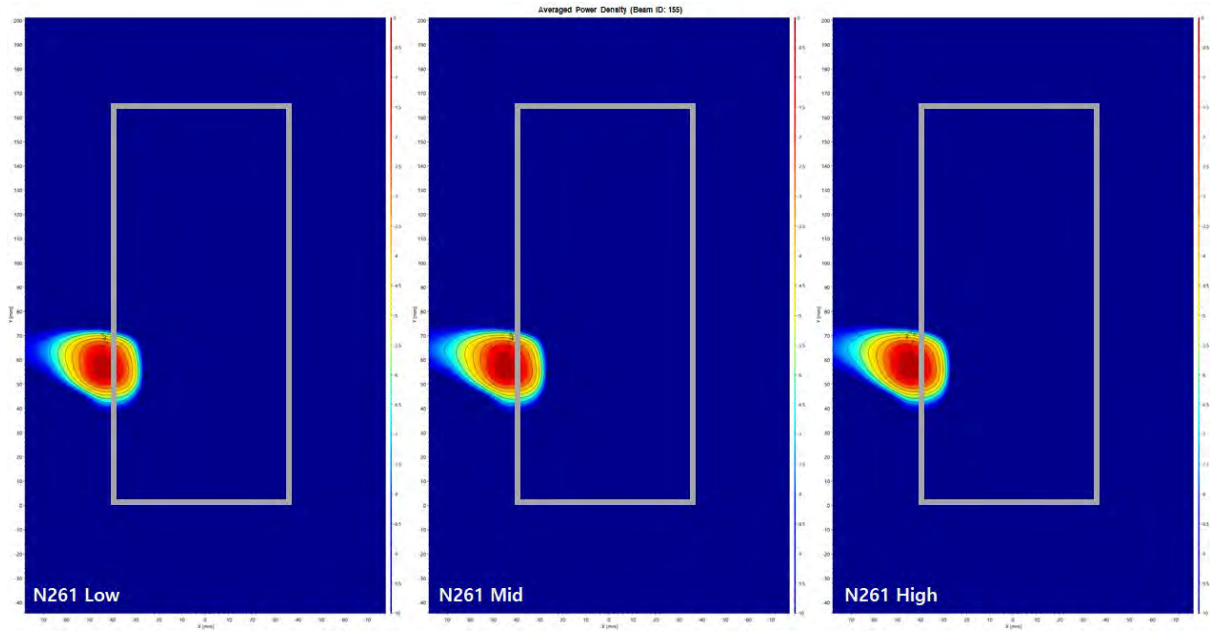
- n261 / Beam ID: 154 / Back surface



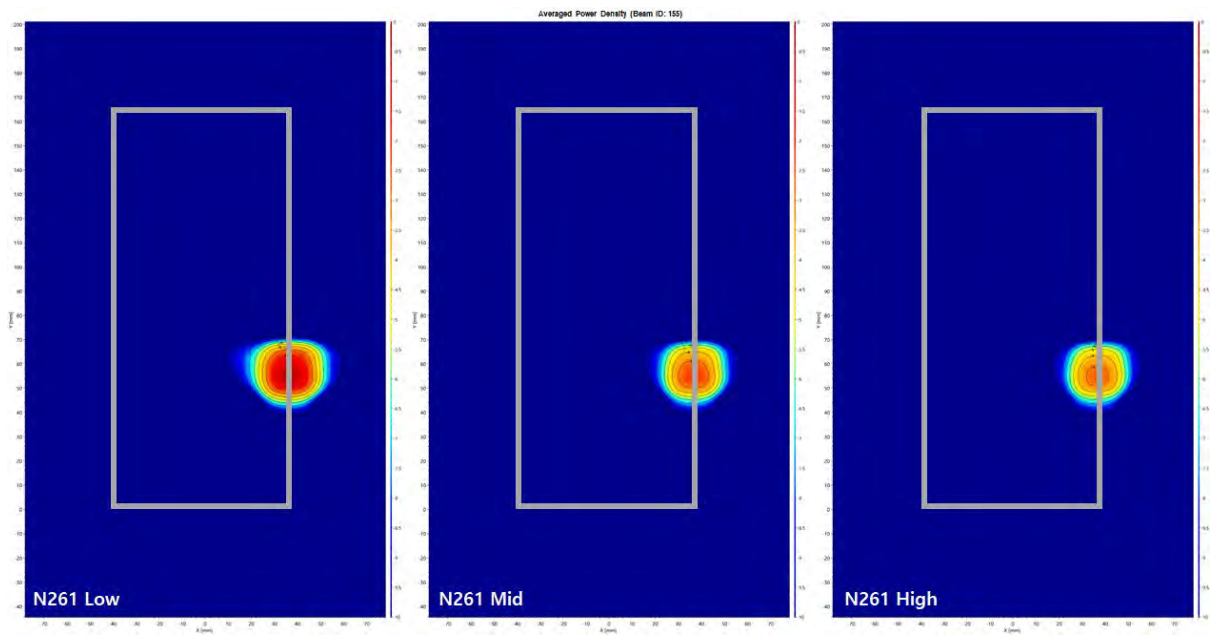
- n261 / Beam ID: 154 / Front surface



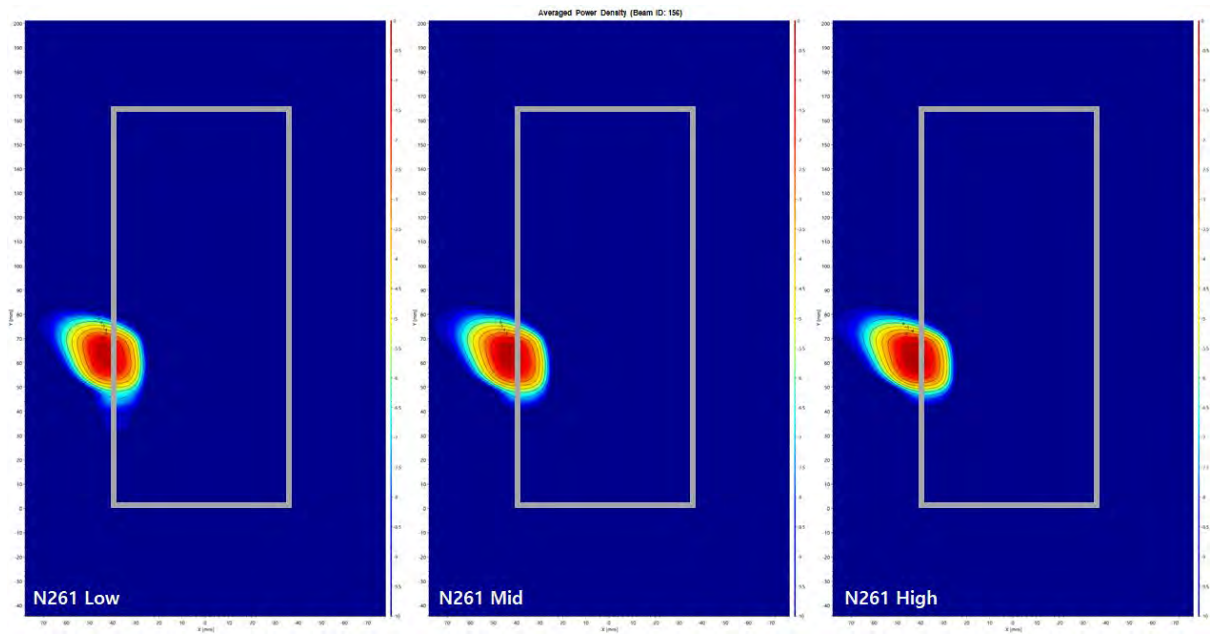
- n261 / Beam ID: 155 / Back surface



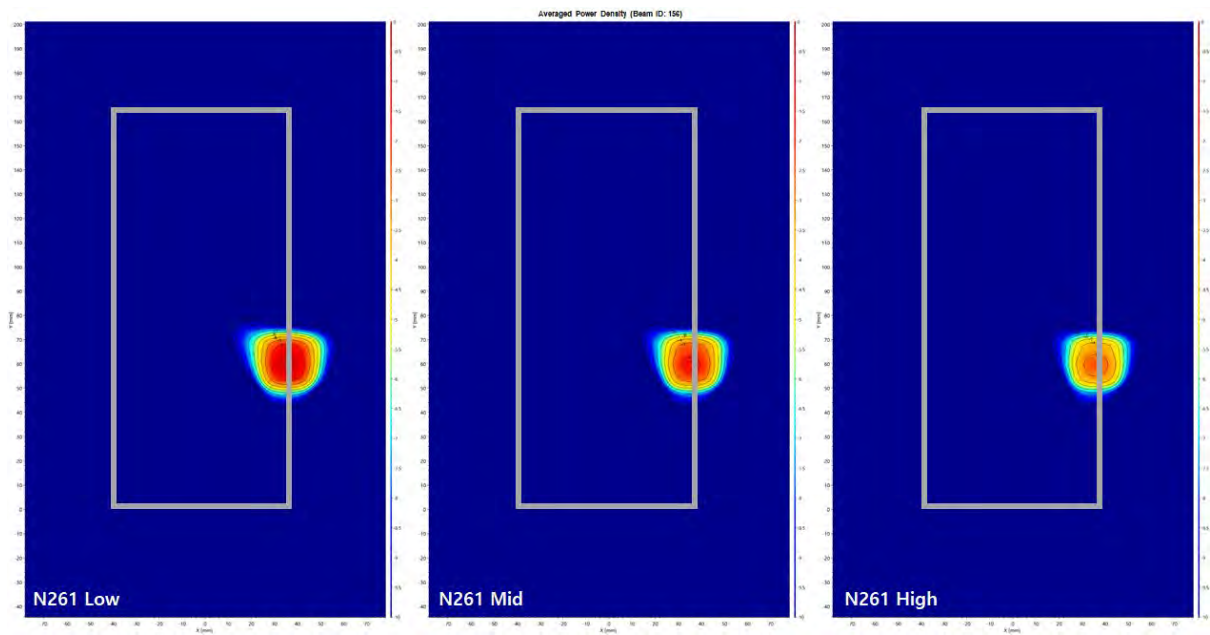
- n261 / Beam ID: 155 / Front surface



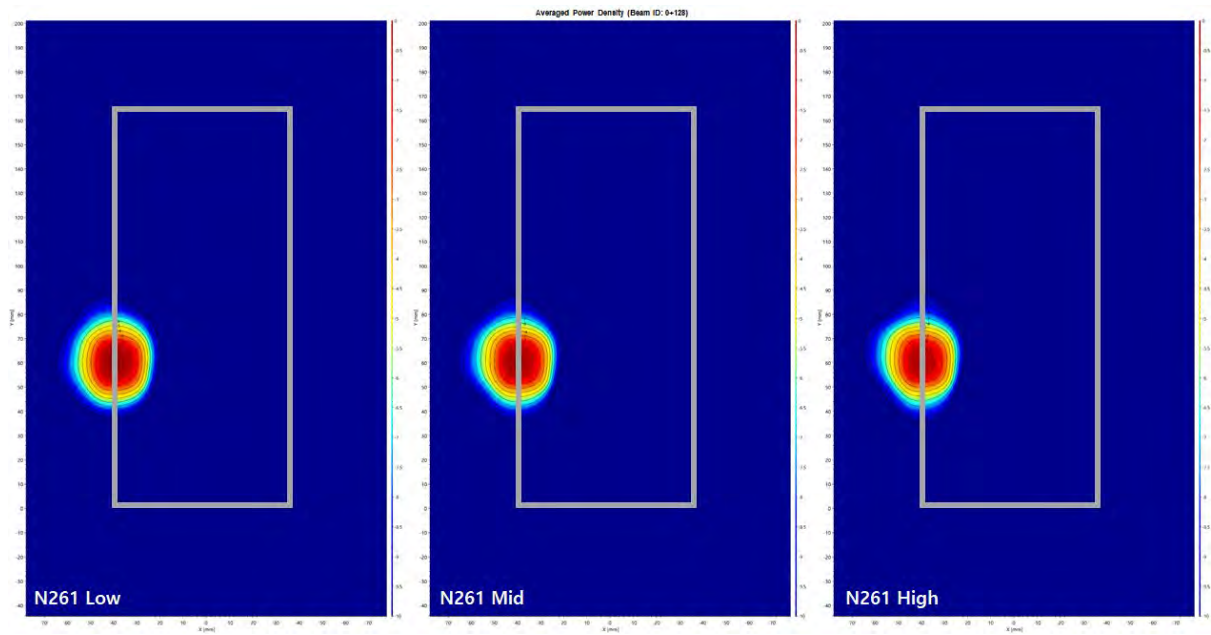
- n261 / Beam ID: 156 / Back surface



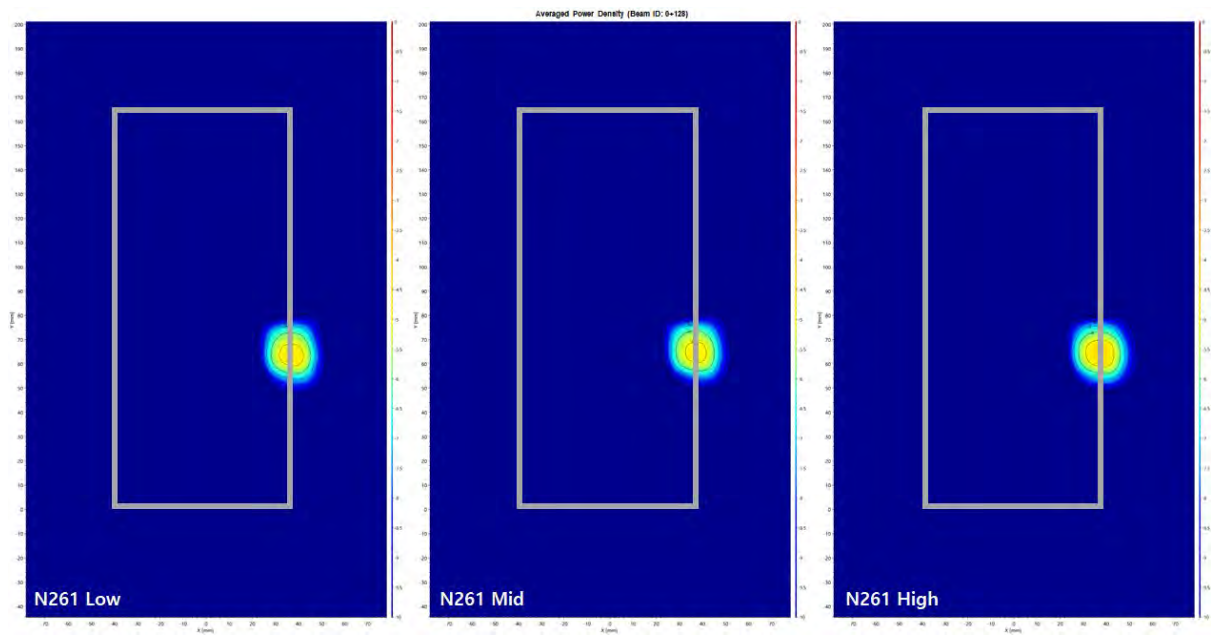
- n261 / Beam ID: 156 / Front surface



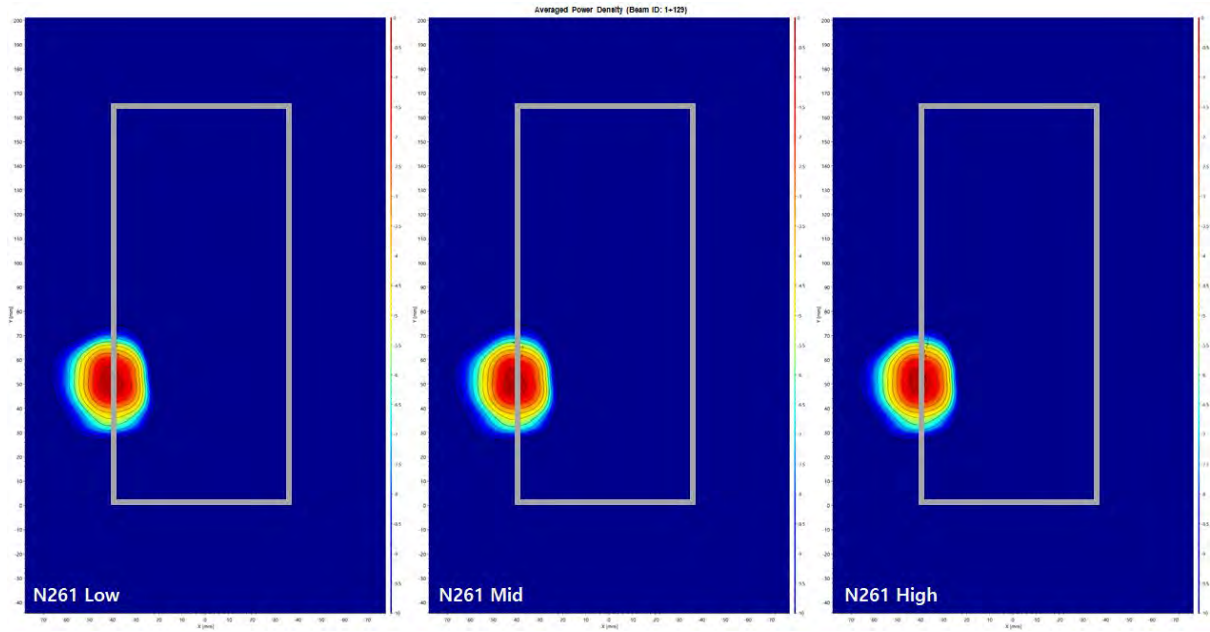
- n261 / Beam ID: 0+128 / Back surface



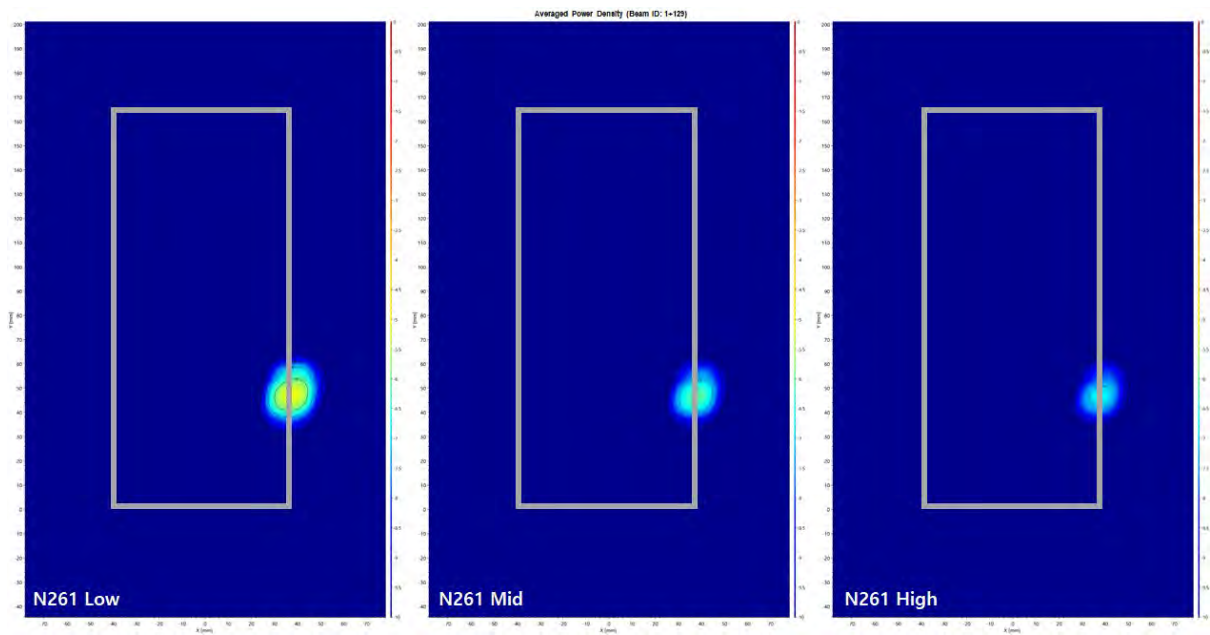
- n261 / Beam ID: 0+128 / Front surface



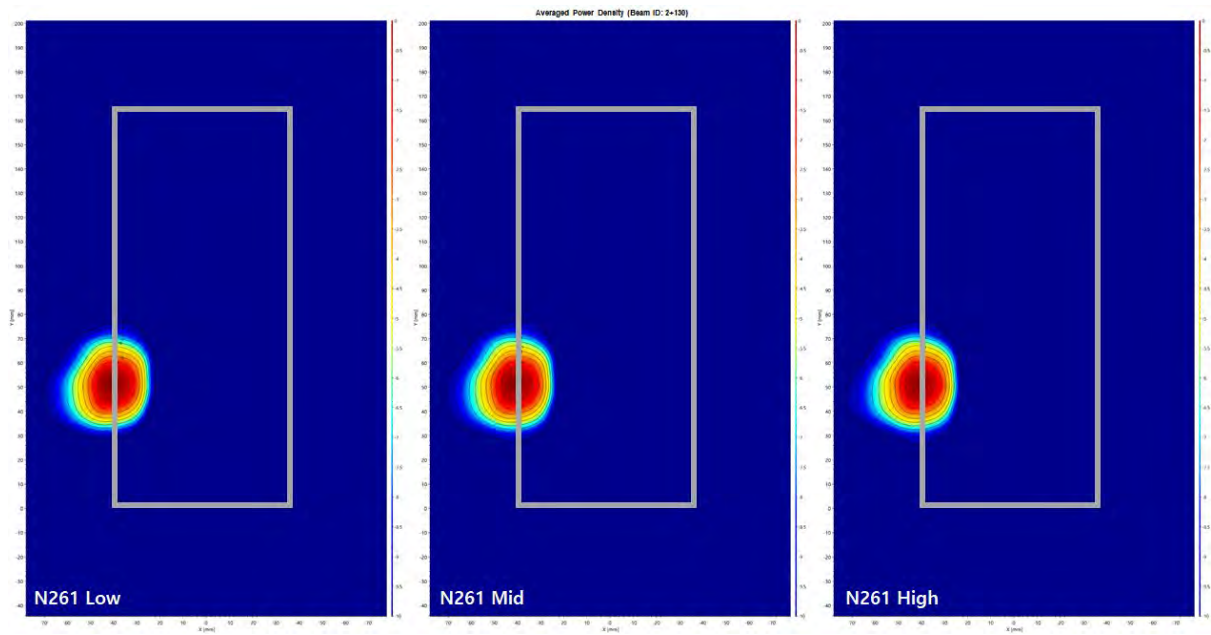
- n261 / Beam ID: 1+129 / Back surface



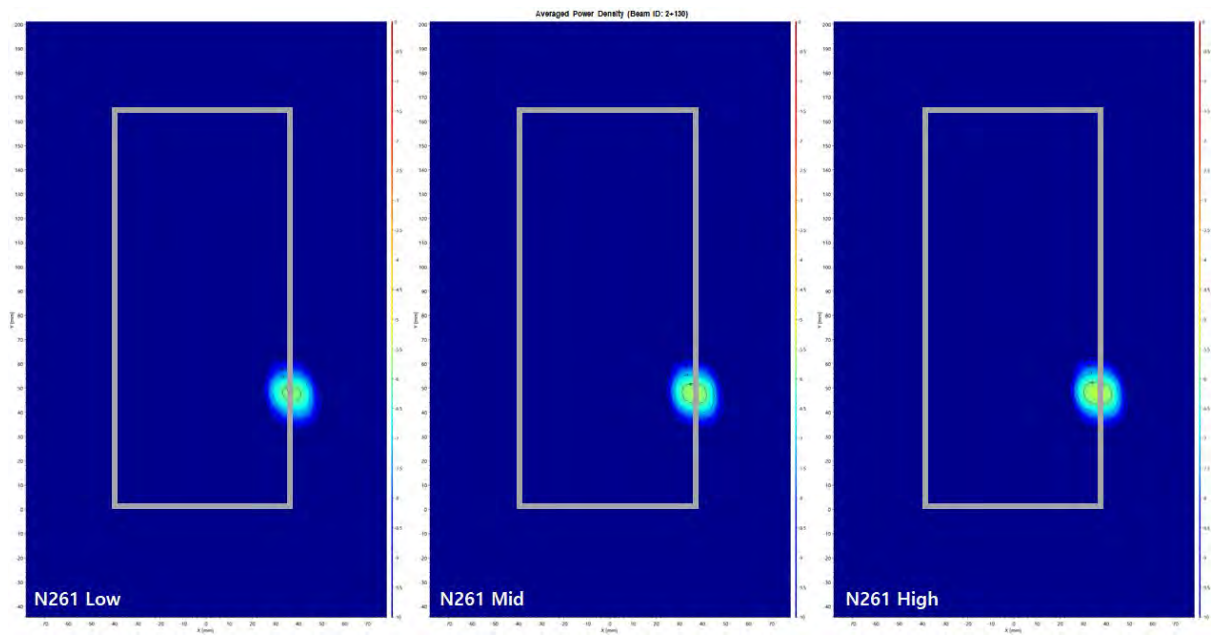
- n261 / Beam ID: 1+129 / Front surface



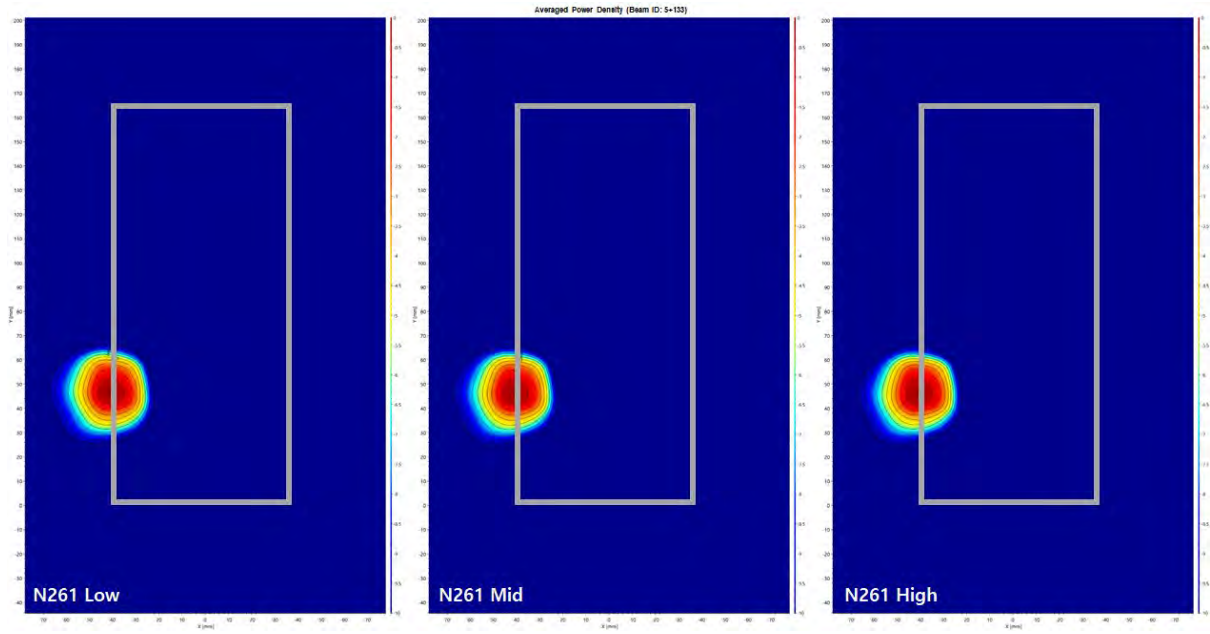
- n261 / Beam ID: 2+130 / Back surface



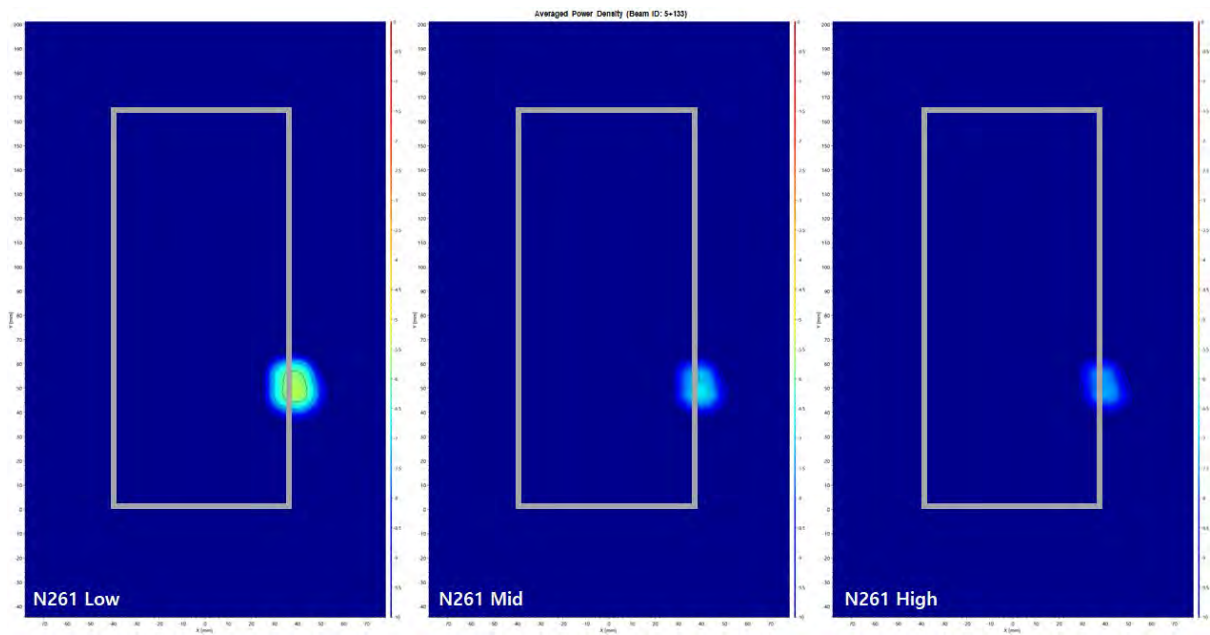
- n261 / Beam ID: 2+130 / Front surface



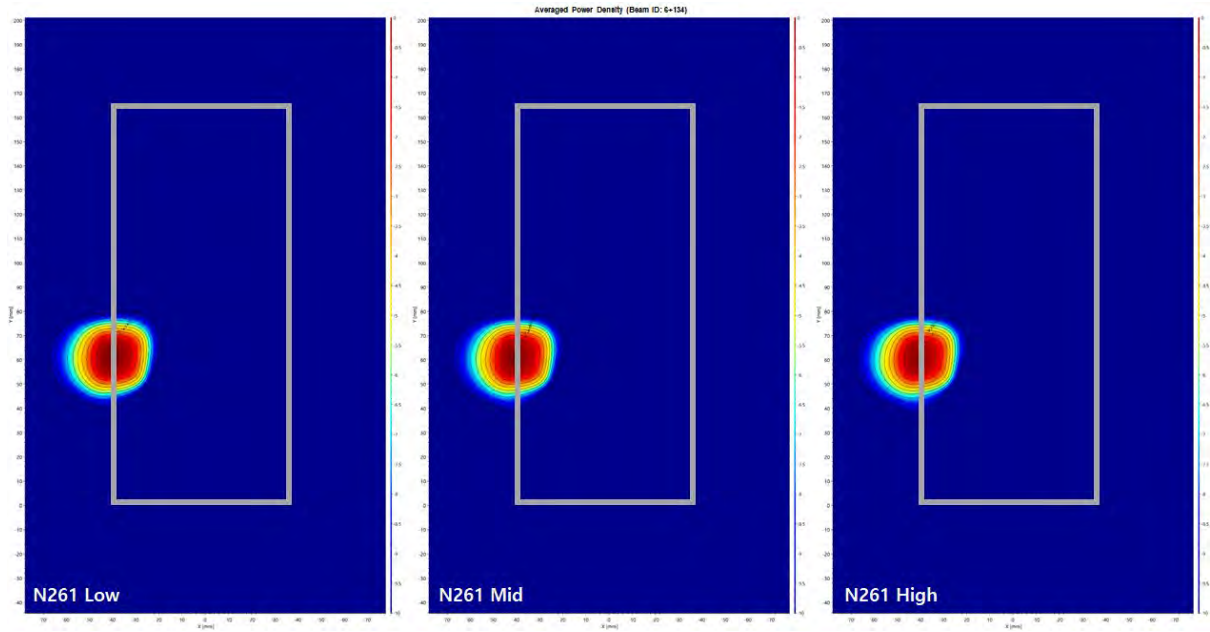
- n261 / Beam ID: 5+133 / Back surface



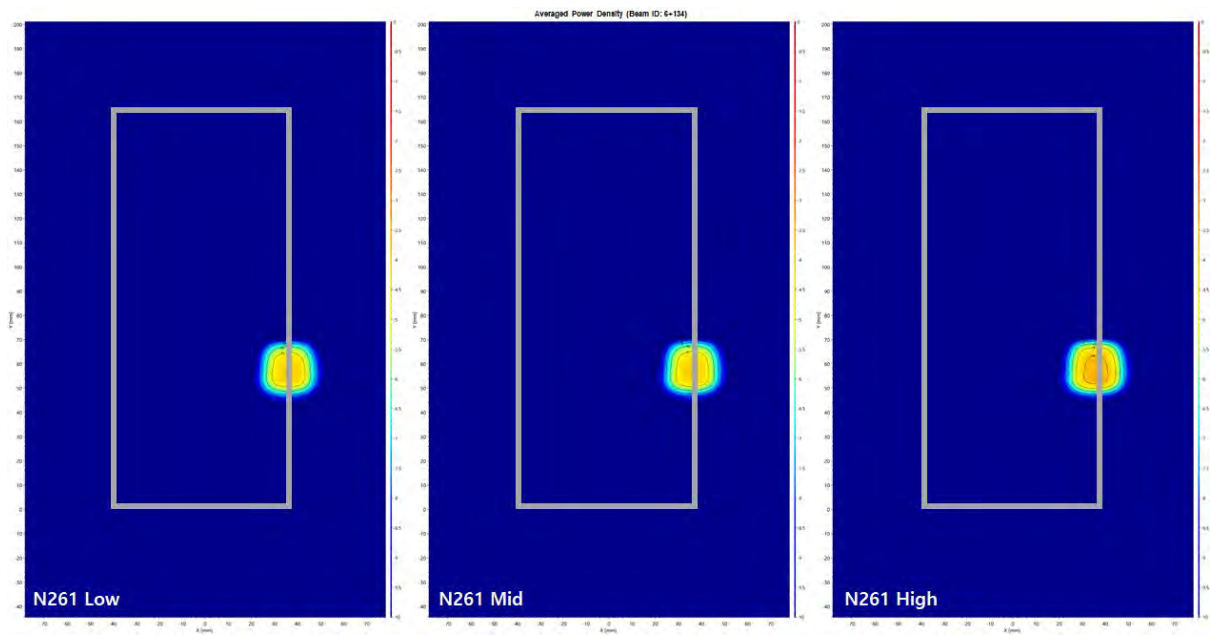
- n261 / Beam ID: 5+133 / Front surface



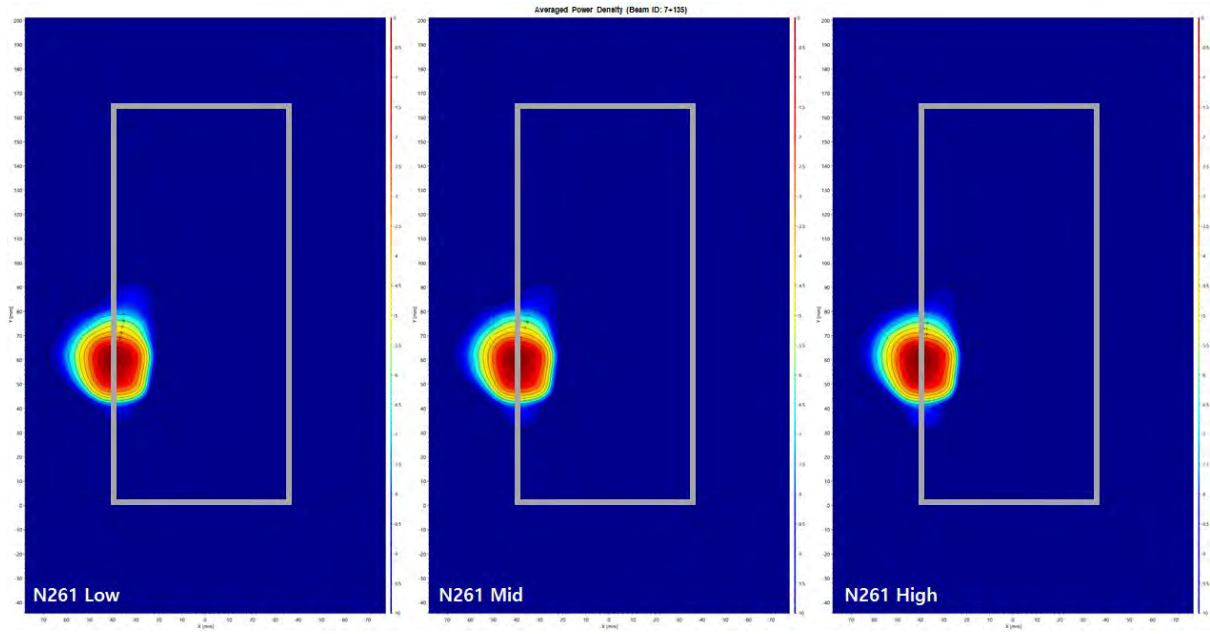
- n261 / Beam ID: 6+134 / Back surface



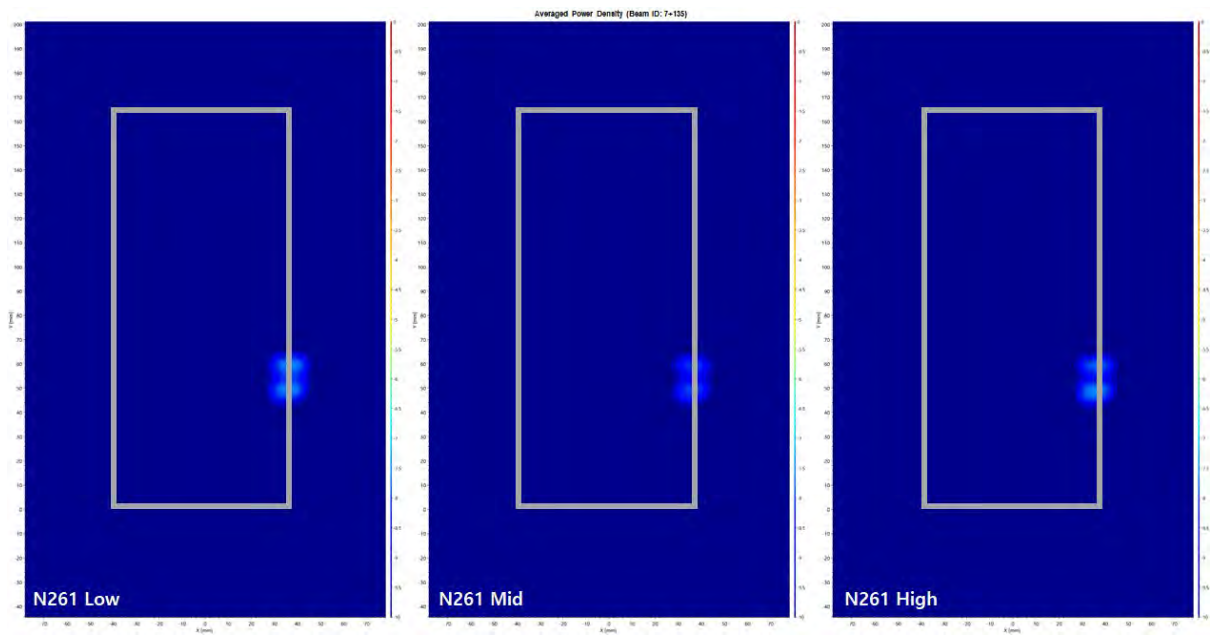
- n261 / Beam ID: 6+134 / Front surface



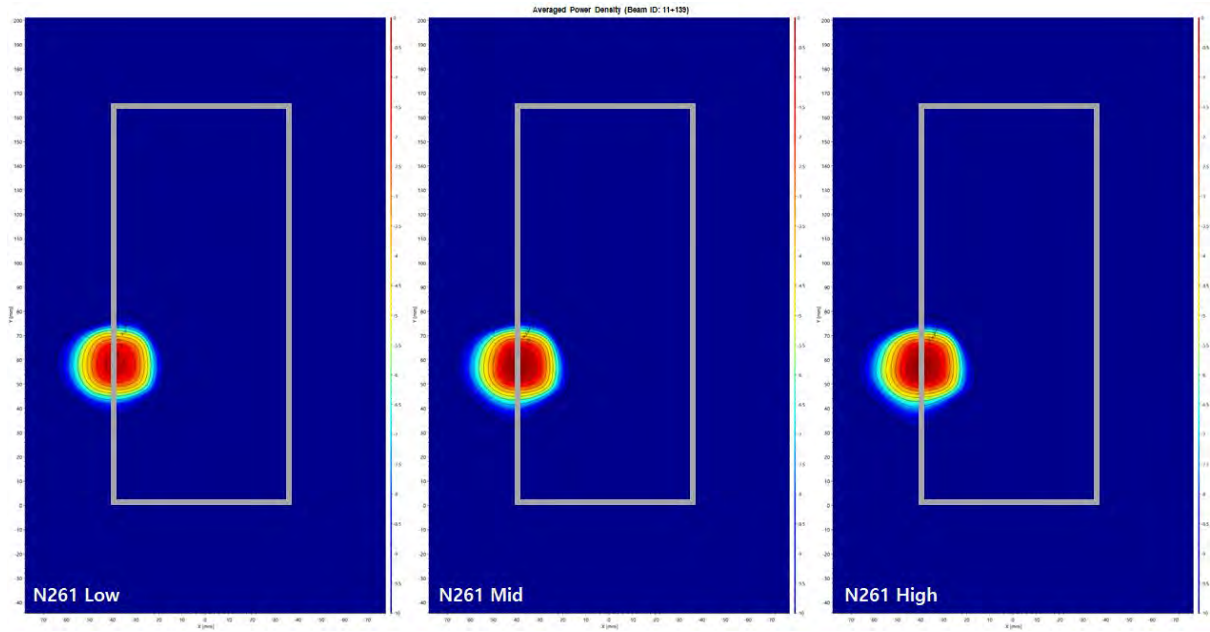
- n261 / Beam ID: 7+135 / Back surface



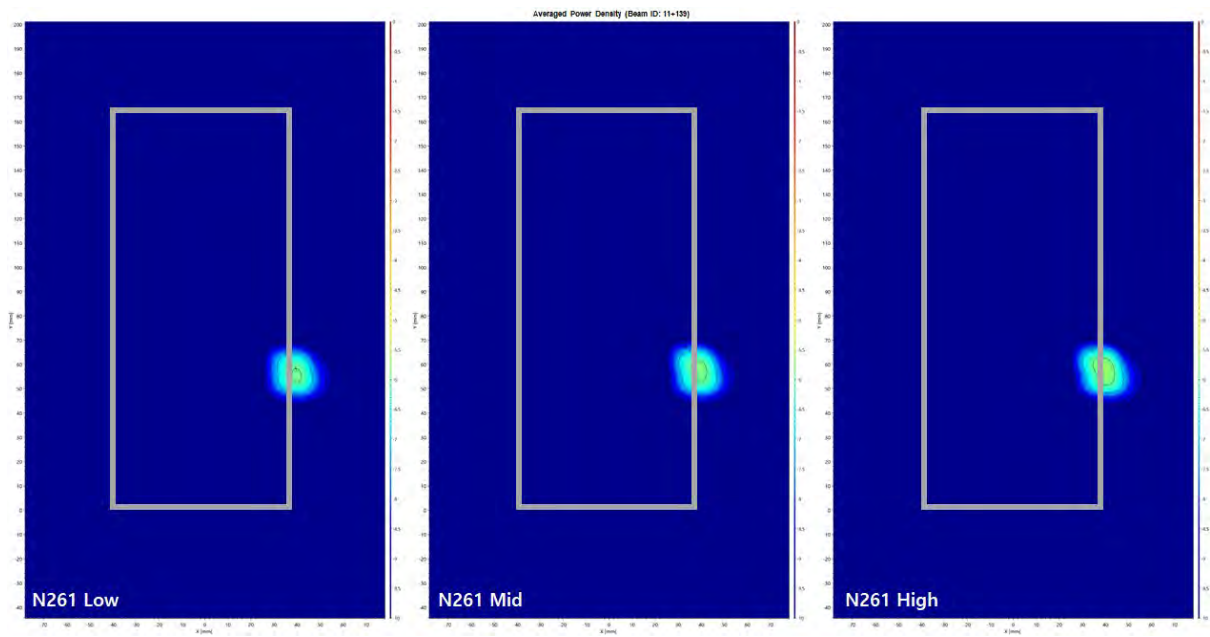
- n261 / Beam ID: 7+135 / Front surface



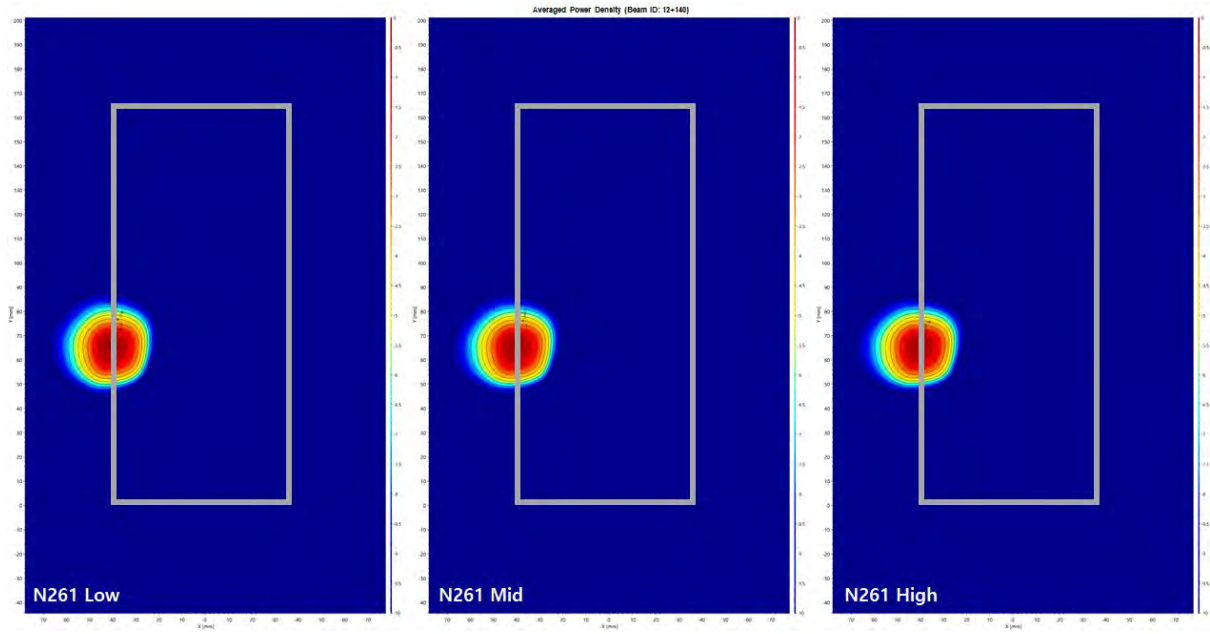
- n261 / Beam ID: 11+139 / Back surface



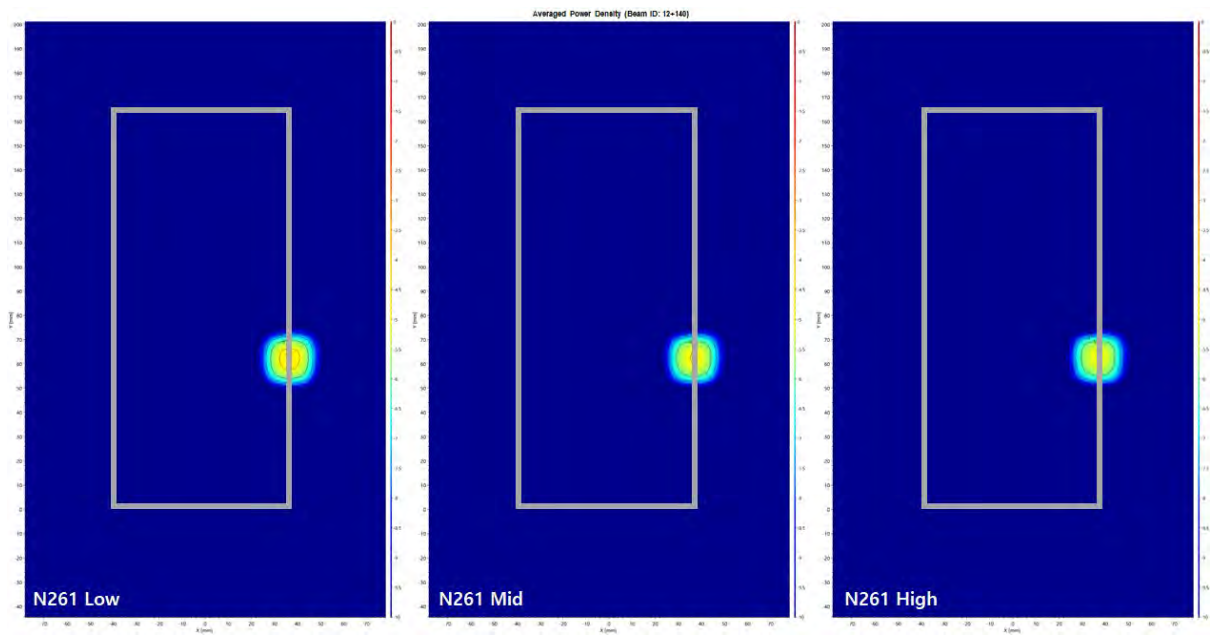
- n261 / Beam ID: 11+139 / Front surface



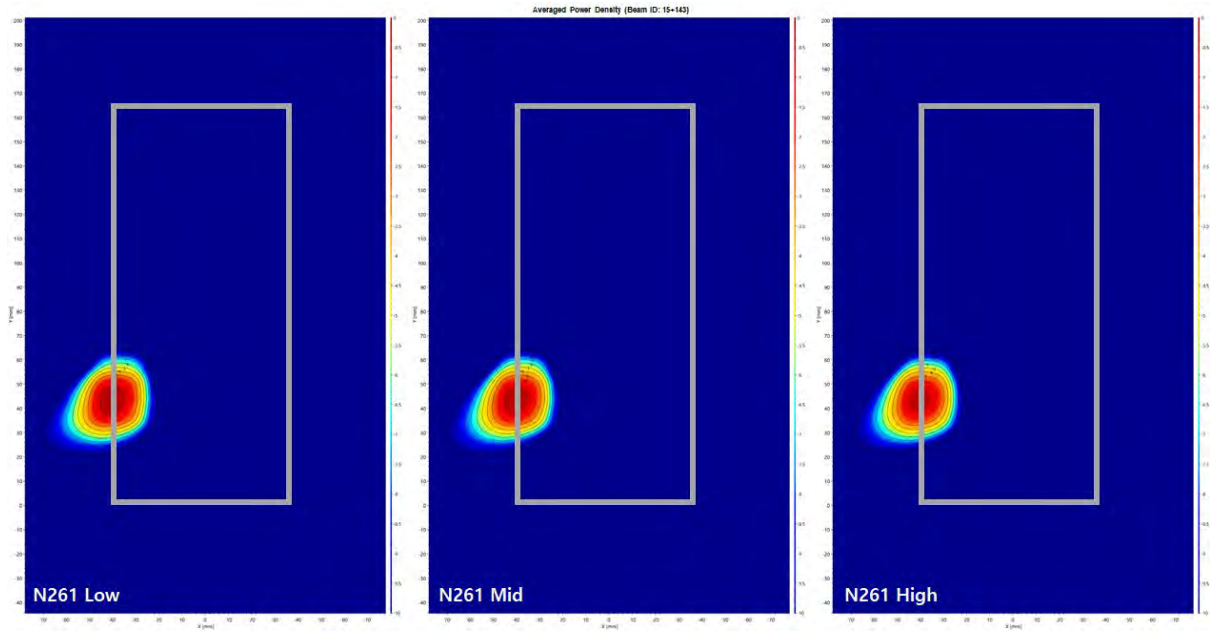
- n261 / Beam ID: 12+140 / Back surface



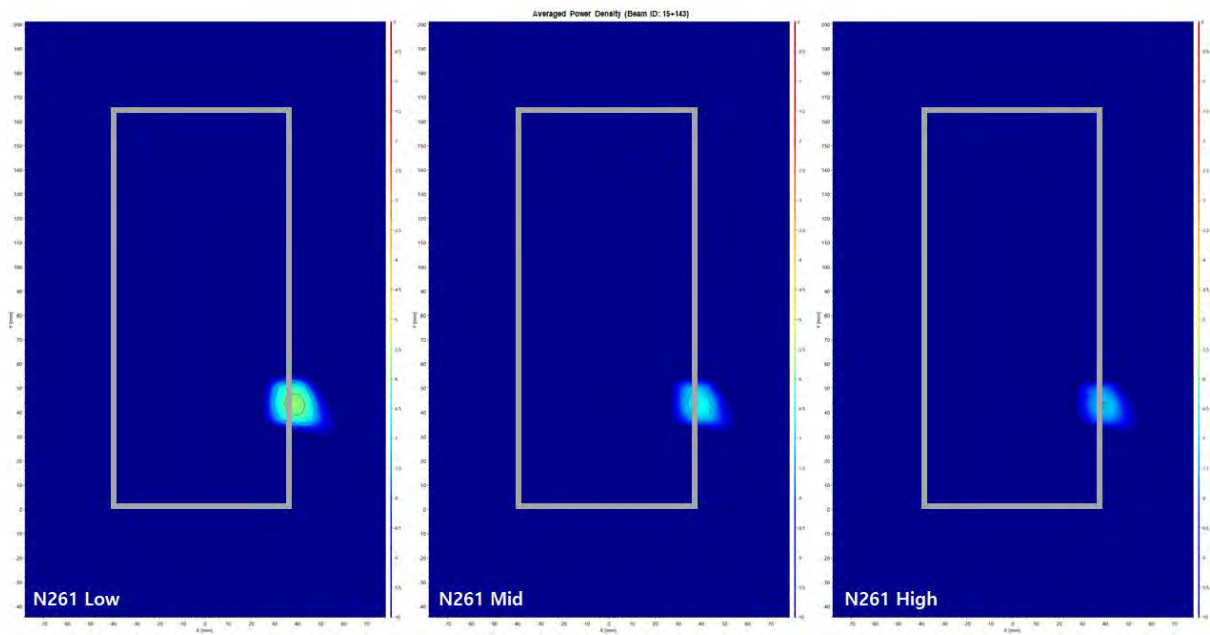
- n261 / Beam ID: 12+140 / Front surface



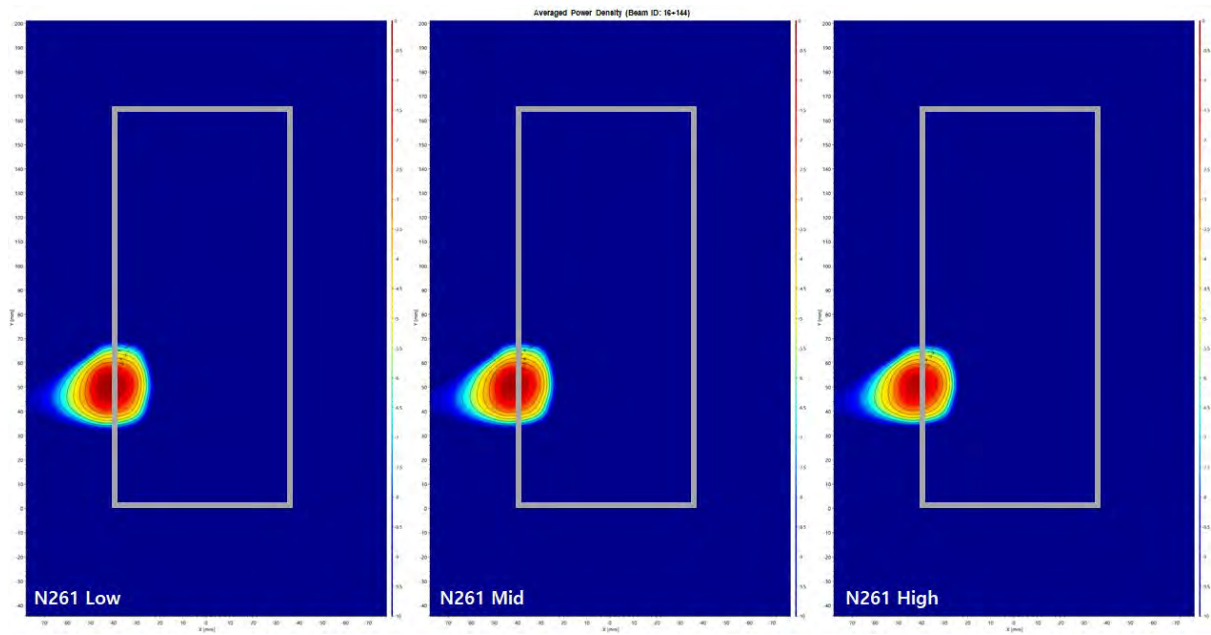
- n261 / Beam ID: 15+143 / Back surface



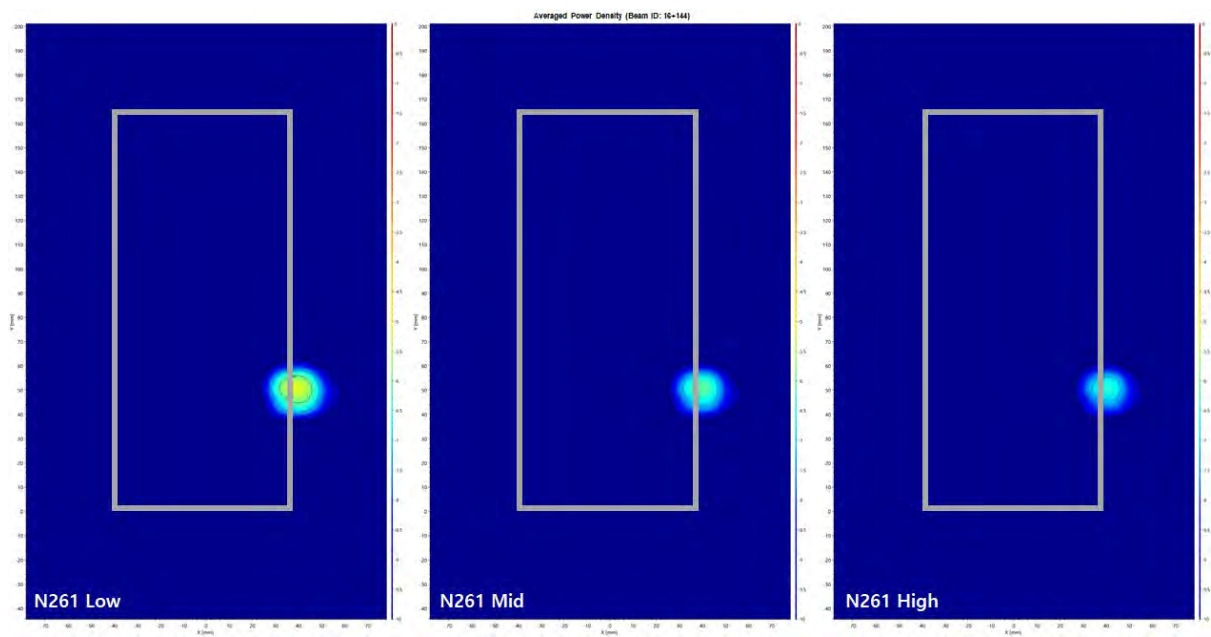
- n261 / Beam ID: 15+143 / Front surface



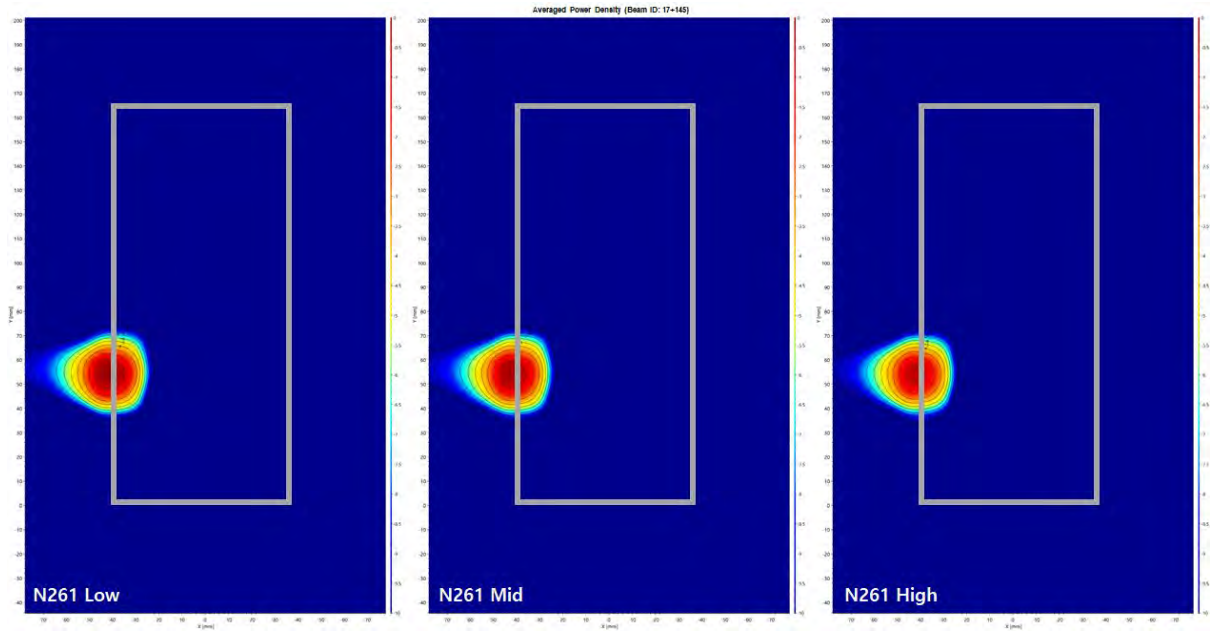
- n261 / Beam ID: 16+144 / Back surface



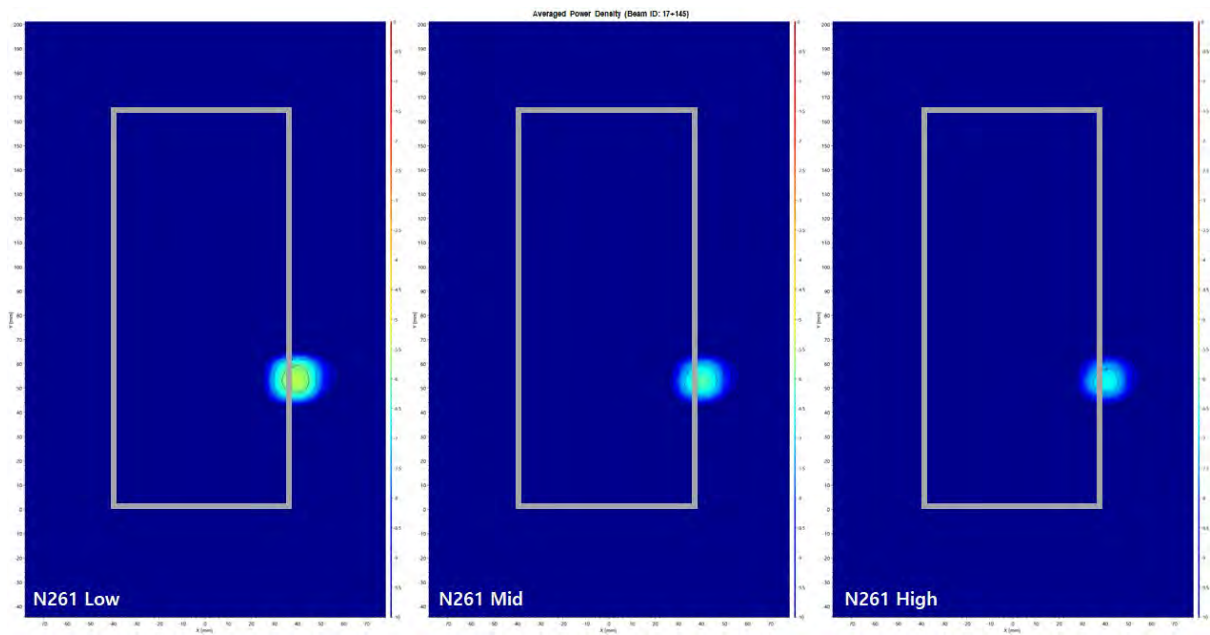
- n261 / Beam ID: 16+144 / Front surface



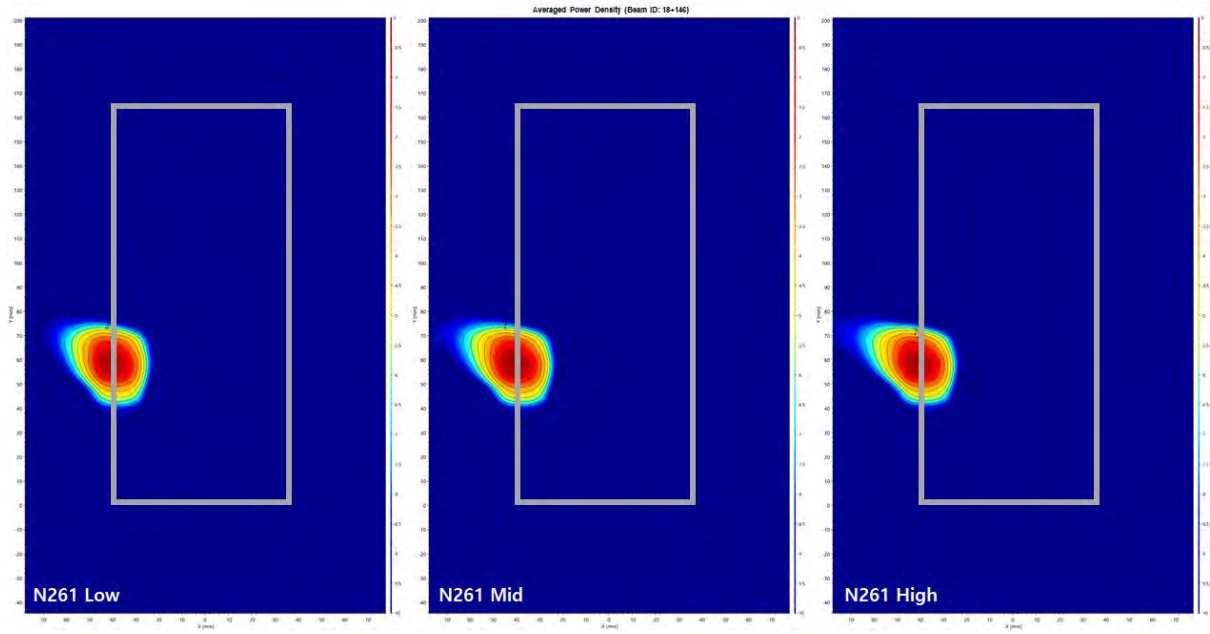
- n261 / Beam ID: 17+145 / Back surface



- n261 / Beam ID: 17+145 / Front surface



- n261 / Beam ID: 18+146 / Back surface



- n261 / Beam ID: 18+146 / Front surface

