

LABOTECH

TECHNICAL INFORMATION

TEST REPORT ON THE PERFORMANCE OF MARINE RADAR

Trade Mark : FURUNO

Model : FR-2155

Report no. : FLI 12-98-022
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All data herein contained is true and correct to our best knowledge.

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1 GENERAL INFORMATION

1.1 General

- (a) **Manufacturer:** Furuno Electric Co., Ltd.
Ashihara-cho 9-52, Nishinomiya-city, 662-8580 Japan
- (b) **Model:** FR-2155
Serial no.: 3387-0001
- (c) **Primary Function:** Search, navigation and anticollision
- (d) **Maximum Range Scale:** 96 nm
- (e) **Discrimination**
Range Discrimination: 25 meters on a range scale of 1.5 nm
Bearing Discrimination: Radiator Type, XN4A XN5A
1.18° 0.98°
on a range scale of 1.5 nm
- (f) **Minimum Range:** 25 meters on a range scale of 0.25 nm
- (g) **Frequency Range:** Fixed frequency, X-band
Type of Emission: P0N
- (h) **Power Supply:** 24 VDC (for Antenna Motor of Scanner Unit RSB-0050)
200 VAC, 50 Hz/220 VAC, 60 Hz, 3 ϕ (for Antenna Motor of Scanner Unit RSB-0049)
100/110/115/($\times$ 220/ $\times$ 230) VAC, 50/60 Hz, 1 ϕ (for Display Unit and Transceiver)
(*: external transformer required.)

1.2 Transmitter

- (a) **Assignable Frequency for Shipborne Radar:**
Between 9300 and 9500 MHz (FCC Rule § 80.375 (d)-(1))
- (b) **Type of RF Generator**
Magnetron Type: M4505E
Peak Output Power: 50 kW nominal
- (c) **Magnetron Ratings**
Center frequency of Magnetron: 9415 MHz
Tolerances
Manufacturing: ± 30 MHz
Pulling: 20 MHz
Tolerance for 20° C temperature variation: 5 MHz
- (d) **Guard Band:**

Guard Band is specified to be equal to $1.5/T$ MHz, where "T" is the pulselength in microseconds. See para (e). (FCC Rule § 80.209)

(e) Pulse Characteristics:

Pulse Type	Short	Middle 1	Middle 2	Long
Range Scale (nm)	0.125 0.25 0.5 0.75 (*) 1.5 (*) 3 (*)	0.75 (*) 1.5 (*) 3 (*) 6 (*)	3 (*) 6 (*) 12 (*) 24 (*)	6 (*) 12 (*) 24 (*) 48 96
Output pulselength (μs)	0.08	0.20	0.60	1.20
P.R.R. (Hz)	2200	1100	600	600
Duty cycle	1.76E-4	2.20E-4	3.60E-4	7.20E-4
Guard Band (MHz)	18.75	7.50	2.50	1.25

Note 1:(*) - Two (2) pulse types are selectable for each Range Scale.

2: Tests were carried out for the underlined Range Scales.

1.3 Modulator

- (a) Thyristor Type: SH16J12U
Trigger Voltage: Approx. +12 VDC positive

1.4 Receiver

- (a) Passband
RF Stage: 100 MHz
IF Stage:

Pulse Type	Short	Middle 1	Middle 2	Long
(MHz)	27	27	3	3

Video Amp. : 14 MHz

- (b) Gain (overall) (dB): Sufficient to cause limiting, approximately 130
- (c) Overall Noise Figure (dB): 6 (typical)
- (d) Video Output Voltage (V): 0.7 positive across 75 ohms
- (e) Features Provided: Sensitivity Time Controls (Anti-clutter Sea),
Fast Time Constant (Anti-clutter Rain)
- (f) If receiver is tunable, describe method of adjusting frequency:
Adjustment of tuning voltage of receiver local oscillator (Automatic and manual)

1.5 Display

- (a) Type: 21 (in.) multi-color, 16-level quantization
Rasterscan, non-interlace, 1280 X 1024 pixels
- (b) Size of Indicator Tube: 21 in. diagonal CRT
effective dia. 275 mm
- (c) Sweep Linearity: 2 % on all ranges
- (d) Range Scales:

Range (nm)	Number of Range Rings	Range Ring Interval (nm)
0.125	5	0.025
0.25	5	0.05
0.5	5	0.1
0.75	3	0.25
1.5	6	0.25
3	6	0.5
6	6	1
12	6	2
24	6	4
48	6	8
96	6	16

- (e) Range Ring Accuracy: Better than 1 % of maximum scale in use
or 15 m, whichever is the greater
- (f) Overall Bearing Accuracy from Scanner to Display:
Better than 1°

- (g) Target Plot Facility: Simulated afterglow in low shade
(h) Heading Indicator: Provided, automatic alignment. Heading Line and Heading Marker
(i) True Bearing Indicator: Provided

1.6 Antenna

- (a) Antenna Rotation ON-OFF Switch:
Provided.

- (b) Reflector: Slotted waveguide array,

Radiator Type	XN4A	XN5A
Length (cm)	250	320
Length (ft)	8.2	10

- (c) Type of Beam: Vertical fan

- (d) Beam Width (between half-Radiator power points)

Radiator Type	XN4A	XN5A
Horizontal	0.95°	0.75°
Vertical	20°	20°

- (e) Polarization: Horizontal

- (f) Antenna Gain:

Radiator Type	XN4A	XN5A
(dB)	31.5	33.0

- (g) Attenuation of Major Side Lobes with respect to main beam:

Radiator Type	XN4A	XN5A
Within $\pm 10^\circ$	-28 dB or less	-26 dB or less (*)
Outside $\pm 10^\circ$	-32 dB or less	-30 dB or less (*)

- (h) Scanning (rotating or Rotating over 360° continuously oscillating):
clockwise

- (i) Antenna Rotation Rate (rpm): 24 rpm (for RSB-0049/0050)

- (j) Number of Degrees Scanned: 360°

- (k) Sector Scan: Not provided. Sector blanking available.

- (l) Type of Transmission System: Contained in scanner unit

- (m) Rated Loss of Transmission System per hundred feet:

None. Transmission path is only in the antenna scanner unit.

1.7 Line Power Supply Requirements

- (a) Input Voltage: 24 VDC (for Antenna Motor of Scanner Unit RSB-0050)
200 VAC, 50 Hz/220 VAC, 60 Hz, 3 ϕ (for Antenna Motor of Scanner Unit RSB-0049)
100/110/115/($\times$ 220/ $\times$ 230) VAC, 50/60 Hz, 1 ϕ (for Display Unit and Transceiver)
(*: external transformer required.)
- (b) Power Drain: 15 W (for DC Antenna Motor)
90 VA (for AC Antenna Motor)
400 VA (for Display Unit and Transceiver)

1.8 Functional Controls

Range selector	Tune (manual)	EBL offset
INDEX LINE	Anti-clutter auto	Power Switch
A/C Sea control	Gain control	Panel dimmer
Heading line off	Echo stretch	MENU
Guard zone set/Audio alarm off	Range ring brilliance	Noise rejector on/off
Interference rejector	STBY/TX	Trackball (VRM,EBL,GUARD)
VRM on/off	Off-center (SHIFT)	A/C Rain control
Range set	Zoom	EBL on/off
Target trail	Brilliance (screen)	TRU/REL
Navigation on/off	Mark Brilliance	Function #1- #4
Range ring on/off	Text Brilliance	
ARPA function (option)		

1.9 Construction Features

- (a) Does equipment embody replacement units with chassis type assembly:
Yes
- (b) Are fuse alarms provided: Fuses are provided.
- (c) State units which are weatherproof: Scanner Unit (IEC 529 - IPX6)
- (d) If all units are not housed in a single container, indicate number and give description of individual units:
- | | | |
|-------------------------|-------|--------------------------------|
| 1 $\times$ Display Unit | Type: | RDP-124 |
| 1 $\times$ Scanner Unit | Type: | RSB-0049 (200/220 VAC, 24 rpm) |
| | | RSB-0050 (24 VDC, 24 rpm) |

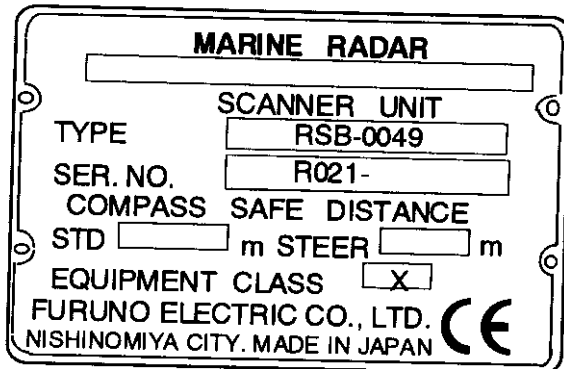


Fig. 2.4
Nameplate for Scanner Unit
(RSB-0049)

Note: Scanner Unit Type
Number changes to RSB-
0050 in case of 24 VDC set.

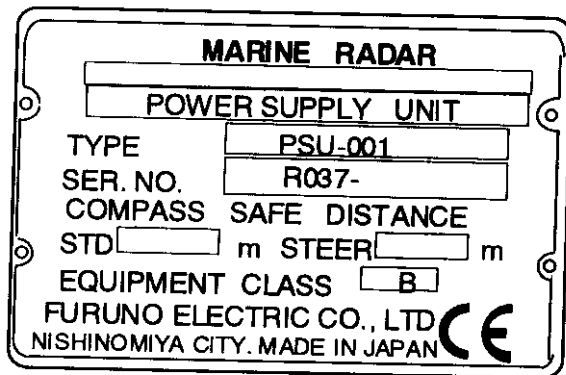


Fig. 2.5
Nameplate for
Power Supply Unit
(PSU-001)

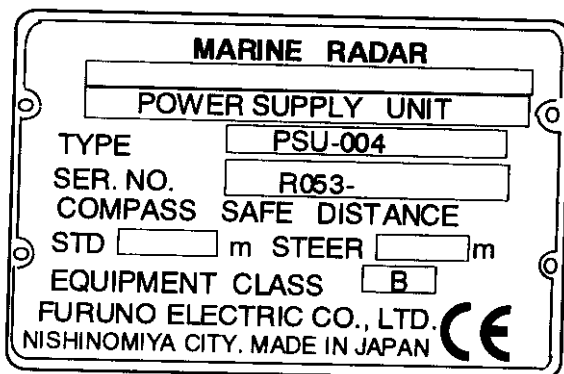


Fig. 2.6
Nameplate for
Power Supply Unit
(PSU-004)

3 RF POWER OUTPUT (FCC Rule §2.985)**3.1 Microwave characteristics**

The peak voltage was determined using the divider having a ratio of 1000 to 1 and the oscilloscope. Current pulse was viewed across the wideband current transformer with output voltage per ampere 1.00.

(1) Nominal values

Pulse Type	Short	Middle 1	Middle 2	Long
Range scale (nm)	0.125	3	12	96
Pulselength (μs)	0.08	0.20	0.60	1.20
PRR (Hz)	2200	1100	600	600
Duty cycle	1.76E-4	2.20E-4	3.60E-4	7.20E-4
Guard band (MHz)	18.75	7.50	2.50	1.25

(2) Measured values**Magnetron input pulse voltage**

Magnetron input pulse voltage was measured at its cathode using the oscilloscope and divider with ratio 1000 to 1.

Pulse Type	Short	Middle 1	Middle 2	Long
Directional coupler attenuation (dB)	50.98	50.98	50.98	50.98
Magnetron input voltage (kV)	12.0	12.0	12.0	12.0
Pulselength (μs) (50 % amplitude)	0.380	0.436	0.924	1.568
Rise time (μs) (10-90 % amplitude)	0.070	0.070	0.070	0.060
Decay time (μs) (90-10 % amplitude)	0.422	0.386	0.416	0.320

Magnetron input pulse current

Magnetron input pulse current was observed across the wideband current transformer with output voltage per ampere 1.00.

Pulse Type	Short	Middle 1	Middle 2	Long
Magnetron input	8.0	11.2	12.0	12.4

Pulse Type	Short	Middle 1	Middle 2	Long
current (A)				
Pulselength (μ s) (50 % amplitude)	0.092	0.154	0.616	1.292
Rise time (μ s) (10-90 % amplitude)	0.090	0.090	0.104	0.100
Decay time (μ s) (90-10 % amplitude)	0.100	0.157	0.180	0.340

RF envelope of the magnetron output pulse

The RF envelope of the magnetron output pulse was measured using a diode and the oscilloscope with the following results:

Pulse Type	Short	Middle 1	Middle 2	Long
Pulselength (μ s) (-3 dB points)	0.095	0.158	0.634	1.308
Rise time (μ s) (10-90 % amplitude)	0.020	0.018	0.052	0.052
Decay time (μ s) (90-10 % amplitude)	0.115	0.116	0.172	0.296

Estimated efficiency

The estimated efficiency of the RF generator (magnetron) was determined by the following measurements and calculation. Power output from magnetron was measured using the directional coupler, power meter and the oscilloscope.

Pulse Type	Short	Middle 1	Middle 2	Long
Range scale (nm)	0.125	3	12	96
PRR (Hz)	2191.4	1095.7	603.4	603.4
Duty cycle	2.08E-4	1.73E-4	3.82E-4	7.89E-4
Magnetron input, av. (W)	19.99	23.27	55.09	117.44
Magnetron input, peak (kW)	96.00	134.40	144.00	148.80
Power meter reading (mW)	0.054	0.041	0.116	0.248
Magnetron output, av. (W)	6.81	5.14	14.57	31.08
Spurious response limits (dB)	51.33	50.11	54.64	57.92
Magnetron Output, peak (kW):	32.69	29.68	38.10	39.38

Pulse Type	Short	Middle 1	Middle 2	Long
Magnetron efficiency (%) :	34.0	22.1	26.5	26.5

Peak Power Input to RF Generator : 130.8 kW

Estimated Efficiency of RF Generator : 27.3 %

4 MODULATION CHARACTERISTICS (FCC Rule § 2.987)

4.1 SCR Trigger Pulse

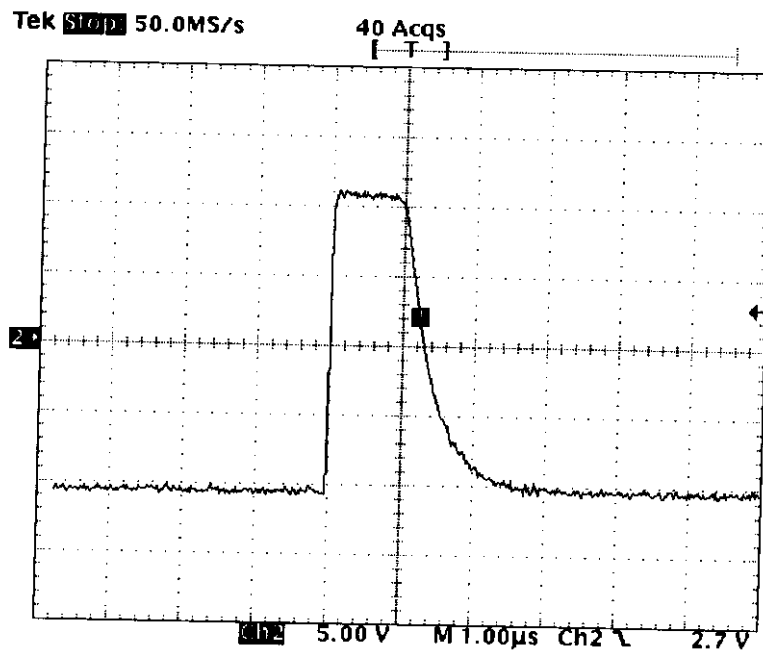


Fig. 4.1.1

Typical wave form of Trigger Pulse Scale: 5 V/div., 1 µs/div.
(NOTE: SCR trigger pulse is common to all ranges)

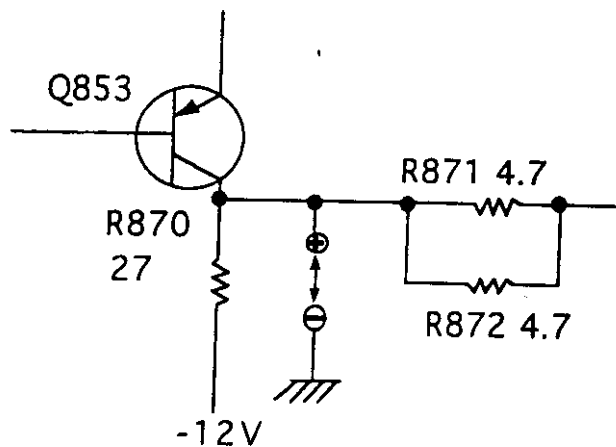


Fig. 4.1.2 Test Point for Trigger Pulse
(in RTB board (03P6666) of Scanner Unit (RSB-0049/0050))

4.2 Trigger Pulse at Magnetron Cathode

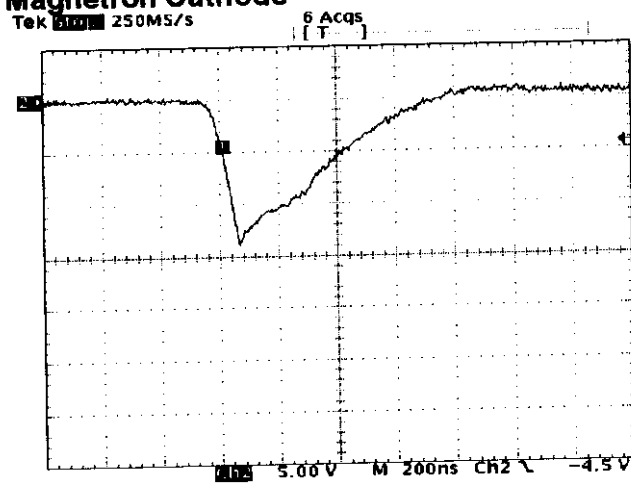


Fig. 4.2.1

Short Pulse (0.125 nm Range)

Scale: 5 kV/div. 200 ns/div.

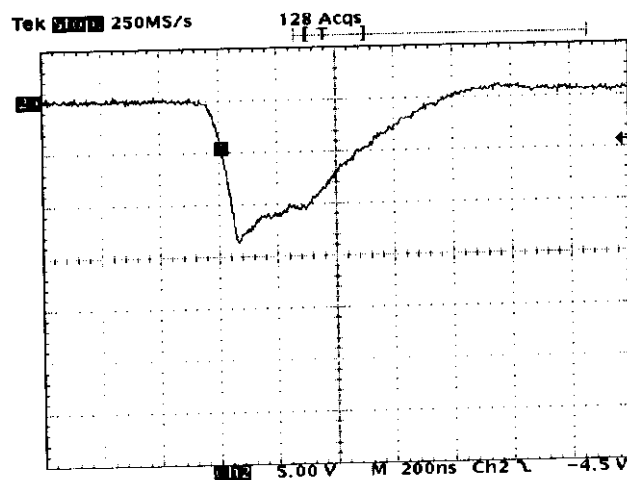


Fig. 4.2.2

Middle 1 Pulse (3 nm Range)

Scale: 5 kV/div. 200 ns/div.

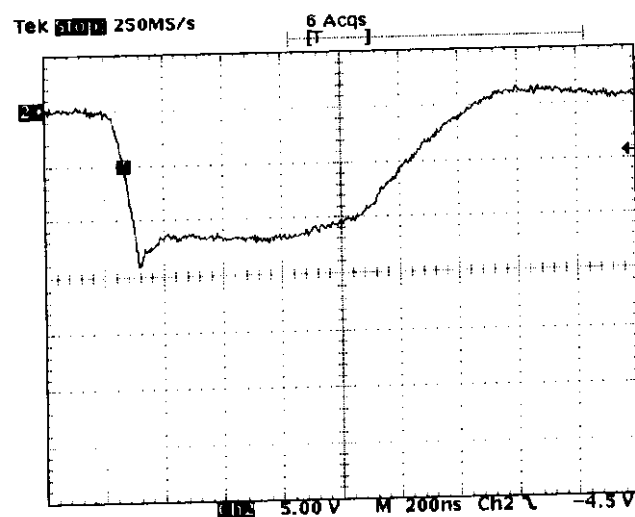


Fig. 4.2.3

Middle 2 Pulse (12 nm Range)

Scale: 5 kV/div. 200 ns/div.

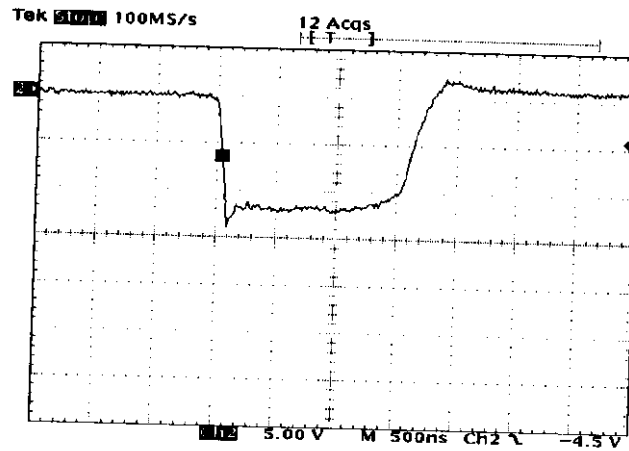


Fig. 4.2.4

Long Pulse (96 nm Range)

Scale: 5 kV/div. 500 ns/div.

4.3 Magnetron Output (detected):

4.3.1 Setup for Measurement:

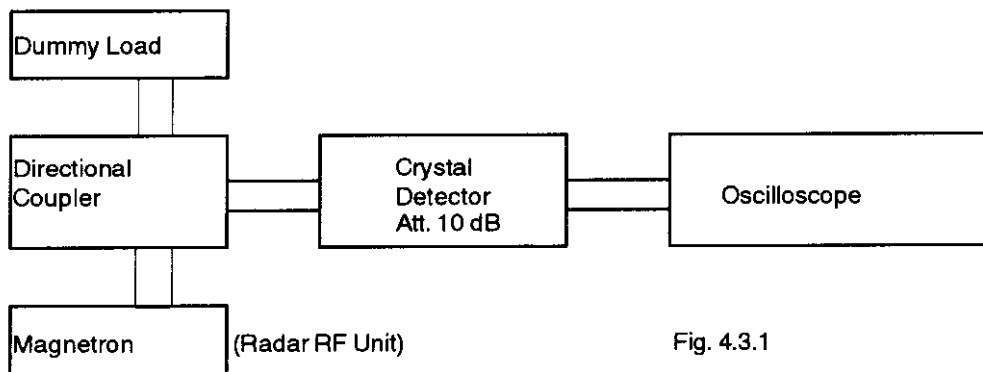


Fig. 4.3.1

4.3.2 Measuring Equipment List:

See ATTACHMENT 4 [LIST OF TEST/MEASURING EQUIPMENT].

4.3.3 Measured Data:

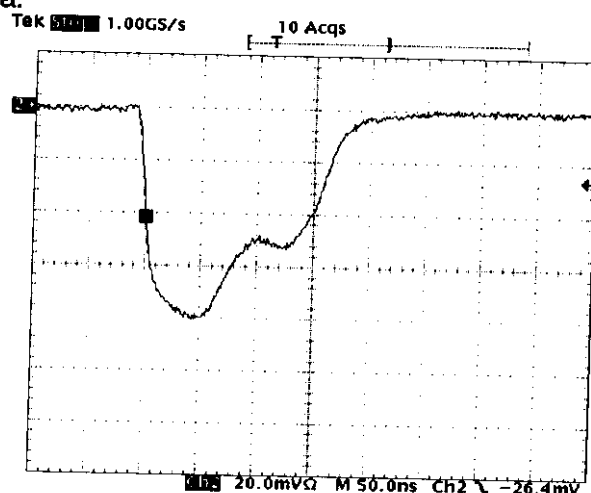


Fig. 4.3.2

Short Pulse (0.125 nm Range)

Scale: 20 mV/div. 50 ns/div.

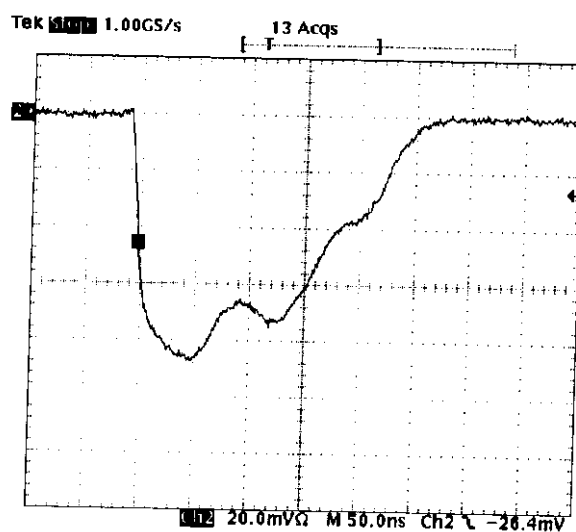


Fig. 4.3.3

Middle 1 Pulse (3 nm Range)

Scale: 20 mV/div. 50 ns/div.

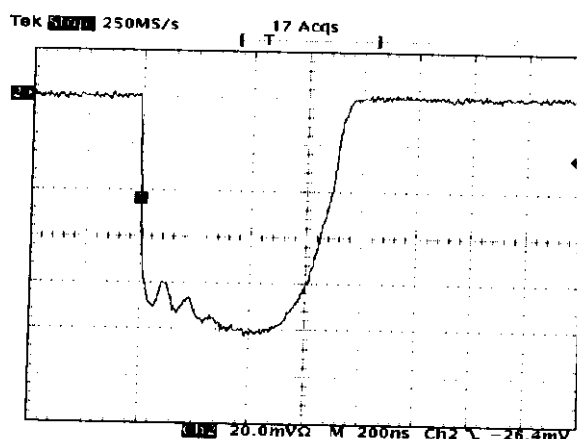


Fig. 4.3.4

Middle 2 Pulse (12 nm Range)

Scale: 20 mV/div. 200 ns/div.

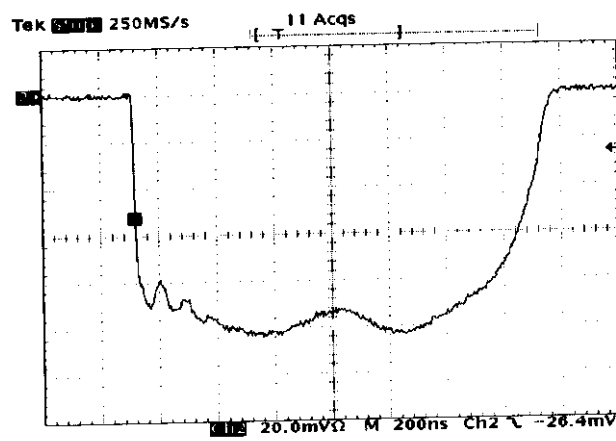


Fig. 4.3.5

Long Pulse (96 nm Range)

Scale: 20 mV/div. 200 ns/div.

4.4 Radar Pulse Spectrum:

Measured by the spectrum analyzer.

(Test Equipment Setup and Measuring Equipment List are same as Clause 6.1 and 6.2.)

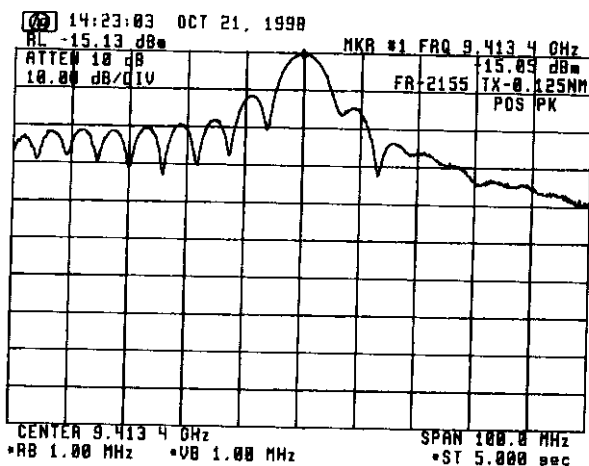


Fig. 4.4.1 For Short Pulse (0.125 nm Range)

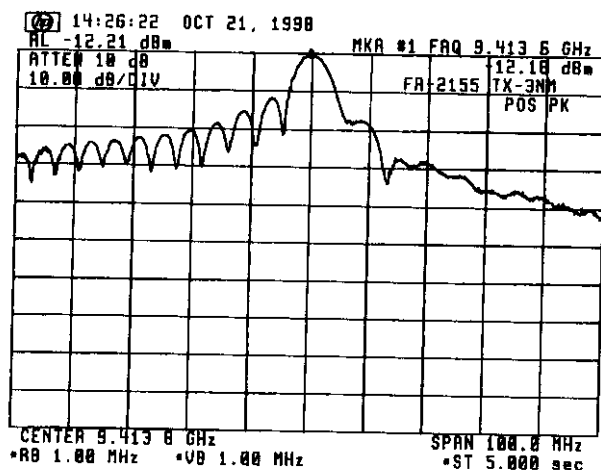


Fig. 4.4.2 For Middle 1 Pulse (3 nm Range)

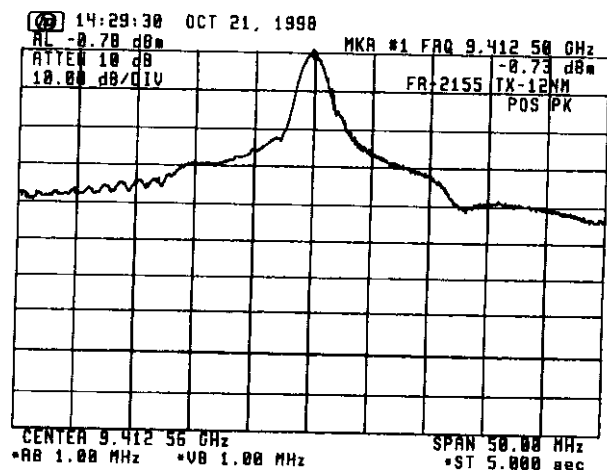


Fig. 4.4.3 For Middle 2 Pulse (12 nm Range)

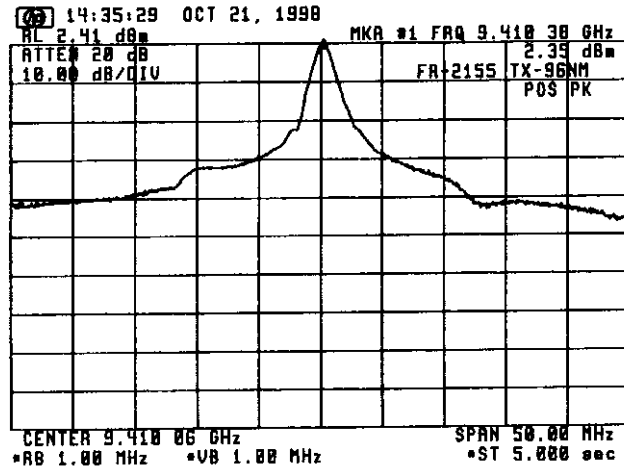


Fig. 4.4.4 For Long Pulse (96 nm Range)

5 OCCUPIED BANDWIDTH (FCC Rule §2.989)**5.1 Measuring Method**

FCC rule 47 CFR 2.989 requires measurements of the occupied bandwidth which is defined in the same section as "the frequency bandwidth such that, below its lower and above its upper frequency limits, the mean powers radiated are each equal to 0.5 percent of the total mean power radiated by a given emission."

To obtain the occupied bandwidth of the radar transmitter, a special program (program list shown below) was loaded to the Hewlett-Packard spectrum analyzer and run by entering the HP-provided POWER BANDWIDTH calculation command [PWRBW].

The result was automatically displayed on the screen on the spectrum analyzer as:

POWER_BW=----- MHz

```

10 ! HP_71000 DOWNLOAD PROGRAM
20 ASSIGN @Sa TO 718
30 CLEAR @Sa
40 CALL M_ain(@Sa)
50 LOCAL @Sa
60 END
70 !
80 SUB M_ain(@Sa)
90 M_ain: !
100 CALL Pwr_bw(@Sa)
110 CALL Limit_line(@Sa)
120 !
130 OUTPUT @Sa;"VARDEF K_ey,0;";
140 !
150 OUTPUT @Sa;"FUNCDEF D_LP,^";
160 OUTPUT @Sa;"MOV K_ey,0;";
170 !
180 Main_menu: !
190 OUTPUT @Sa;"REPEAT;";
200 OUTPUT @Sa;"READMENU K_ey;";
210 ! location: %Top---Bottom-%
220 OUTPUT @Sa;"1,%Limit line %, ";
230 OUTPUT @Sa;"2,%Power bw %, ";
240 OUTPUT @Sa;"14,% Exit%;";
250 !
260 OUTPUT @Sa;"IF K_ey,EQ,1;THEN;LIMIT_LINE;";
270 OUTPUT @Sa;"ELIF K_ey,EQ,2;THEN;PWR_BW;";
280 OUTPUT @Sa;"ELIF K_ey,EQ,14;THEN;ABORT;";
290 OUTPUT @Sa;"ENDIF;";
300 OUTPUT @Sa;"UNTIL K_ey,EQ,14;";
310 OUTPUT @Sa;"IP;TS;";
320 OUTPUT @Sa;"ADORT;";
330 OUTPUT @Sa;"^"
340 !
350 Define_keydef: !
360 OUTPUT @Sa;"KEYDEF 7,D_LP, %DLP TEST%;";
370 !
380 OUTPUT @Sa;"FUNCDEF D,^";
390 OUTPUT @Sa;"KEYPST;";
400 OUTPUT @Sa;"^"
410 !
420 SUBEND

430 !
440 SUB Limit_line(@Sa)
450 Limit_line: !
460 OUTPUT @Sa;"CLRDISP;";
470 OUTPUT @Sa;"FUNCDEF LIMIT_LINE,^";
480 OUTPUT @Sa;"PU;PA 0,654;";
490 OUTPUT @Sa;"LINET 1;";
500 OUTPUT @Sa;"PD;PA 100,654;";
510 OUTPUT @Sa;"PU;PA 201,654;";
520 OUTPUT @Sa;"PD;PA 300,654;";
530 OUTPUT @Sa;"PU;PA 105,630;";
540 OUTPUT @Sa;"TEXT @-35dB@;";
550 OUTPUT @Sa;"PU;PA 205,720;";
560 OUTPUT @Sa;"TEXT @-25dB@;";
570 OUTPUT @Sa;"PU;PA 301,743;";
580 OUTPUT @Sa;"LINET 1;";
590 OUTPUT @Sa;"PD;PA 400,743;";
600 OUTPUT @Sa;"PU;PA 601,743;";
610 OUTPUT @Sa;"LINET 1;";
620 OUTPUT @Sa;"PD;PA 700,743;";
630 OUTPUT @Sa;"PU;PA 701,654;";
640 OUTPUT @Sa;"LINET 1;";
650 OUTPUT @Sa;"PD;PA 1000,654;HD;";
660 OUTPUT @Sa;"^"
670 SUBEND
680 SUB Pwr_bw(@Sa)
690 Pwr_bw: !
700 ! Calculating Power band width
710 OUTPUT @Sa;"VARDEF P_bw,0;";
720 OUTPUT @Sa;"FUNCDEF PWR_BW,^";
730 OUTPUT @Sa;"CLRWA TRA;";
740 OUTPUT @Sa;"CLRDISP;";
750 OUTPUT @Sa;"SNGLS;";
760 OUTPUT @Sa;"MXMH TRA;TS;TS;TS;";
770 OUTPUT @Sa;"MOV P_bw,PWRBW TRA,99.0;";
780 OUTPUT @Sa;"DIV P_bw,P_bw,1000000;";
790 OUTPUT @Sa;"PU;PA 10,800;HD;";
800 OUTPUT @Sa;"TEXT @POWER BW = @;";
810 OUTPUT @Sa;"DSPLY P_bw,8,3;";
820 OUTPUT @Sa;"TEXT @ MHz @;";
830 OUTPUT @Sa;"^"
840 SUBEND

```

Fig. 5.1

Program for Calculation of Occupied Bandwidth

5.2 Test Equipment Setup:

Same as Clause 6.1.

5.3 Measuring Equipment List:

Same as Clause 6.2.

5.4 Test Result:

The test result is shown below.

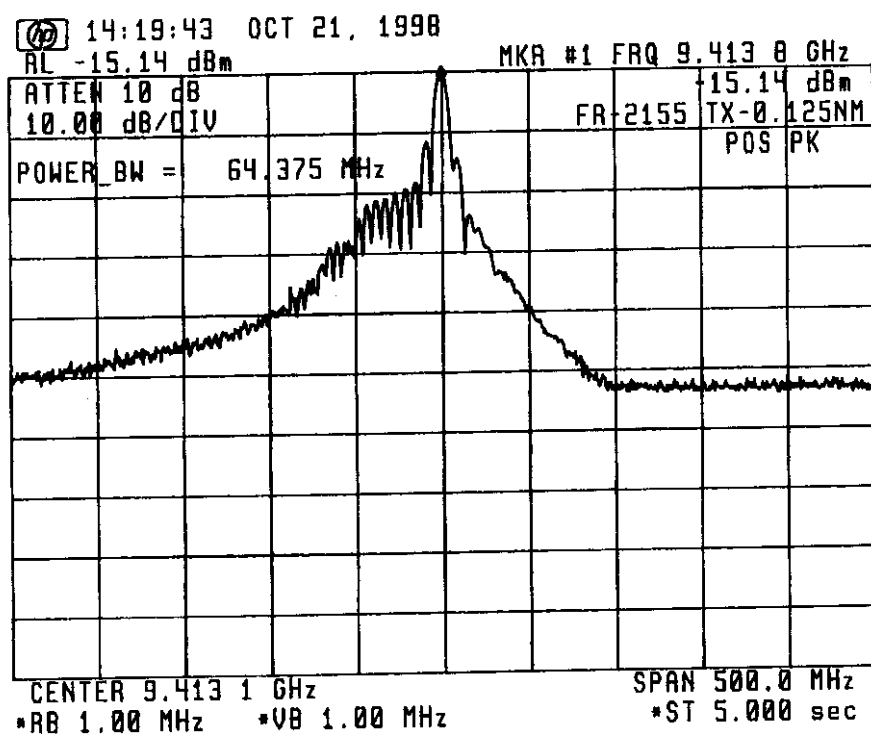


Fig. 5.2 Measurement of Occupied Bandwidth

Occupied bandwidth = 64.375 MHz

6 SPURIOUS EMISSIONS AT ANTENNA TERMINAL (FCC Rule § 2.991)

6.1 Test Equipment Setup:

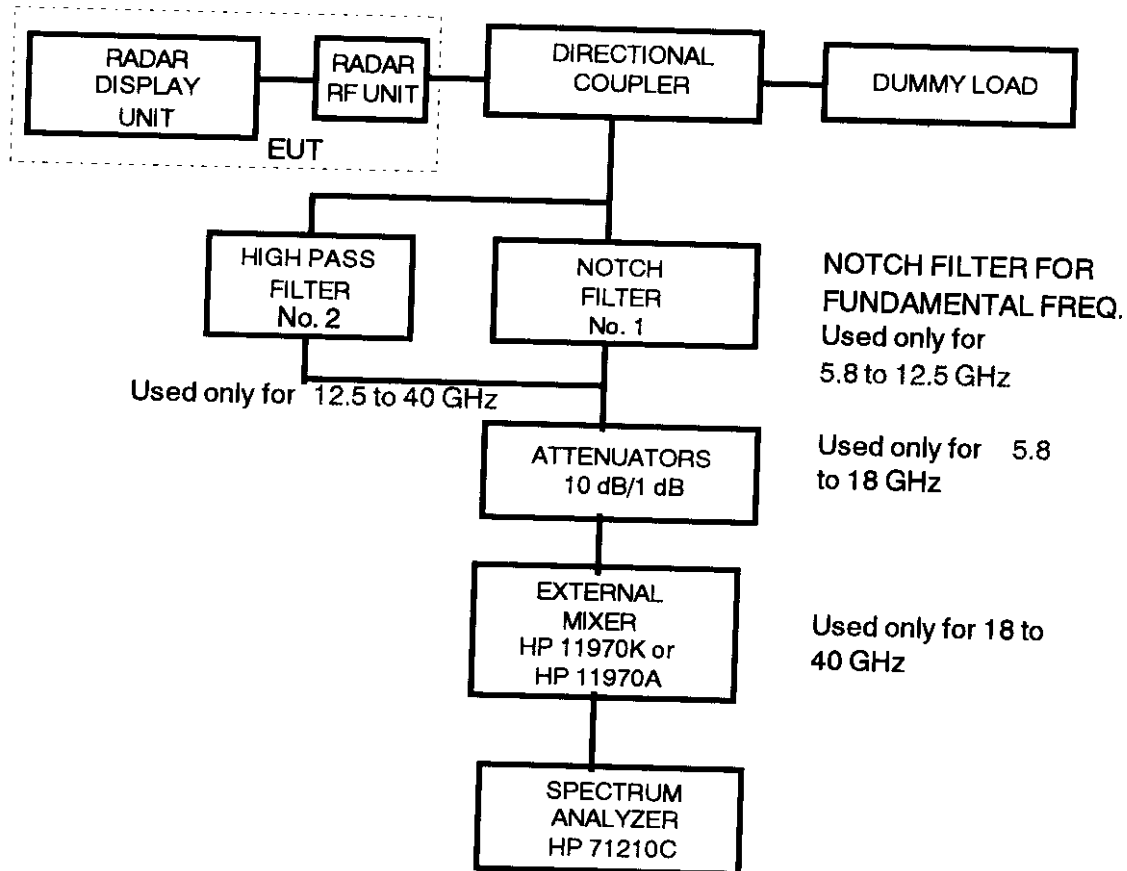


Fig. 6.1

6.2 Measuring Equipment List:

See ATTACHMENT 4 [LIST OF TEST/MEASURING EQUIPMENT].

- Note : (1) The characteristics of Notch Filter (No. 1) are described in Fig. 6.2 to Fig. 6.5.
(2) The characteristic of High Pass Filter (No. 2) is described in Fig. 6.6.

6.3 Test Conditions:

Radar Range Settings: 0.125 nm (Short)/ 3 nm (Middle 1)/ 12 nm (Middle 2)
96 nm (Long)

6.4 Emission Limits:

- (a) Frequency Range (FCC Rule § 2.997) : 10 kHz - 40 GHz
(b) Emission Limits (FCC Rule § 80.211) :

Frequency removed from the assigned frequency	Frequency (Hz)	Emission attenuation (mean power ,dB)
50 - 100 % (of the authorized bandwidth)	9310 - 9360 M	At least 25
	9460 - 9510 M	
100 - 250 %	9160 - 9310 M	At least 35
	9510 - 9660 M	
more than 250 %	10 k - 9160 M	At least $43 + 10 \log 10$ (mean power in watts)
	9660 - 40,000 M	

- Note : (1) Assigned frequency (center frequency) = 9415 MHz
(2) Authorized bandwidth = 100 MHz

6.5 Test Results:

As shown in ATTACHMENT 1 , the spurious emissions at antenna terminal of EUT are found lower than the specified limits.

(Note: Spurious emissions for 10 kHz to 5 GHz are not found due to the antenna terminal structure. (wave guide tube)).

Characteristic of Filter No. 1 (for X-band)

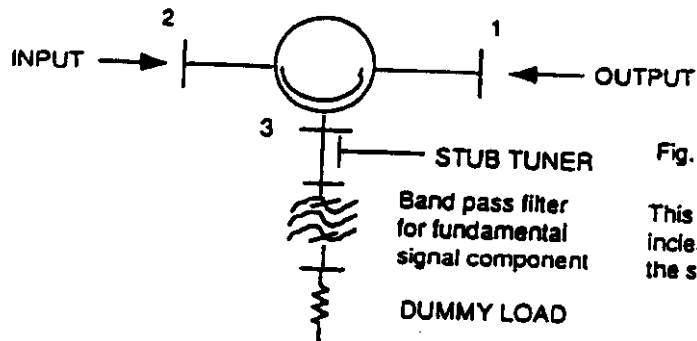


Fig. 6.2 Setup of Notch Filter No.1

This notch filter is used to increase the dynamic range of the spectrum analyzer

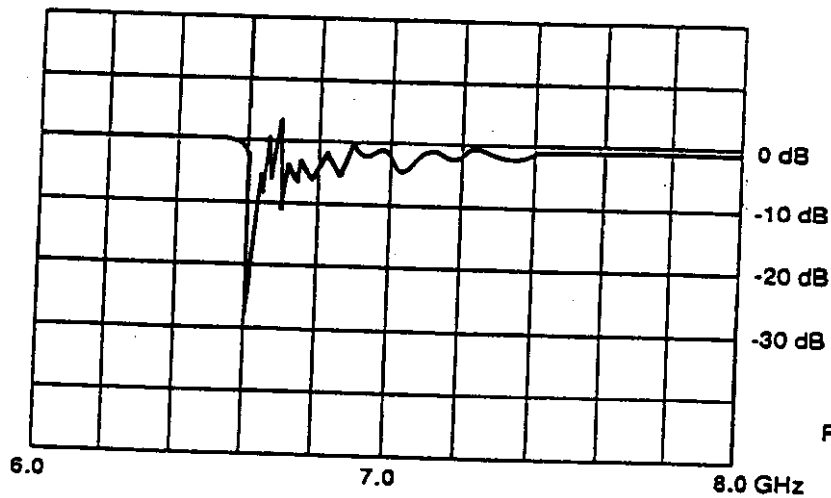


Fig. 6.3

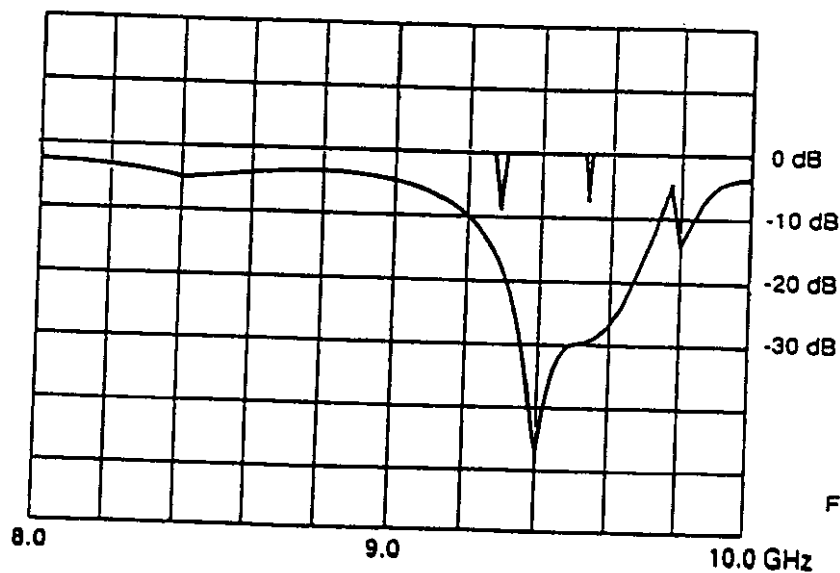


Fig. 6.4

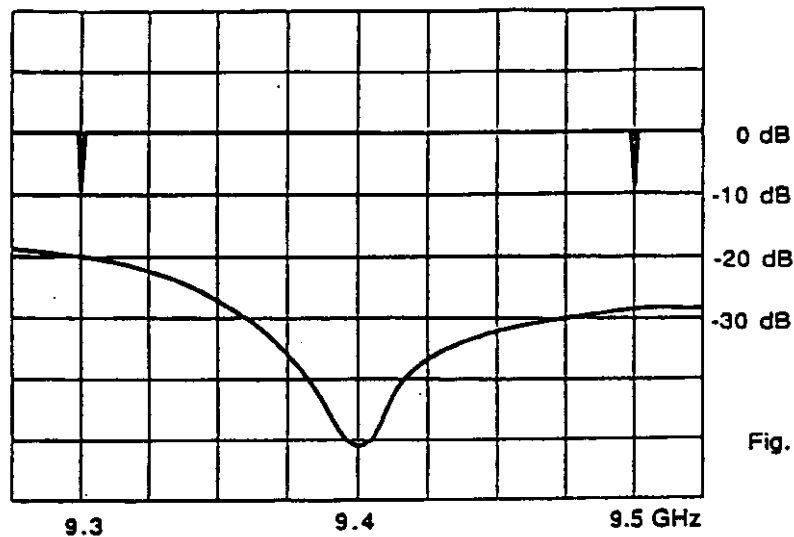
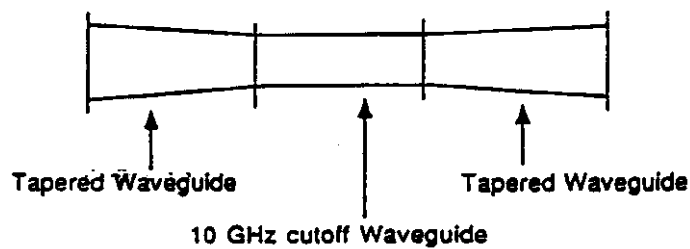


Fig. 6.5

Characteristic of Filter No. 2 (for X-band)



This filter is used to filter out the high level fundamental signal to avoid damage to the analyzer.

High Pass Filter Construction

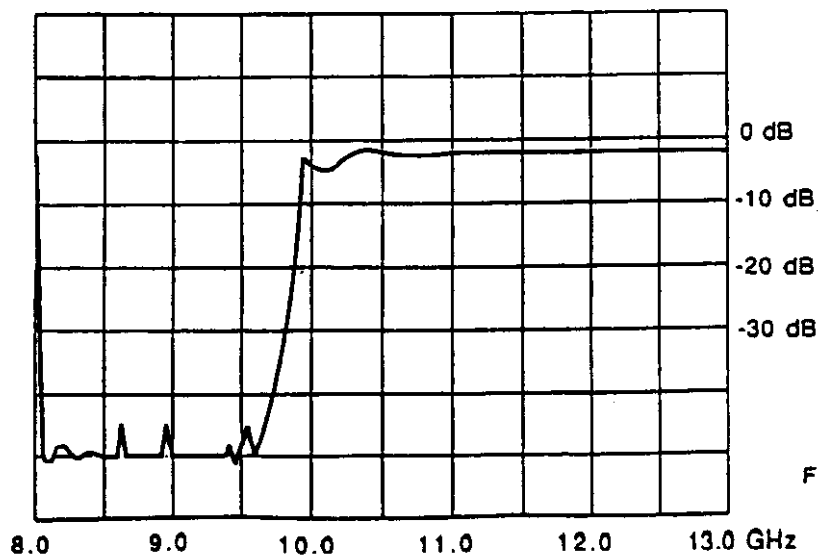


Fig. 6.6

7 FIELD STRENGTH OF SPURIOUS RADIATION (FCC Rule § 2.993)

7.1 **Test Site:** Rooftop of 6-story building,
FURUNO ELECTRIC CO., LTD.
Ashihara-cho 9-52, Nishinomiya-city, 662-8580 Japan

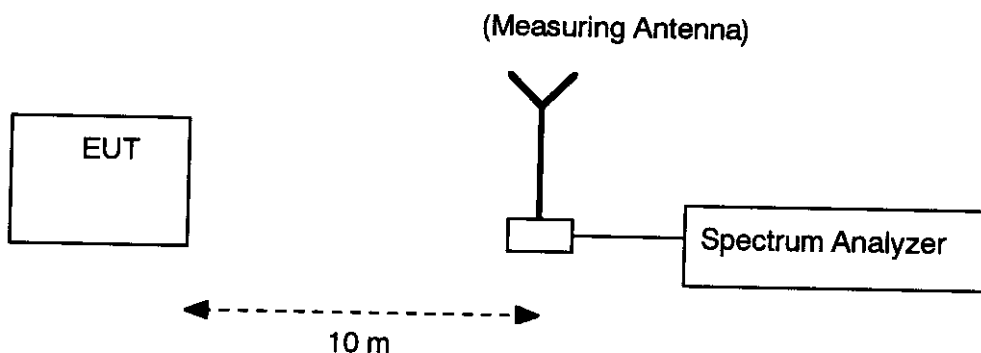
7.2 **Date:** Oct., 1998

7.3 **Distance between the radar set and measuring antenna:** 10 m

7.4 **Radar Range settings:** 0.125 nm (Short)/ 3 nm (Middle 1)/ 12 nm (Middle 2)
96 nm (Long)

7.5 **Measuring Equipment List:**
See ATTACHMENT 4 [LIST OF TEST/MEASURING EQUIPMENT].

7.6 **Test settings:**



7.7 Field Strength Limits:

(a) Frequency Range (FCC Rule § 2.997) : 10 kHz - 40 GHz

(b) Emission Limits (FCC Rule § 80.211) :

Frequency removed from the assigned frequency	Frequency (Hz)	Emission attenuation (mean power ,dB)
50 - 100 % (of the authorized bandwidth)	9310 - 9360 M	At least 25
	9460 - 9510 M	
100 - 250 %	9160 - 9310 M	At least 35
	9510 - 9660 M	

Frequency removed from the assigned frequency	Frequency (Hz)	Emission attenuation (mean power ,dB)
more than 250 %	10 k - 9160 M 9660 - 40,000 M	At least $43 + 10 \log 10$ (mean power in watts)

Note : (1) Assigned frequency (center frequency) = 9415 MHz

(2) Authorized bandwidth = 100 MHz

7.8 Test Results:

As shown in ATTACHMENT 2 , the field strengths of spurious radiation generated by EUT are found lower than the specified limits.

8 FREQUENCY STABILITY (FCC Rule § 2.995)

8.1 Setup for Measurement

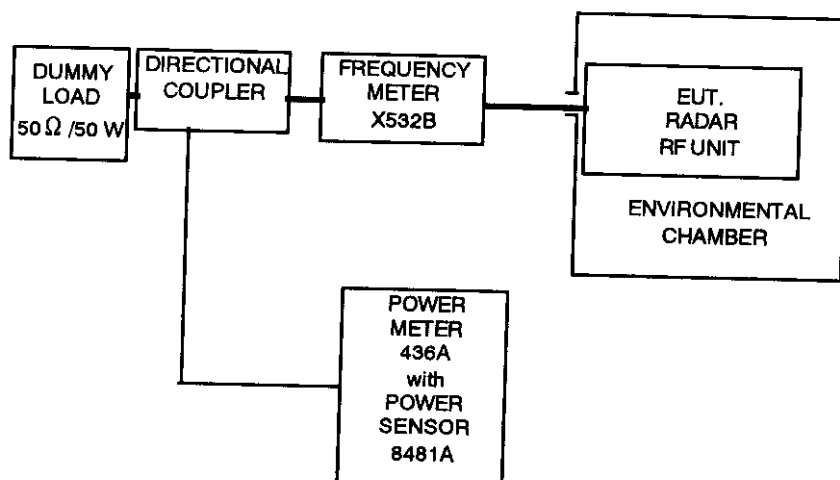


Fig. 8.1

8.2 Test Conditions:

- 1) Radar Range settings : 0.125 nm (Short)/3 nm (Middle 1)/ 12 nm (Middle 2)
96 nm (Long)
- 2) Ambient Temperature settings: - 20 to + 50 °C (10 °C step)
- 3) Power Supply Voltage settings: 85 /115 % of nominal voltage (85 to 115 VAC)

8.3 Measuring Equipment List:

See ATTACHMENT 4 [LIST OF TEST/MEASURING EQUIPMENT].

8.4 Frequency Tolerance Limits:

"The frequency at which maximum emission occurs must be within the authorized bandwidth and must not be closer than $1.5/T$ MHz to the upper and lower limits of the authorized band width, where "T" is the pulse duration in microseconds. "

(FCC Rule § 80.209)

1) Center frequency (f_0): 9415 MHz

2) Authorized bandwidth ($f(\text{AUBW})$): 100 MHz

"Upper limit frequency of the authorized band", $f(\text{UAUBW}) = f_0 + f(\text{AUBW})/2 = 9465$ MHz

"Lower limit frequency of the authorized band", $f(\text{LAUBW}) = f_0 - f(\text{AUBW})/2 = 9365$ MHz

3) Assignable frequency bandwidth : 200 MHz (between 9300 MHz and 9500 MHz)

(FCC Rule § 80.375 (d)-(1))

"Upper limit frequency of the assignable band", $f(\text{UASB}) = 9500$ MHz

"Lower limit frequency of the assignable band", $f(\text{LASB}) = 9300$ MHz

4) Guard Band ($f(1.5/T)$) :

Pulse Type	Short	Middle 1	Middle 2	Long
Range Scale (nm)	0.125	3	12	96
Pulse length (μ sec)	0.08	0.20	0.60	1.20
Guard Band $f(1.5/T)$ (MHz)	18.75	7.50	2.50	1.25

8.5 Test Results:

Shown on Fig. 8.2.

(1) "Upper Tolerance Frequency measured (at -20°C)", $f(\text{U}) = 9417.5$ MHz

(2) "Lower Tolerance Frequency measured (at $+50^\circ\text{C}$)", $f(\text{L}) = 9406.1$ MHz

(3)-(a)

$f(\text{U}) + \max. f(1.5/T) = 9436.3 \text{ MHz} < f(\text{UAUBW}) = 9465 \text{ MHz} \leq f(\text{UASB}) = 9500 \text{ MHz}$

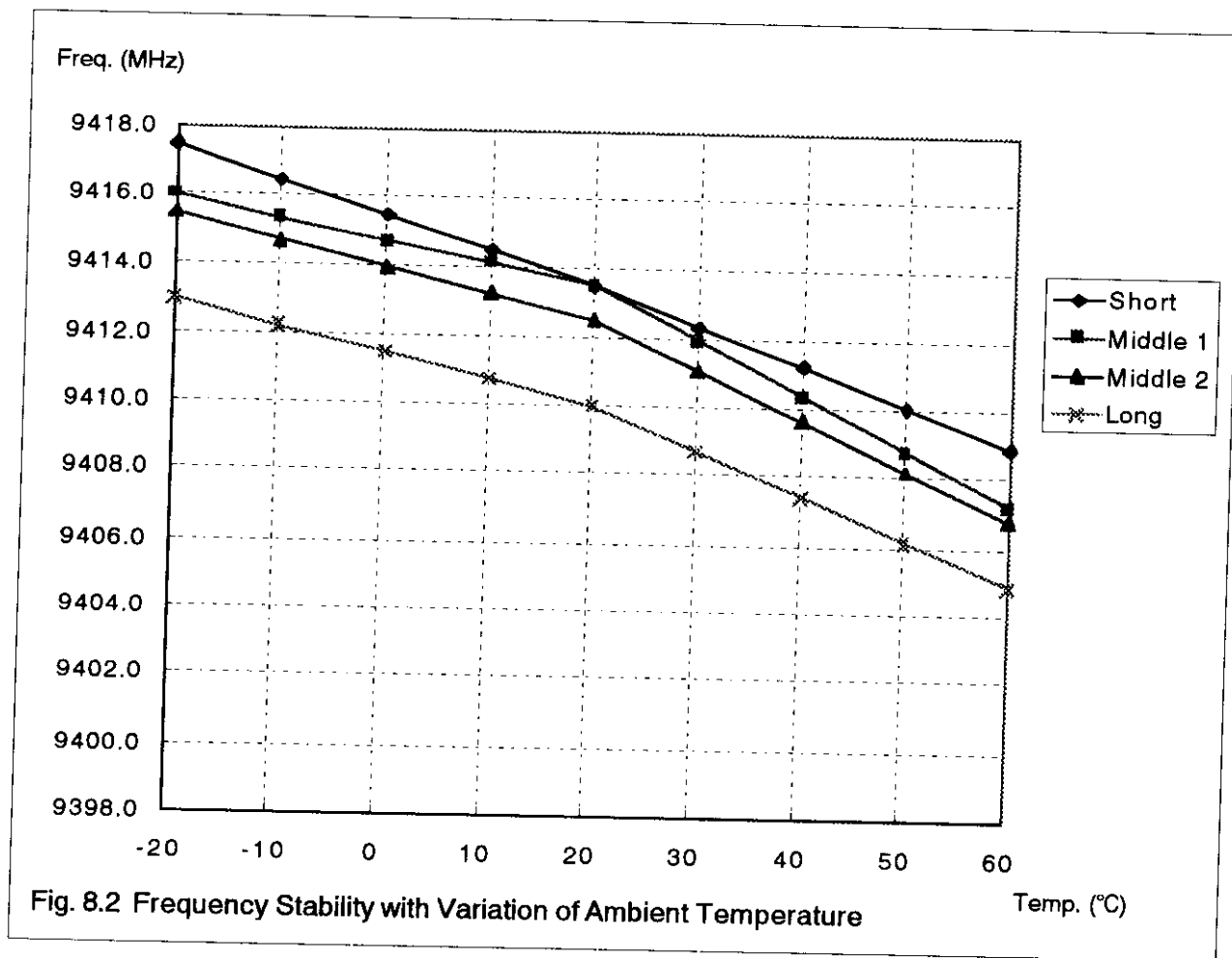
(3) - (b)

$f(\text{L}) - \max. f(1.5/T) = 9387.3 \text{ MHz} > f(\text{LAUBW}) = 9365 \text{ MHz} \geq f(\text{LASB}) = 9300 \text{ MHz}$

So, both are found within the specified limits.

FREQUENCY STABILITY WITH VARIATION OF PRIMARY SUPPLY VOLTAGE:

The built-in voltage regulator allows no frequency variation against variations of $\pm 15\%$ of nominal power supply voltage (85 to 115 VAC for nominal 100 VAC).



9 SUPPRESSION OF INTERFERENCE ABOARD SHIPS (FCC Rule § 80.217)

9.1 Measuring Antenna Characteristics at Representative Frequencies:

Whip antennas are used to determine the level of interference caused by the radar to shipboard receivers. These antennas have the following characteristics (refer to impedance charts attached):

Length	Test Frequency (Hz)	Impedance (Ω)	θ	R (Ω)	C or L
6 m	500.5 k	1 k	-90°	0	80 pF
6 m	1.992 M	1.25 k	-86°	87.2	64 pF
6 m	10.00204 M	158		109	140 pF
4 m	27.5 M	95		83.5	128 pF
5/8 λ	150 M	116.5		105.5	52.5 nH
1/4 λ	450 M	70.5		34.5	5.68 pF

9.2 Test Site: Rooftop of 6-story building,
Furuno Electric Company, Ltd.
Ashihara-cho 9-52, Nishinomiya-city, 662-8580 JAPAN

9.3 Measuring Instrument List:

See ATTACHMENT 4 [LIST OF TEST/MEASURING EQUIPMENT].

(Instruments for measuring antenna characteristics are listed below.)

- (1) RF Vector Impedance Meter, HP 4815A
- (2) Spectrum Analyzer, ADVANTEST TR4172
- (3) Spectrum Analyzer, HP 8566B
- (4) Antennas,
for 14 k - 10 MHz, 6 m whip
for 10 - 30 MHz, 4 m whip
for 30 - 300 MHz, VHF whip
for 300 - 1000 MHz, UHF whip

9.4 Test Results:

Interference levels to the respective antenna were measured at 2 m from the radar which was put in OFF, STANDBY, TRANSMIT conditions., and found within the specified limits.

9.4.1 Harmful Interference to Receiver (FCC Rule § 80.217 (a))

Limits: for 14 - 490 kHz, 5 μ V/m
 for 490 kHz - 1 GHz, 1 μ V/m

Results: There is no spurious component which is deemed harmful interference. (Test data are shown in ATTACHMENT 3)

9.4.2 Electromagnetic Field (FCC Rule § 80.217 (b) - 1)

Limits: for below 30 MHz, 0.1 μ V/m at 1 nm (-20 dB μ V/m)
 for 30 to 100 MHz, 0.3 μ V/m at 1 nm (-10.5 dB μ V/m)
 for 100 to 300 MHz, 1.0 μ V/m at 1 nm (0 dB μ V/m)
 for over 300 MHz, 3.0 μ V/m at 1 nm (9.5 dB μ V/m)

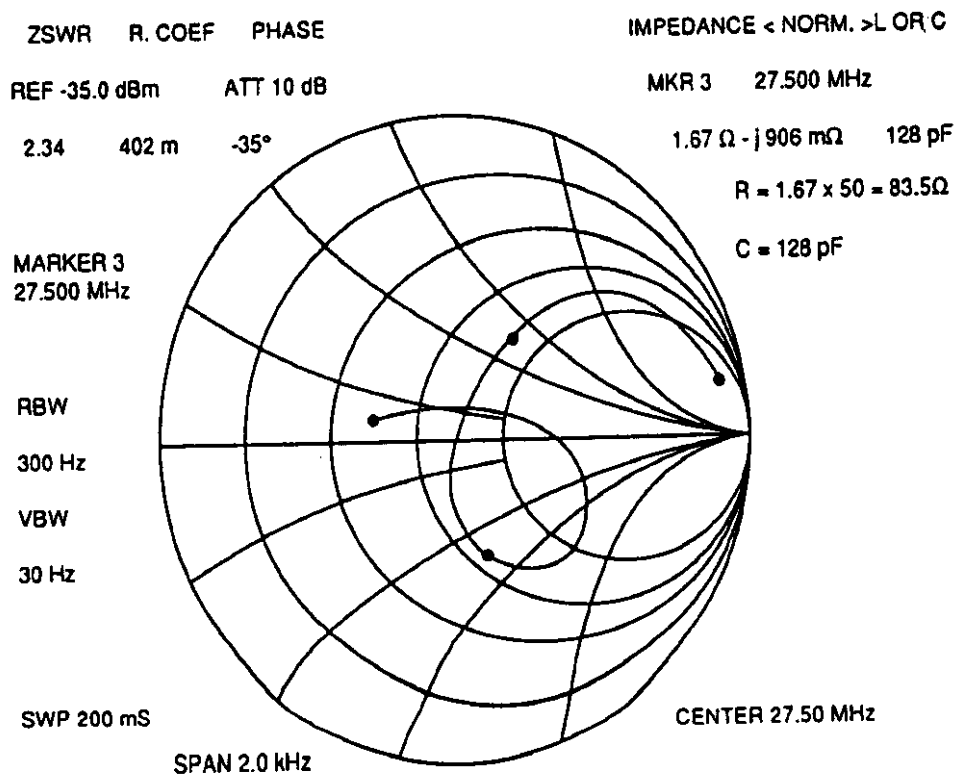
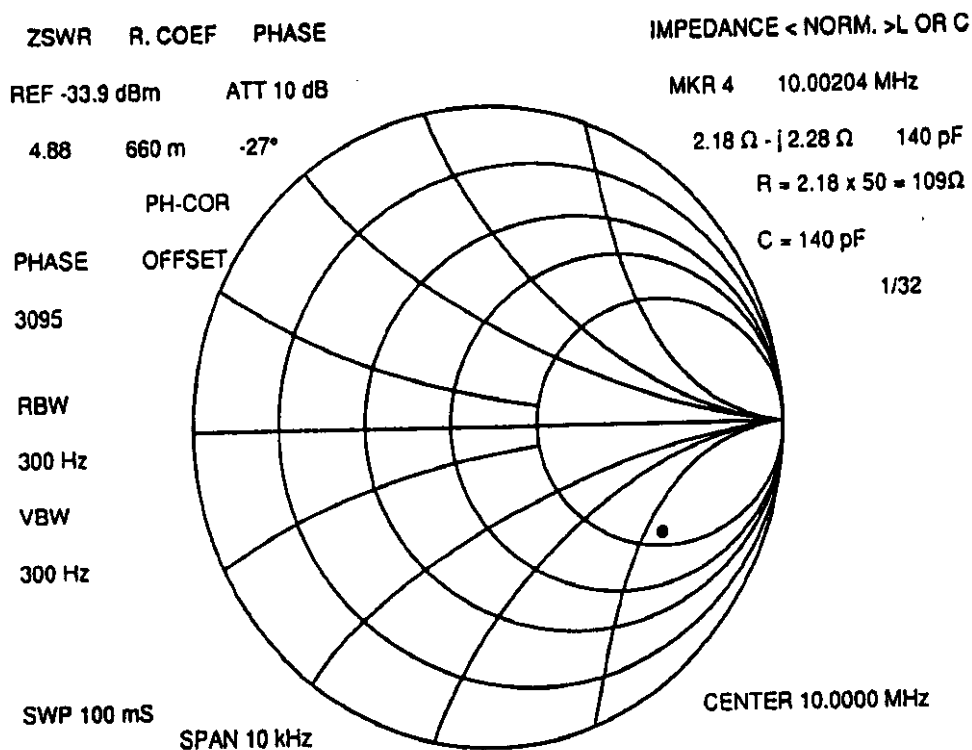
Results: Interference was measured with the antenna located 2 m from the radar and converted to levels at 1 nm. There is no spurious component exceeding the limits.
(Test data are shown in ATTACHMENT 3)

9.4.3 Power Input to an Artificial Antenna (FCC Rule § 80.217 (b) - 2)

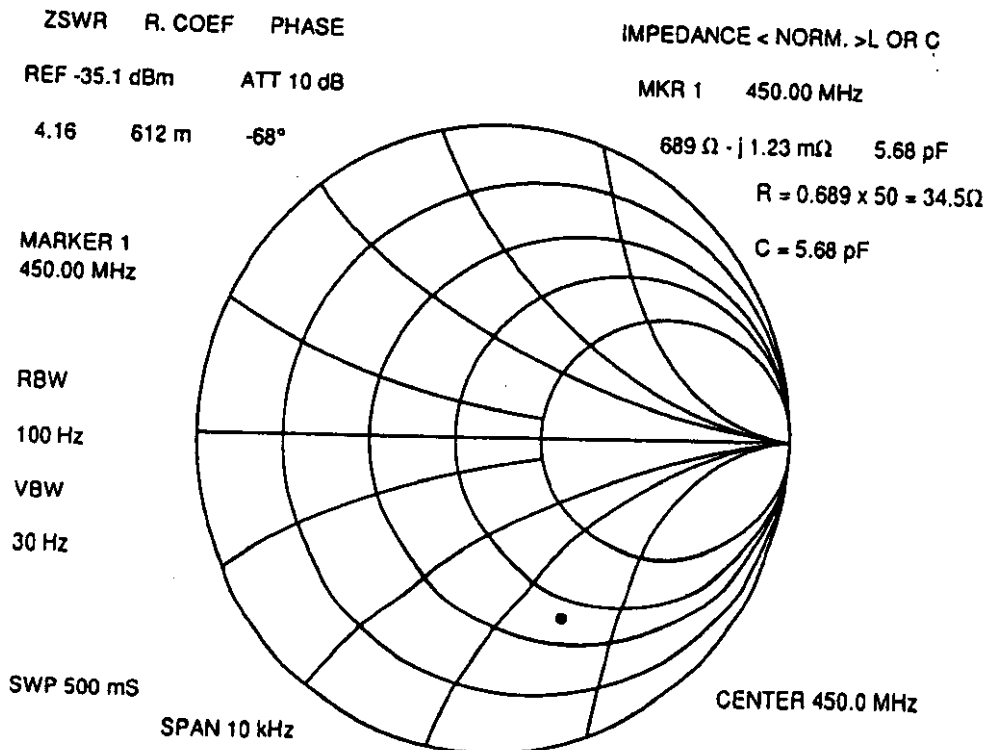
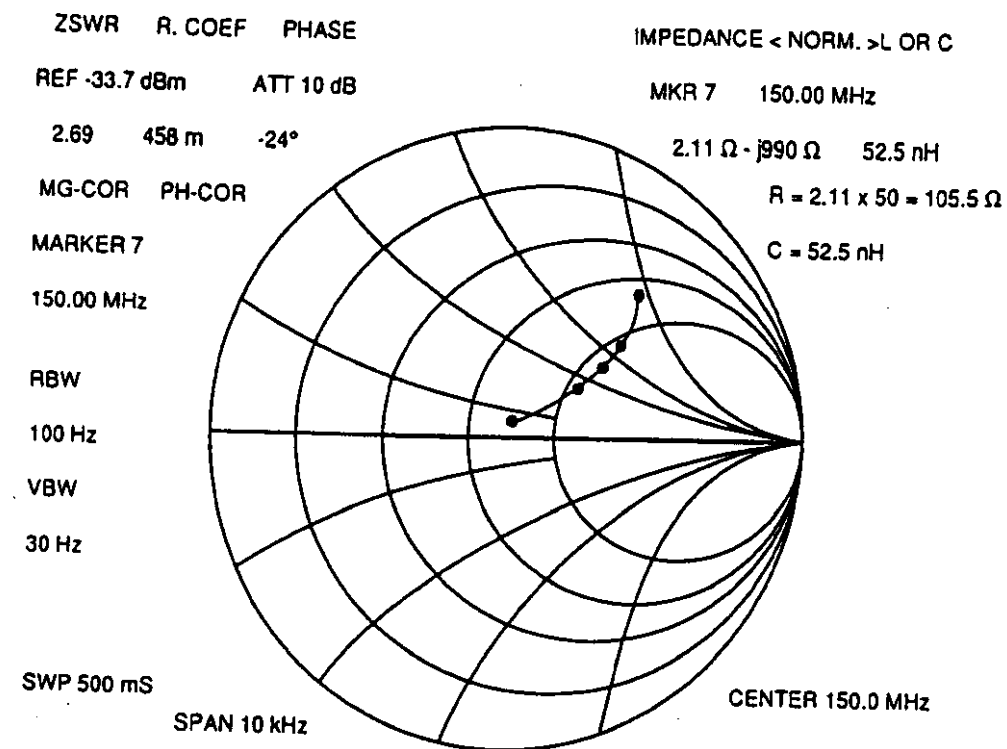
Limits: for below 30 MHz, 400 μ W
 for 30 to 100 MHz, 4,000 μ W
 for 100 to 300 MHz, 40,000 μ W
 for over 300 MHz, 400,000 μ W

Results: There is no spurious component exceeding the limits.
(Test data are shown in ATTACHMENT 3)

MEASUREMENT OF IMPEDANCE OF TEST ANTENNAS



MEASUREMENT OF IMPEDANCE OF TEST ANTENNAS



11 TECHNICAL DESCRIPTION OF EQUIPMENT (FCC Rules § 2.983)

11.1 Function of Each Semiconductor or Active Device (FCC Rule § 2.983 (d)(6))

ANTENNA UNIT

TRANSCIVER MODULE (RTR-030)

Modulator Trigger PCB 03P6666

CR850/CR851:	Switching
CR853:	Reverse Voltage Protection
CR854:	Switching
CR855 to CR858:	Reverse Voltage Protection
Q850:	SCR Driver
Q854:	Switching
Q884:	Current Amplifier
U850:	Monostable Multivibrator
U851:	AND Gate
U852/U853:	Inverter

Modulator PCBs 03P6668/03P6827/03P6669

CR801/CR802:	Charging
CR807:	Switching
CR816 to CR824:	SCR Protection
CR825:	Reverse Voltage Protection
CR840/CR842:	Switching

Chassis Mounted Parts

CR803 to CR805:	Relay Driver Protection
CR808/CR809:	Reverse Voltage Protection
CR810:	TR Limiter (BS4122/E3902)
CR813 to CR815:	SCR Switching
V801 :	Magnetron. microwave oscillator
HY801:	Circulator
U801:	MIC, frequency converter

IF Amplifier PCB 03P6570

CR601 to CR606:	Switching
CR608:	Thermal Sensor
CR609:	Level Shift
CR610 to CR613:	Switching
CR614:	Frequency Adjuster
CR615:	LED
CR616:	Temperature Compensation
CR617:	Tuning Voltage Limiter
CR618:	Voltage Regulator
Q601:	IF Amplifier
Q602:	Switching
Q603 to Q607:	Buffer Amplifier
Q608:	IF Switching
Q609:	IF Amplifier
Q610:	DC Amplifier
U601 to U610:	IF Amplifier
U611 to U614:	Voltage Regulator
U615:	MBS Pulse forming Network and Bandwidth Selector
U616:	Tuning Amplifier

Bearing Signal Generator PCB MP-3795

Q901/Q902:	Pulse Amplifier
U901:	Photo Interrupter
U902:	Comparator

Interface Board 03P9004

CR1 to CR3:	Switching
U1:	Comparator

11.2 Description of the circuits employed for suppression of spurious radiation, for limiting or shaping the control pulse, and for limiting or controlling power

(FCC Rule § 2.983 (d) (11))

ANTENNA UNIT

TRANSCEIVER MODULE (RTR-030)

Modulator Trigger Circuit 03P6666

The modulator trigger circuit consisting of Q850, Q854, Q853 and U850 generates pulses that fire SCRs CR813 thru CR815.

Normally the circuit is stable with Q850/Q853 off. Q850 turns on upon receiving the TX trigger from the display unit and a negative going pulse is produced at its collector. Then, a positive going pulse is produced at pin #6 of U850 and sent to Q854, and then a negative going pulse is generated at the collector of Q854. The negative going pulse is differentiated by C866 and R865, and then only a negative going differentiated waveform is applied to the base of Q853. As a result, a positive going pulse (Modulator Trigger Pulse) is produced at the collector of Q853 and delivered to the modulator SCRs.

The circuit made up of U850 and Q854 prevents the modulator from being fired by noise. The first stage of the one-shot multivibrator U850 operates immediately after the TX trigger pulse, then the second stage of U850 operates. The output (#9) of U850 is applied to the reset terminal (#3) of the first stage of U850. In this manner, the level at pin #6 of U850 is kept "L" while the level at pin #9 of U850 is "L". Therefore, even if noise appears after the TX trigger pulse, Q853 is kept off.

The circuit made up of U852 and U853 is a decoder to drive the relays for changing the TX pulse length depending on the setting of the RANGE selectors and MENU functions of Display Unit.

Modulator

The function of the modulator is to produce a narrow high tension pulse that drives the magnetron. It is composed of a line-type-pulser.

L801 is a charging choke, which forms a series resonant Circuit with the pulse forming network (PFN) consisting of C811 thru C824, and L811. The TX high voltage in the input is doubled by the electromotive force of this coil and the PFN is charged up twice the input voltage. The time taken for

full charge is roughly given by the equation $T = 2\pi\sqrt{L \times C}$, where L represents the L801 and C capacitance of the PFN.

The PFN is a lumped constant L-C circuit, which is an application of parallel two-line circuits with an open end. The modulation pulse that drives the magnetron is developed when the energy in the PFN discharges through CR813 thru CR815. The duration of the pulse is equal to the time required for the voltage wave to go and return in the L-C network, and it is given by the duration $t = 2\pi N\sqrt{L \times C}$, where N is the number of sections of the PFN.

CR801 and CR802 prevent the energy stored in the PFN from discharging to the input line. The advantage of employing CR801 and CR802 is that they allow a wide choice of CR813 thru CR815 firing timing and efficient utilization of the stored energy: CR813 thru CR815 can be fired at anytime after the PFN has been charged to a peak point and fluctuation of trigger timing does not affect the amplitude of the resultant pulse.

The pulse transformer T801 boosts up the pulse produced by the PFN. Since the characteristic impedance of the PFN and the input impedance of T801 is matched (about 3 ohms), a pulse with half the network voltage is developed across T801's primary winding. T801 boosts this pulse up by 18 times and applies the resultant output to the magnetron.

L801 is a switching coil. This conducts after CR813/CR814/CR815 turn on completely in order to minimize heat energy loss. CR816/CR817/CR818 and R816/R817/R818 absorb the counter electromotive force that develops the moment CR813/CR814/CR815 from damage. C804 decouples the pulse energy that is liable to occur across the magnetron heater when T801 secondary windings are unbalanced or the load is asymmetric.

Duplexer and Mixer

Since the radar system uses a single antenna for transmission and reception, an efficient device is required for switching between the transmitter and the receiver. This radar employs a circulator (HY801) for this purpose.

The circulator HY801 is a passive directional coupler with three ports. It contains a permanent magnet and a core of ferrite material and bends the electromagnetic waves in a specific direction. The microwave energy produced by the magnetron enters the circulator from port 2. It is bent in the specific direction and emerges from port 3 with a little loss, port 1 being isolated. In the same manner, the received signal entering into port 3 is transferred to port 1 , isolating port 2. This operation of the circulator protects the receiver during transmitting and minimizes the loss of the received signal during

reception.

The received microwave signal from the circulator is delivered to the TR limiter (CR810), which is composed of a gas filled primerless switching tube and a varactor limiter. It is a passive device and no electrode is provided. During transmission it serves as a barrier to protect the MIC from high RF power generated by the magnetron.

The RF energy from the magnetron ionizes the gas in the switching tube, and the switching tube behaves like a short-circuit across the waveguide. Leakage energy from the switching tube is further attenuated by the varactor limiter.

During the receiving period, echoes being received by the antenna and entering the waveguide are considerably weaker and the gas in the switching tube remains de-ionized. In this time, echoes pass through the varactor limiter to the MIC without any attenuation.

Since the TR limiter is a passive device, it can protect the MIC from strong signals transmitted from other radars operating in the close proximity even while the radar is switched off.

U801 is a microwave IC (MIC) incorporating a local oscillator and mixer diodes. The received microwave signal of 9415 MHz coming from the TR limiter is mixed with the local oscillation signal in the mixer diodes and converted to IF signal of 60 MHz.

IF Amplifier 03P6734

The IF signal of 60 MHz coming from the MIC is amplified and converted into a video signal, which is delivered to the Display Unit.

The IF amplifier is composed of 5 major circuits; Linear Amplifier (Q601), Logarithmic Amplifier (U601 to U610), Video Amplifier (Q606/Q607), MBS pulse forming network, Bandpass Selector (Q615) and Tuning Indicator Circuit (U616).

The IF amplifier operates in either narrow or wide bandwidth mode depending on the settings of the RANGE selector and TX touchpad. For short ranges, a wide bandwidth (27 MHz) is selected as pin 10 of U615 Becomes low. Thus, CR602 to CR605 are conductive and CR601/CR606 are cut off, causing the signal to pass through CR603/CR604. On the contrary, CR602 to CR605 are cut off and CR601/CR606 are conductive, which causes the signal to pass through T603/T604, selecting a narrow bandwidth (3 MHz) on middle and long ranges.

The signal through the bandpass selector is coupled to the logarithmic amplifier and amplified by

U601 to U607 and Q603/Q604. Thus, the output signals of Q603/Q604 are fed to Q606/Q607 to be amplified further, and then sent to the Display Unit.

The IF signal of 60 MHz is amplified by Q609/U610. Then the detected signal (Turning Indicator Signal) is sent to the Display Unit via U616.

On the other hand, Q609/U610 and U608/U609 are additional amplifier circuits to make the dynamic range of the IF signal wider, causing the discrimination of the target echoes to get better. The IF signal from the MIC is fed to Q609 as well as through resistors R639/R640 which are employed to attenuate the signal level.

Therefore, Q609/U610 amplifies even a strong signal which may be saturated in Q601/Q602 and U601 to U607, and then sent to logarithmic amplifier U608/U609. This signal is added to the saturated signal in U601 to U607, causing the saturation level of the IF signal to become high.

The MBS (Main Bang Suppression) waveform is fed to pin 1 of U616 to eliminate the strong transmission signal (main bang).

Bearing Signal Generator MP-3795

The bearing signal generator produces a square wave signal that is used to synchronize the sweep rotation with that of the antenna.

U901 is a photo interrupter composed of a light emitting diode and a photo transistor. It has a U-shaped construction. The light emitting diode is mounted on one wall of the "U" shape and the photo transistor on the other wall. A rotating timing disc is arranged between the two walls.

The timing disc is provided with 60 slits at regular intervals along its circumference. It is fitted on the scanner motor shaft and rotates at a speed of 144 rpm.

The photo transistor receives the light emitted by the light emitting diode thru each slit of the timing disc and converts it into electric currents. The output of the photo transistor across R903 is a half-rectified sine wave at a frequency of 144 kHz. This signal is amplified, reshaped and sent to the Display Unit for display echo synchronization.

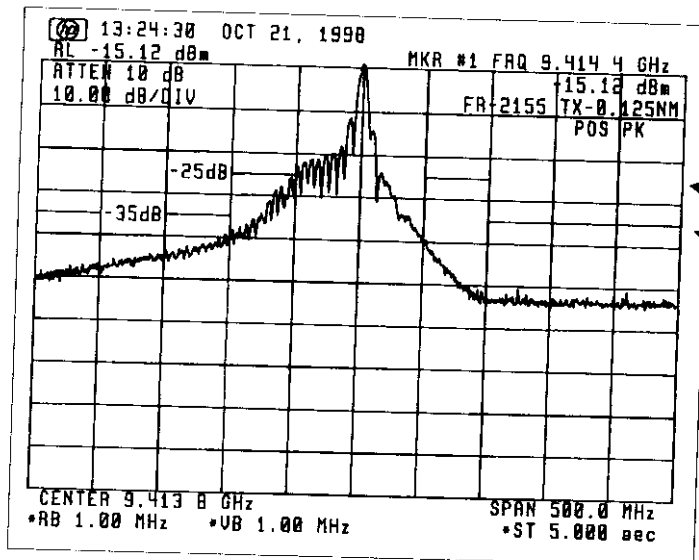
12 OPERATOR'S MANUAL INCL. CIRCUIT DIAGRAMS (FCC Rule § 2.983)

(See separate covers)

ATTACHMENT 1

[TEST DATA FOR 6. SPURIOUS EMISSIONS AT ANTENNA TERMINALS]

1. Spurious emissions for 0.125 nm Range:

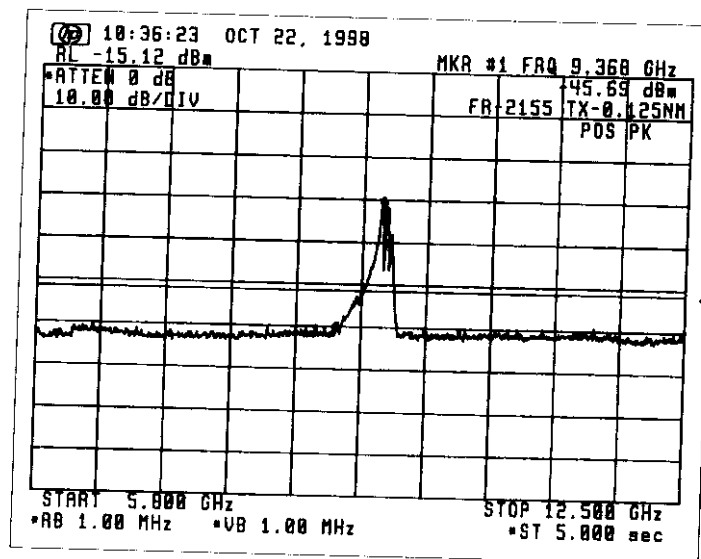


Ref. level: -15.12 dBm

Emission limitations:

- (a) 25 dB for 50 to 100 % of the authorized BW (100 MHz)
- (b) 35 dB for 100 to 250 % of the authorized BW (100 MHz)

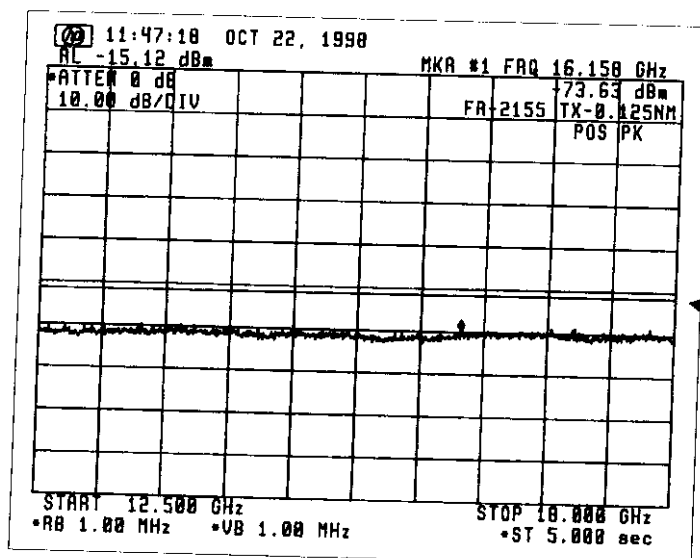
Fig. 1.1 Without Filter



Emission limitations:

- (c) $43 + 10 \log P_m = 51.33 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

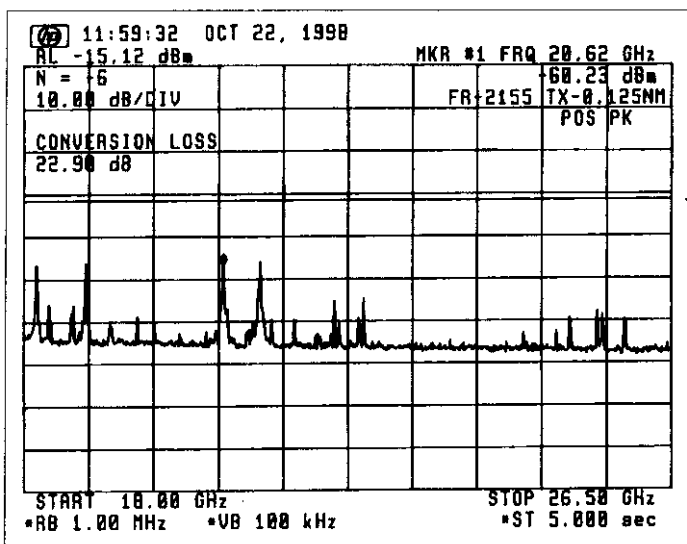
Fig. 1.2 With Filter No.1



Emission limitations:

- (c) $43 + 10 \log P_m = 51.33 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

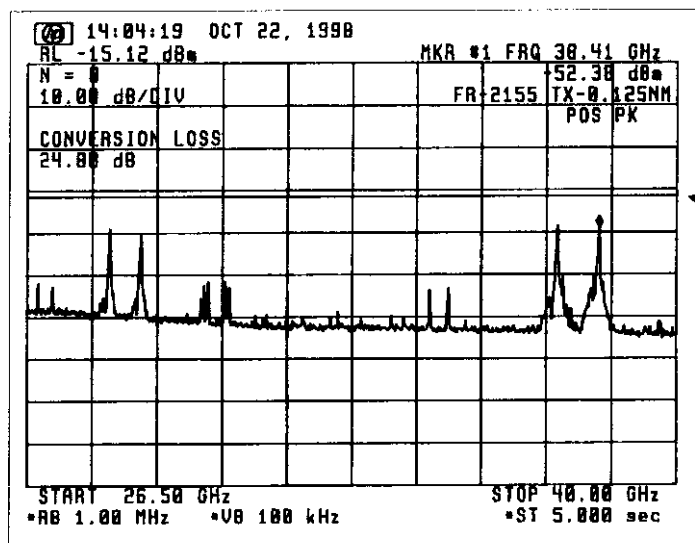
Fig. 1.3 With Filter No.2



Emission limitations:

- (c) $43 + 10 \log P_m = 51.33 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 1.4 With Filter No. 2

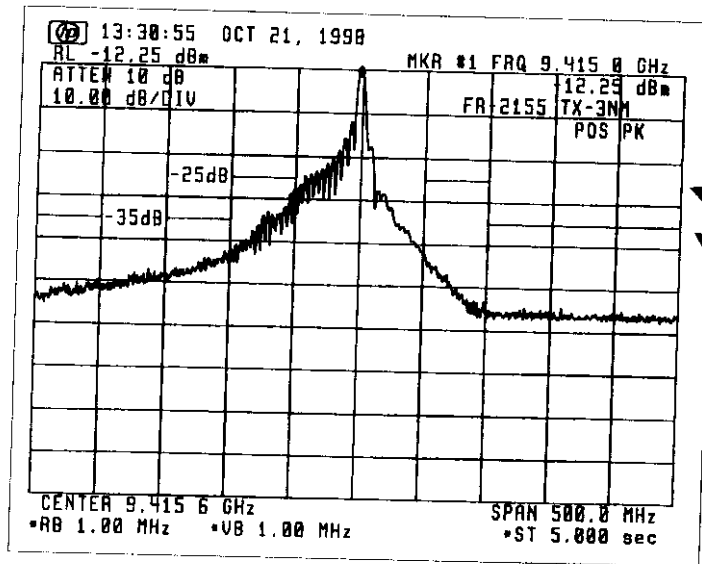


Emission limitations:

- (c) $43 + 10 \log P_m = 51.33 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 1.5 With Filter No. 2

2. Spurious emissions for 3 nm Range:

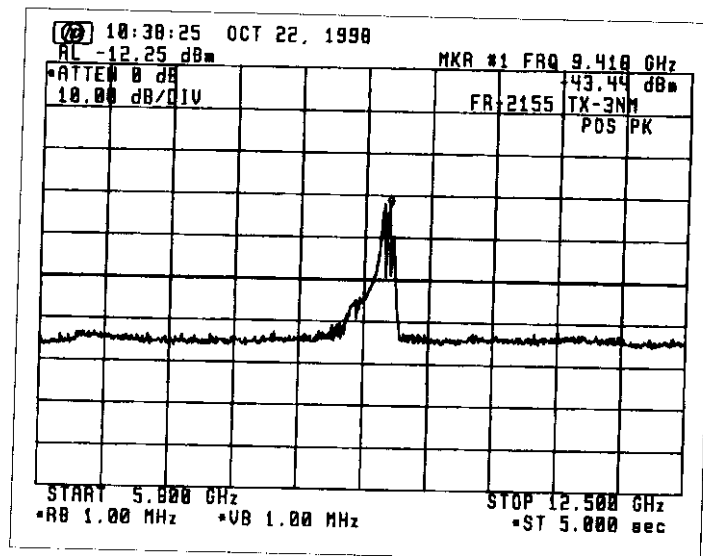


Ref. level: -12.25 dBm

Emission limitations:

- (a) 25 dB for 50 to 100 % of the authorized BW (100 MHz)
- (b) 35 dB for 100 to 250 % of the authorized BW (100 MHz)

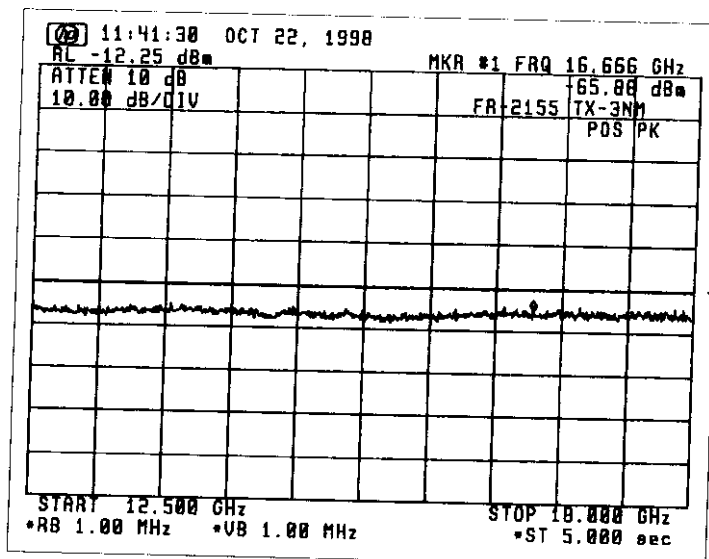
Fig. 2.1 Without Filter



Emission limitations:

- (c) $43 + 10 \log P_m = 50.11 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

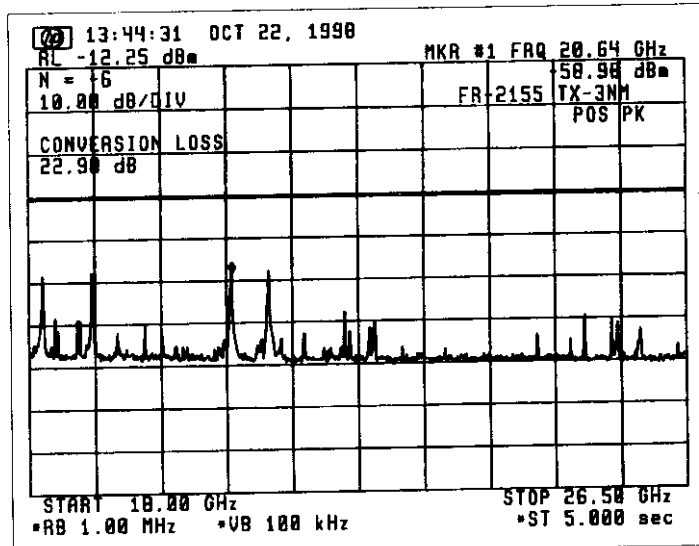
Fig. 2.2 With Filter No.1



Emission limitations:

- (c) $43 + 10 \log P_m = 50.11 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

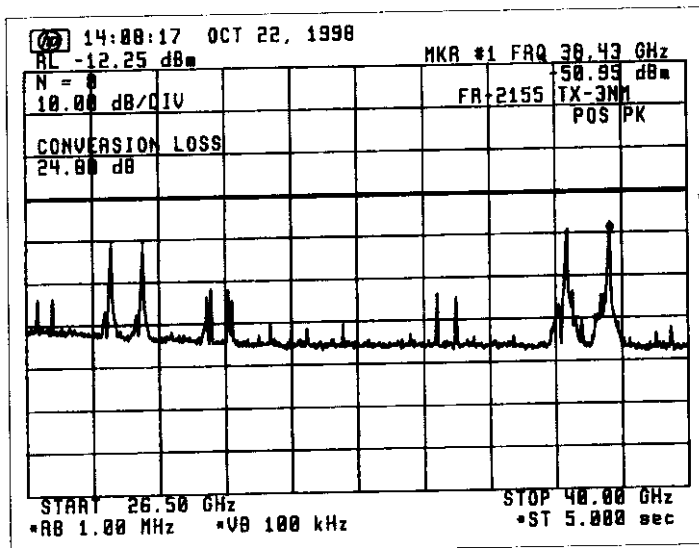
Fig. 2.3 With Filter No. 2



Emission limitations:

- (c) $43 + 10 \log P_m = 50.11 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 2.4 With Filter No. 2

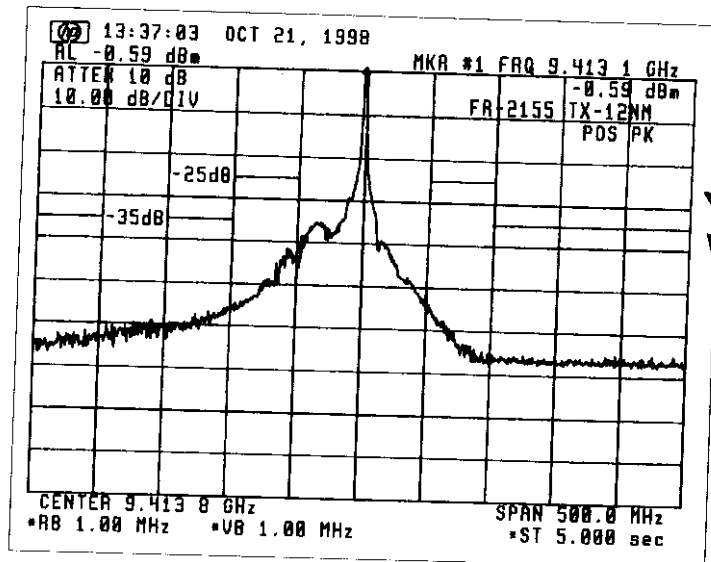


Emission limitations:

- (c) $43 + 10 \log P_m = 50.11 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 2.5 With Filter No. 2

3. Spurious emissions for 12 nm Range:

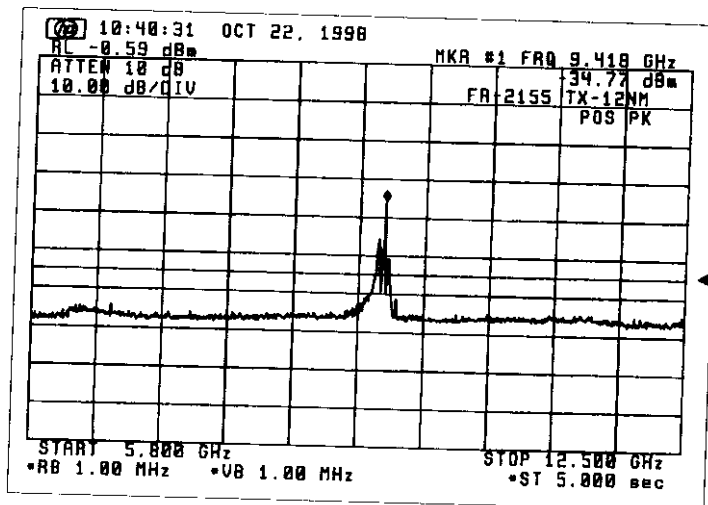


Ref. level: -0.59 dBm

Emission limitations:

- (a) 25 dB for 50 to 100 % of the authorized BW (100 MHz)
- (b) 35 dB for 100 to 250 % of the authorized BW (100 MHz)

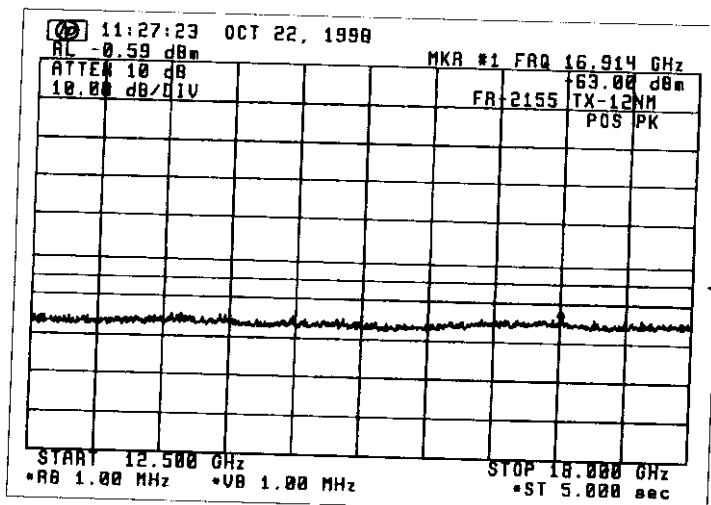
Fig. 3.1 Without Filter



Emission limitations:

- (c) $43 + 10 \log P_m = 54.64 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

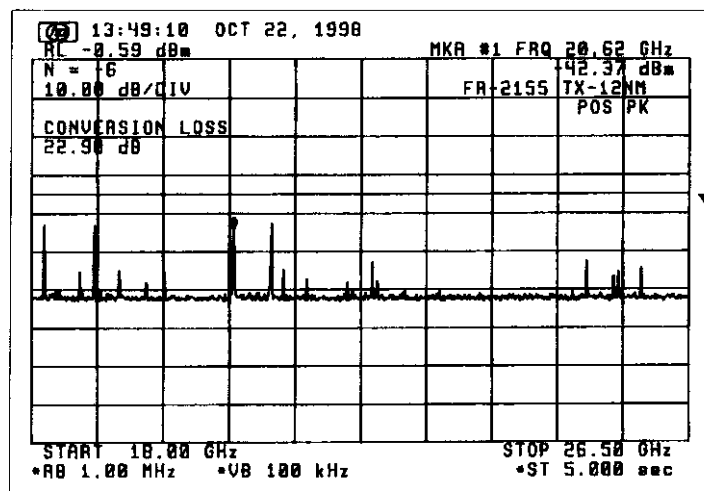
Fig. 3.2 With Filter No.1



Emission limitations:

- (c) $43 + 10 \log P_m = 54.64 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

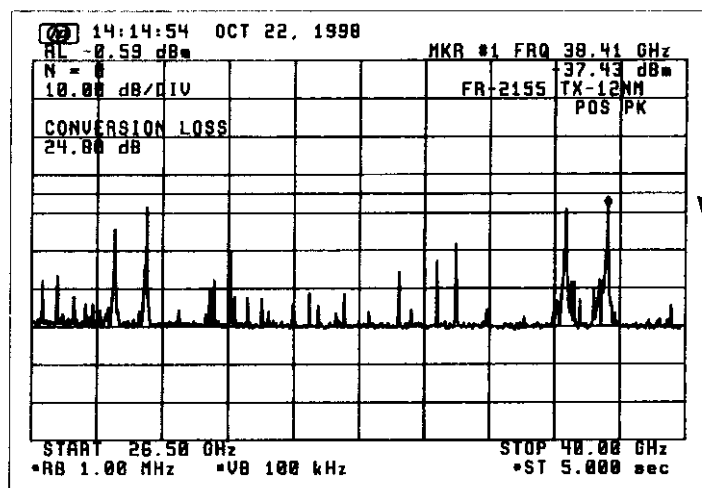
Fig. 3.3 With Filter No. 2



Emission limitations:

- (c) $43 + 10 \log P_m = 54.64 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 3.4 With Filter No. 2

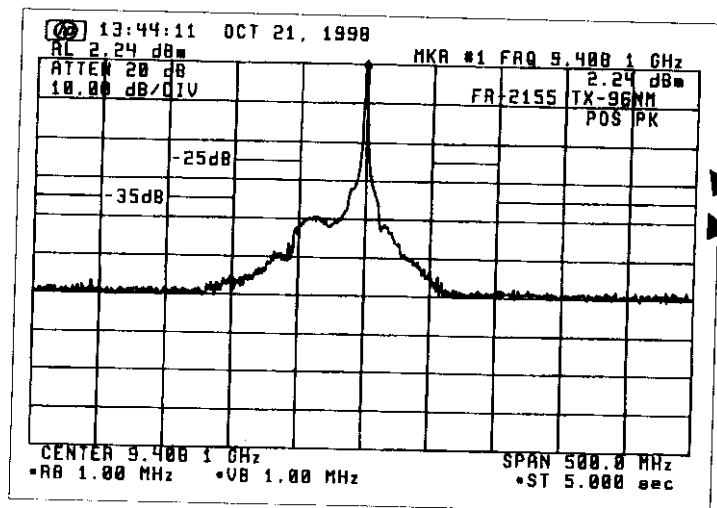


Emission limitations:

- (c) $43 + 10 \log P_m = 54.64 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 3.5 With Filter No. 2

4. Spurious emissions for 96 nm Range:

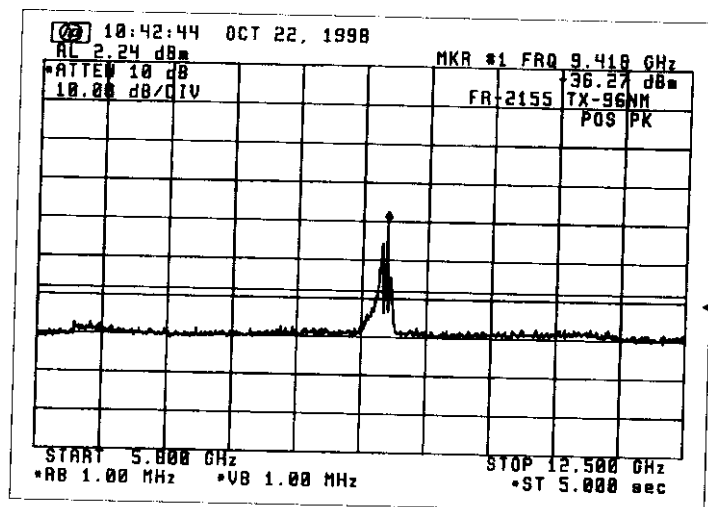


Ref. level: 2.24 dBm

Emission limitations:

- (a) 25 dB for 50 to 100 % of the authorized BW (100 MHz)
- (b) 35 dB for 100 to 250 % of the authorized BW (100 MHz)

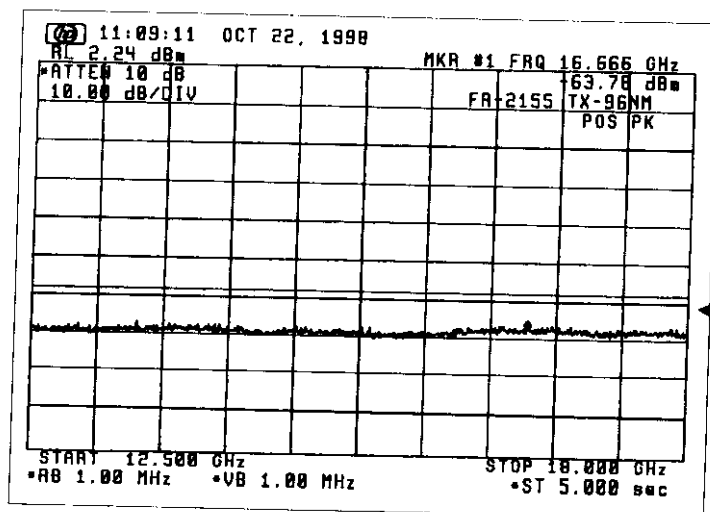
Fig. 4.1 Without Filter



Emission limitations:

- (c) $43 + 10 \log P_m = 57.92 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

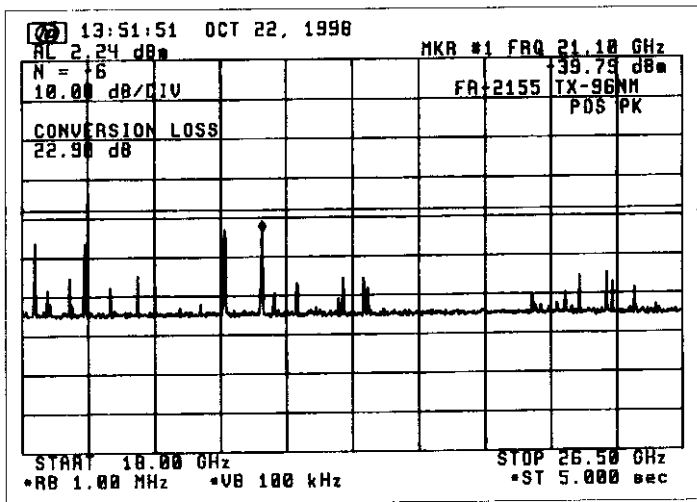
Fig. 4.2 With Filter No.1



Emission limitations:

- (c) $43 + 10 \log P_m = 57.92 \text{ dB}$ for more than 250 % of the authorized BW (100 MHz)

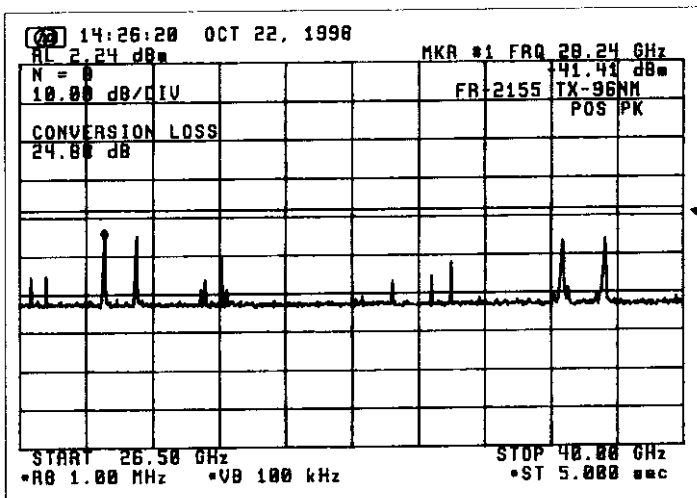
Fig. 4.3 With Filter No. 2



Emission limitations:

- (c) $43 + 10 \log P_m = 57.92 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

Fig. 4.4 With Filter No. 2



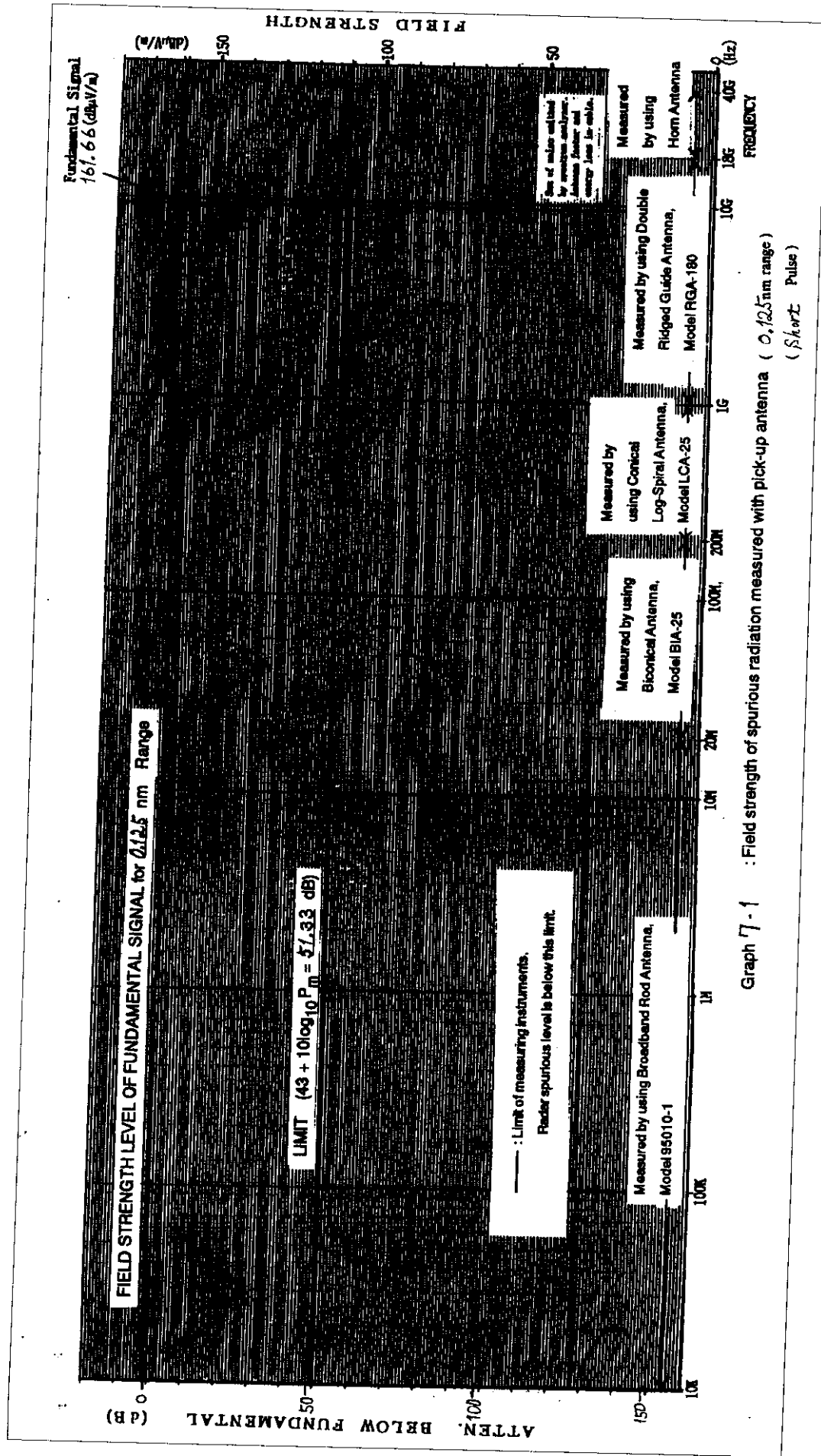
Emission limitations:

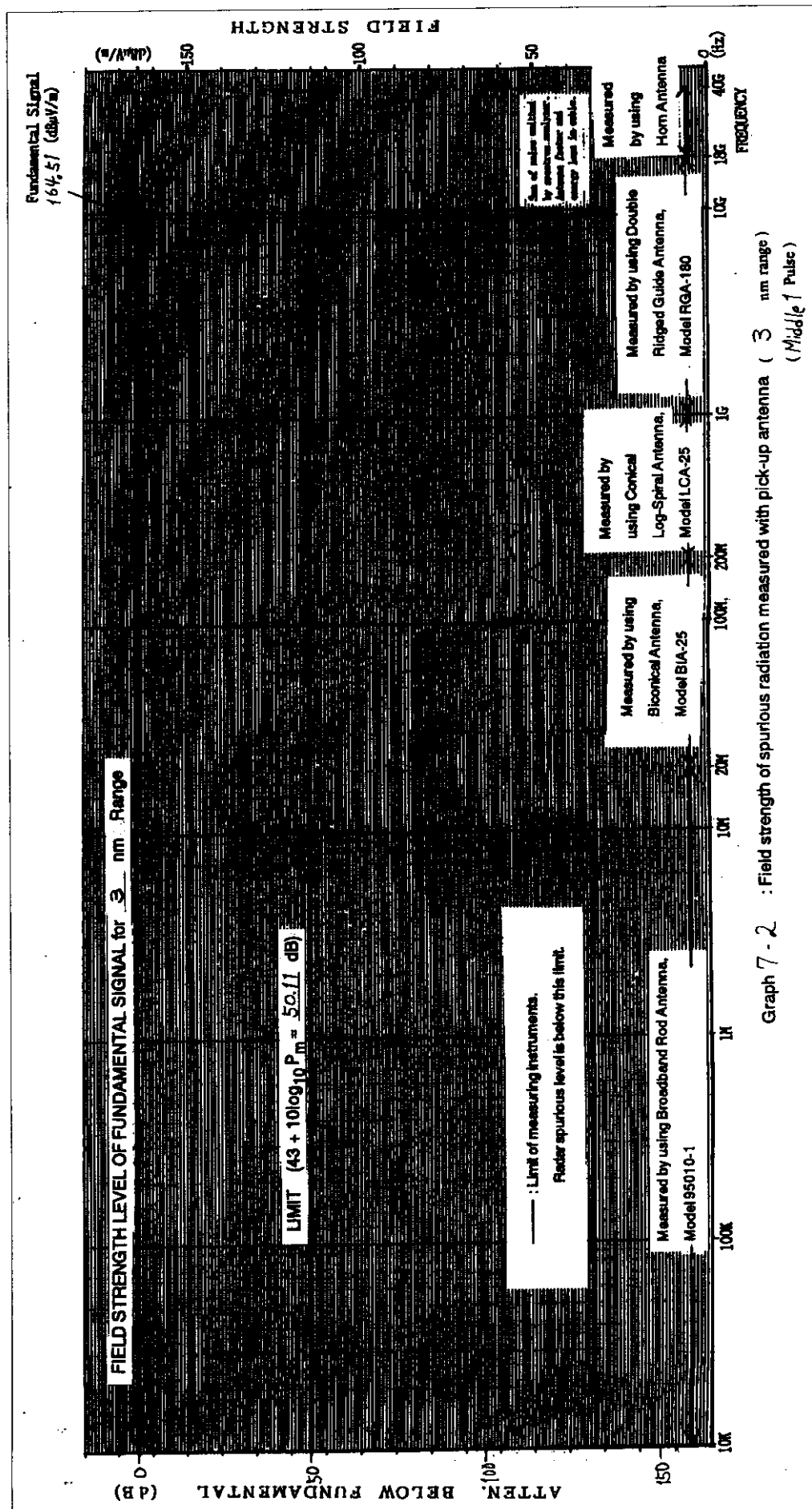
- (c) $43 + 10 \log P_m = 57.92 \text{ dB}$
for more than 250 % of
the authorized BW (100 MHz)

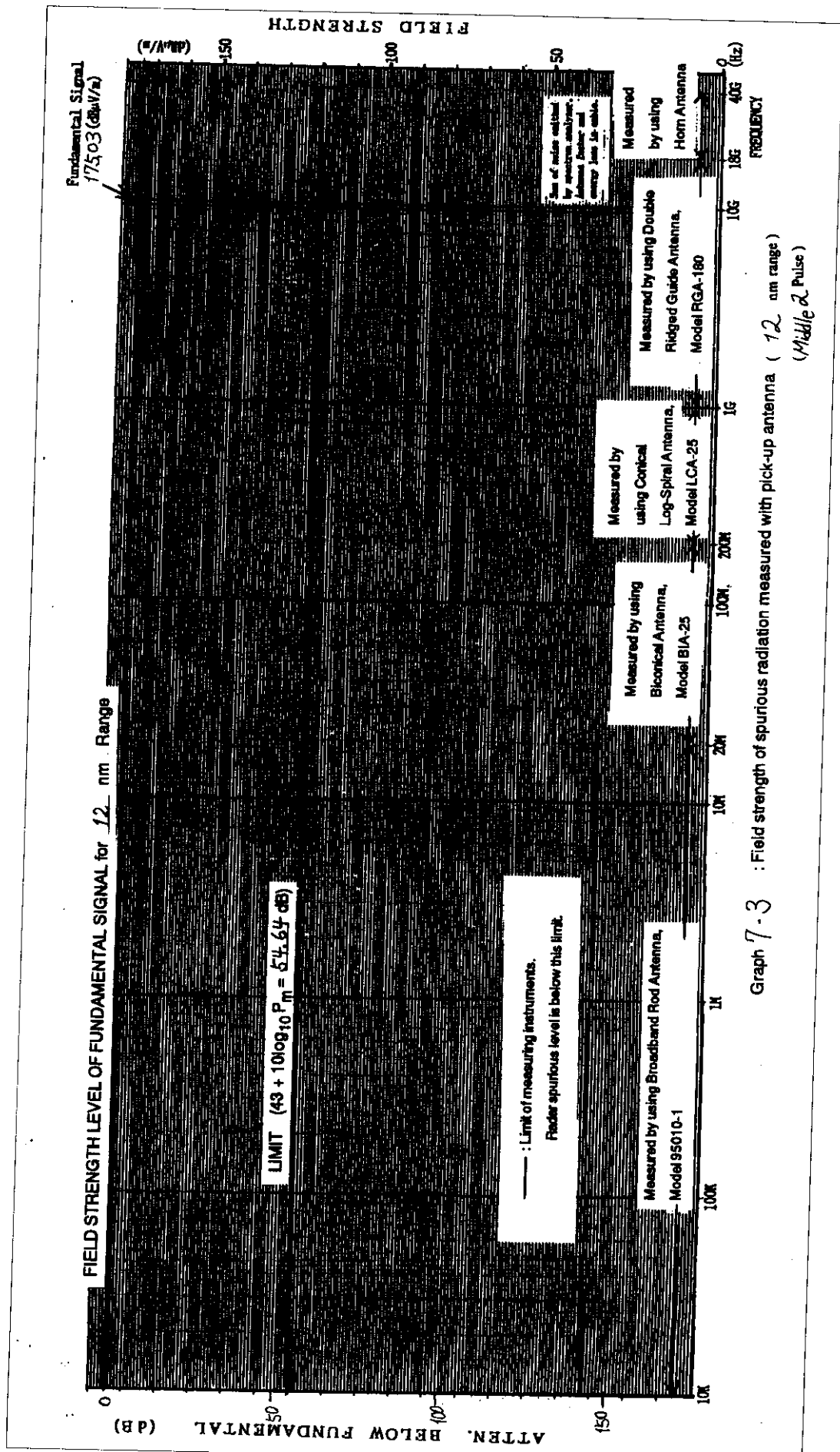
Fig. 4.5 With Filter No. 2

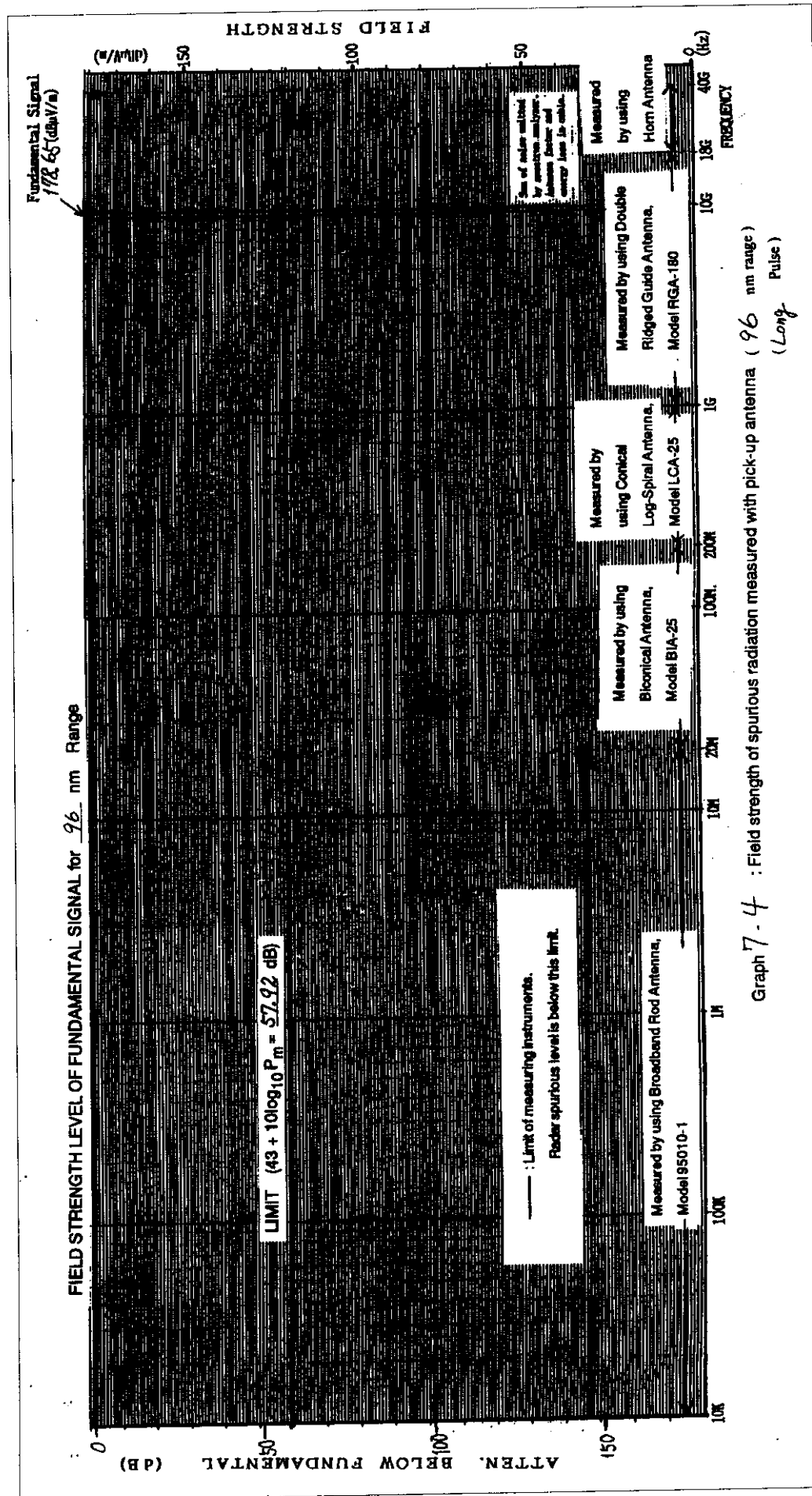
ATTACHMENT 2

[TEST DATA FOR 7. FIELD STRENGTH OF SPOURIOUS RADIATION]







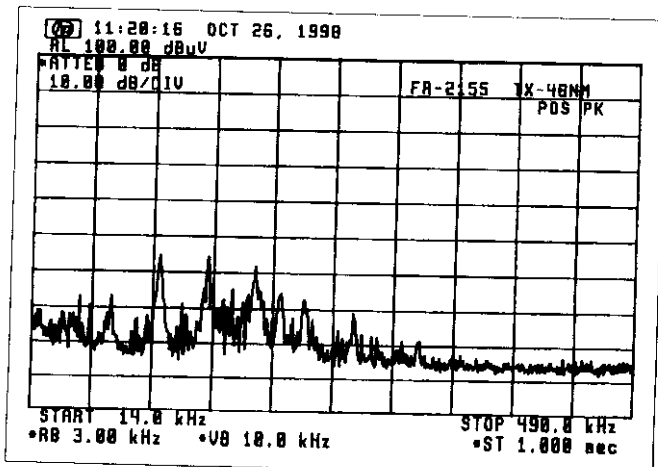
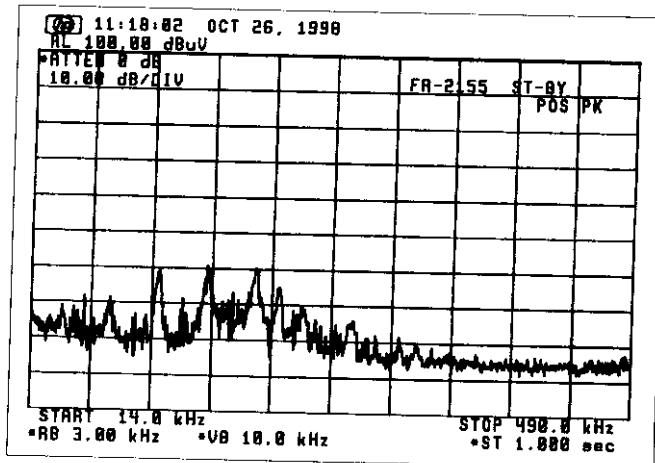
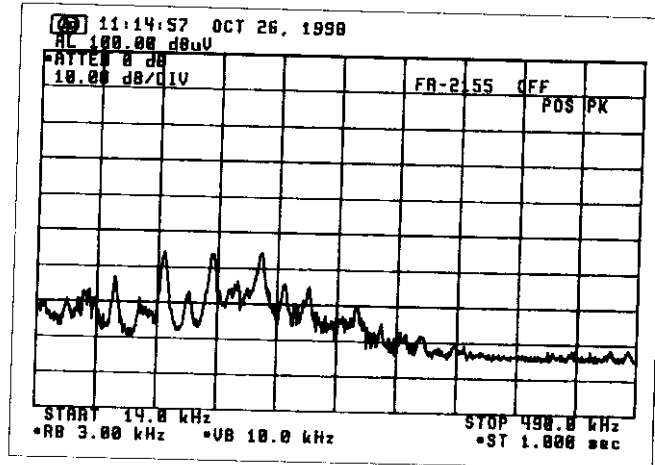


ATTACHMENT 3

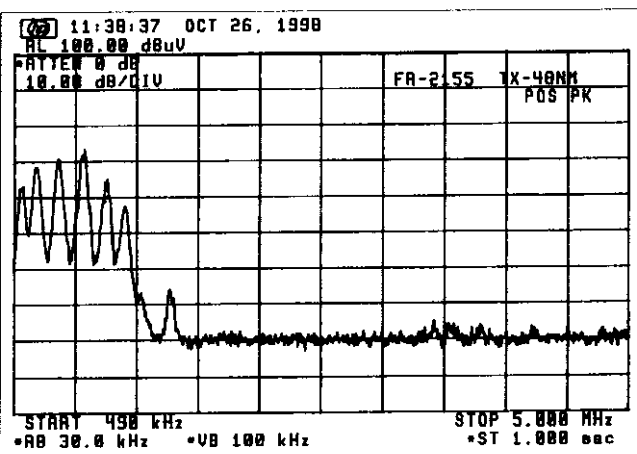
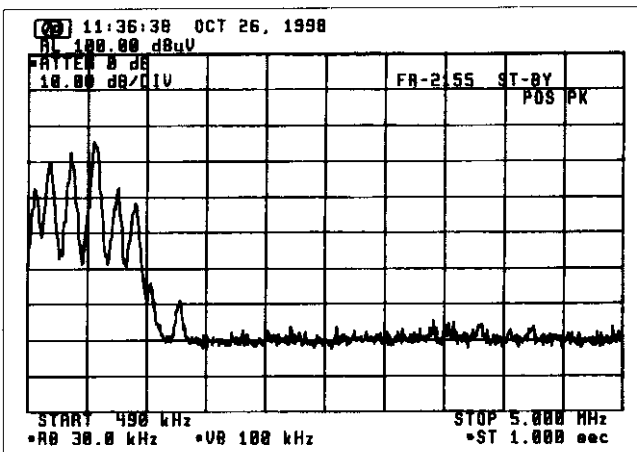
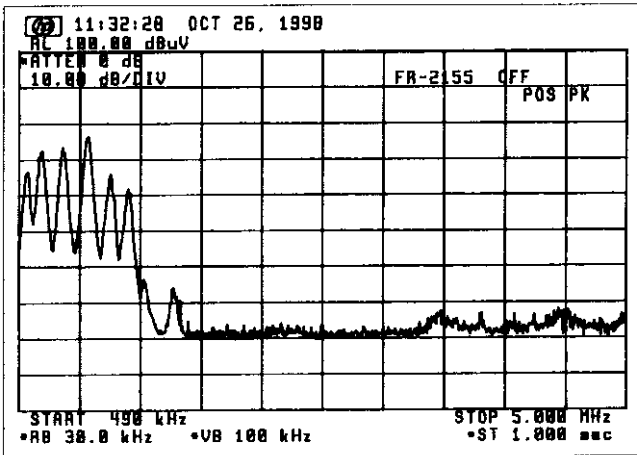
[TEST DATA FOR 9. SUPPRESSION OF INTERFERENCE ABOARD SHIPS]

1. Harmful Interference to Receiver

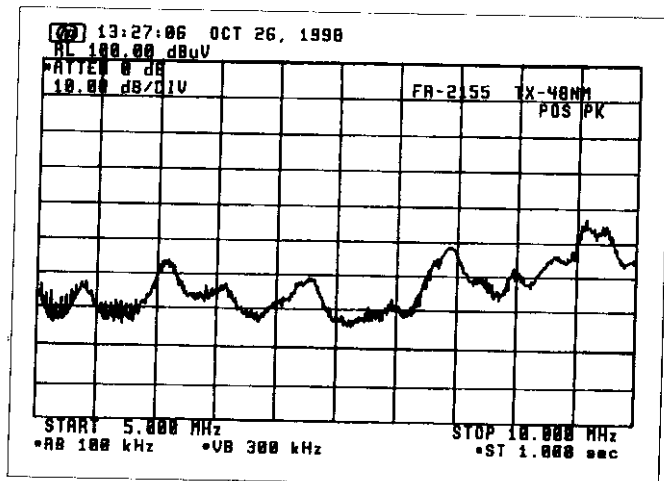
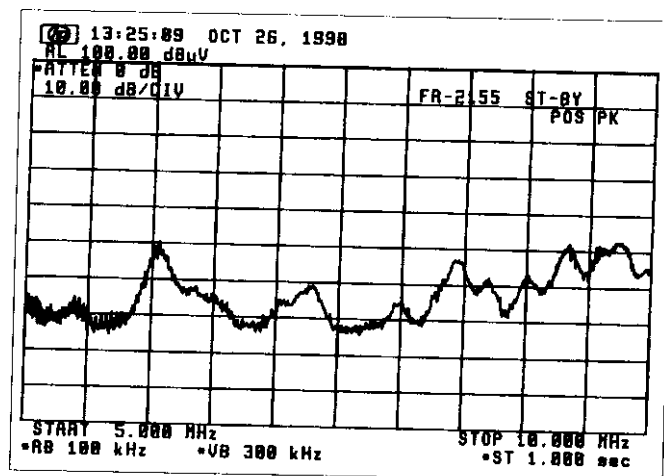
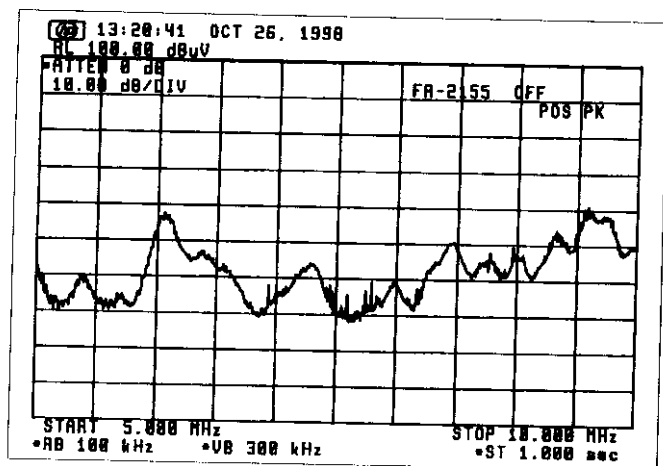
(Band : 14 kHz - 490 kHz)



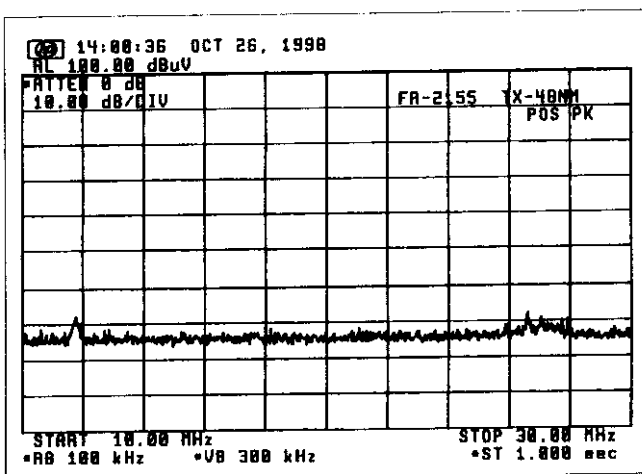
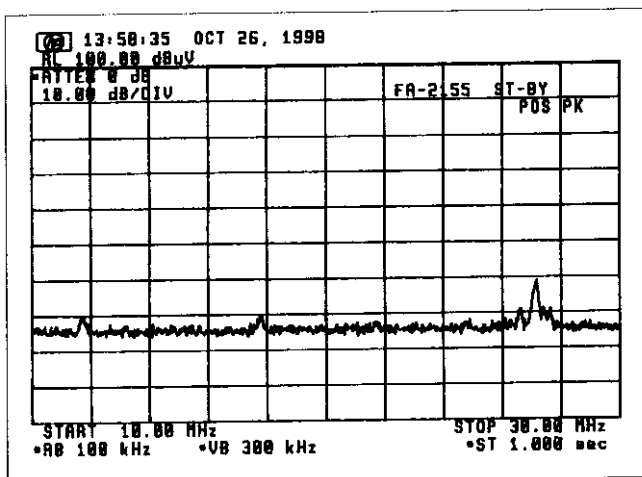
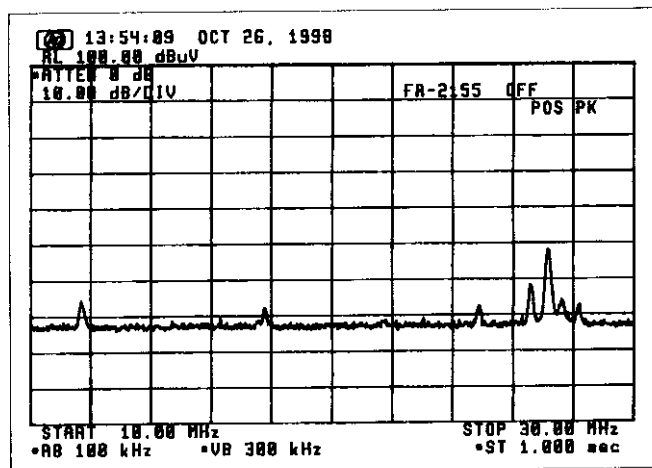
(Band : 490 kHz - 5 MHz)



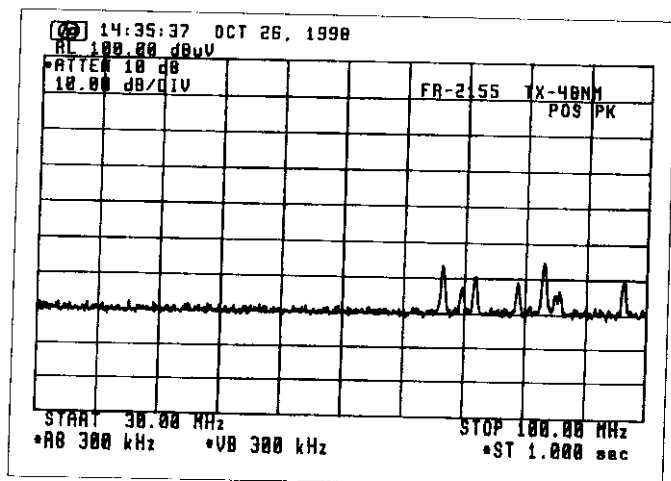
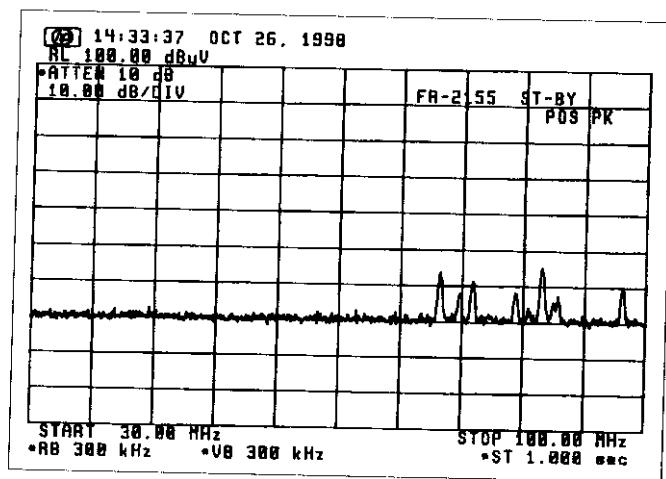
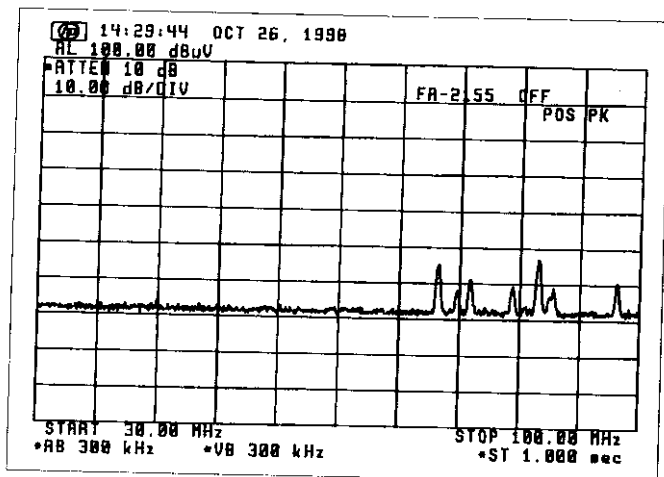
(Band : 5 MHz - 10 MHz)



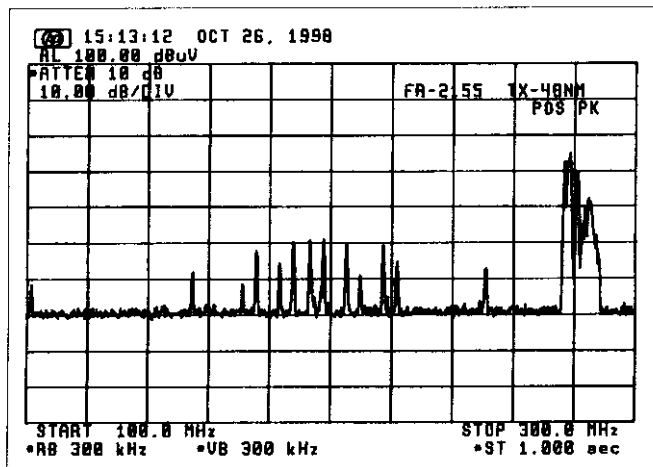
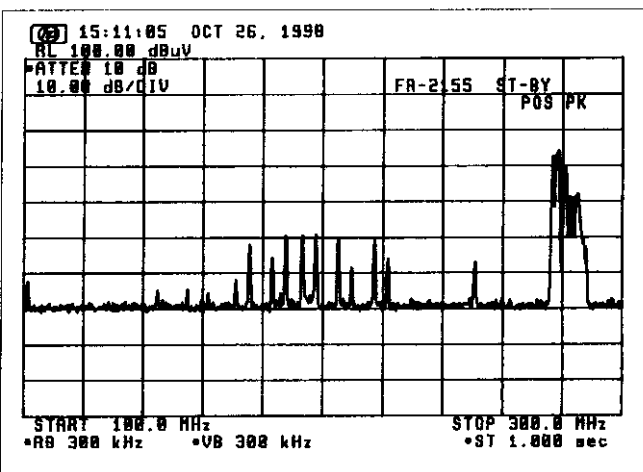
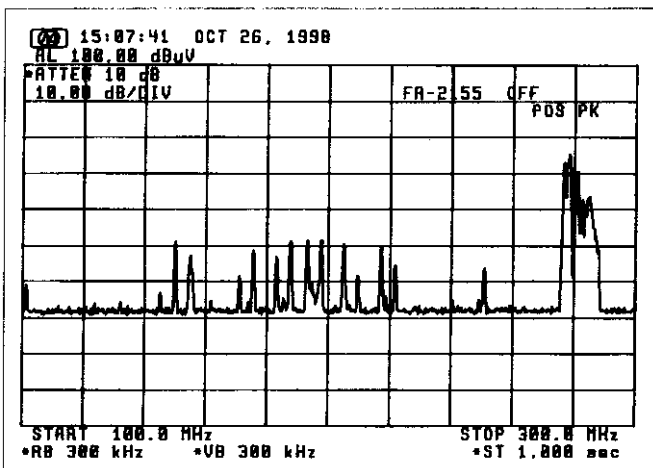
(Band : 10 MHz - 30 MHz)



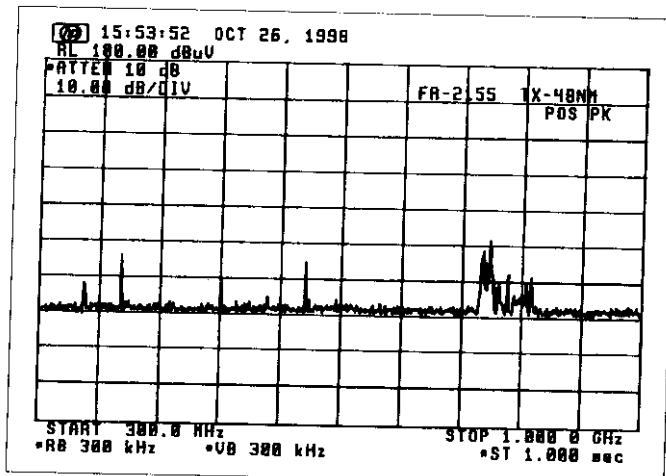
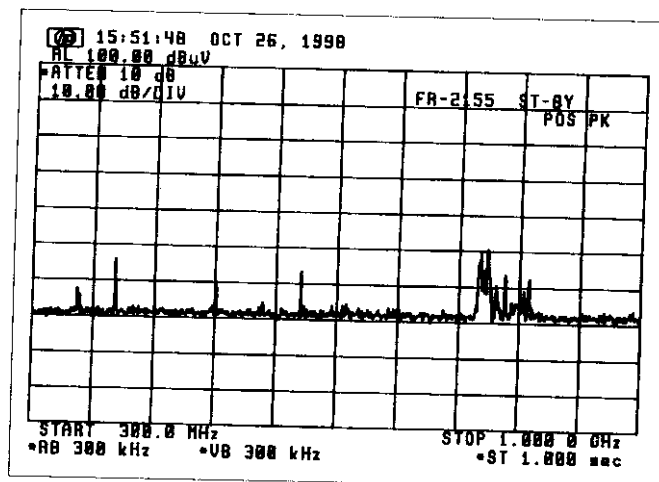
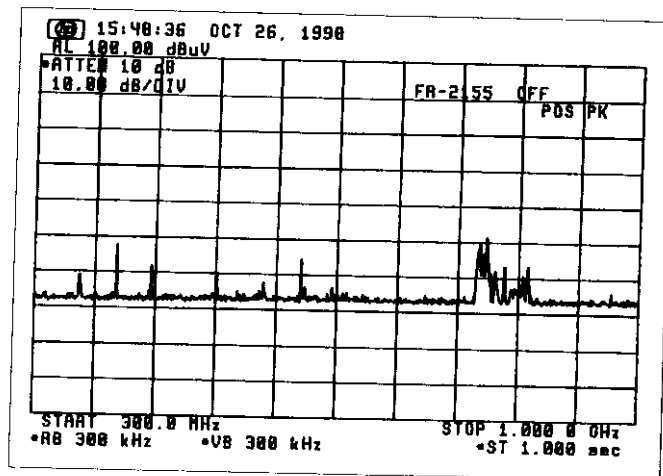
(Band : 30 MHz - 100 MHz)



(Band : 100 MHz - 300 MHz)

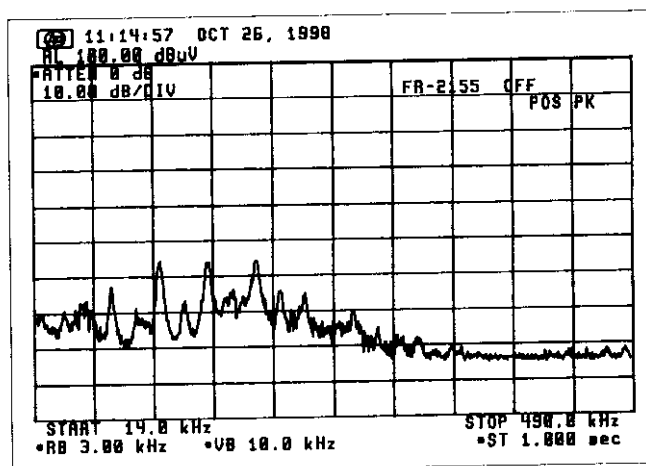


(Band : 300 MHz - 1 GHz)

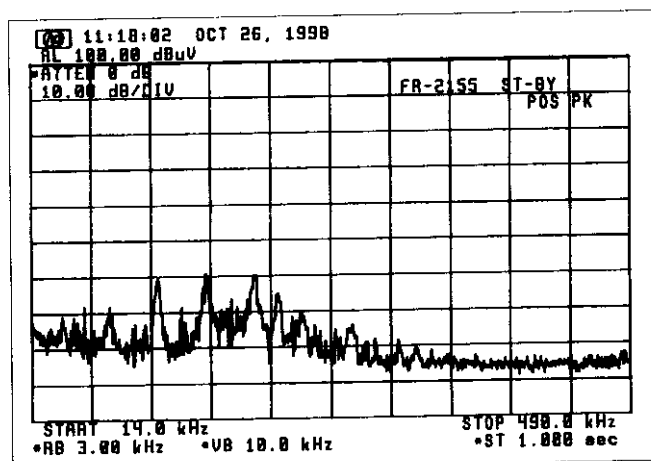


2. Electromagnetic Field

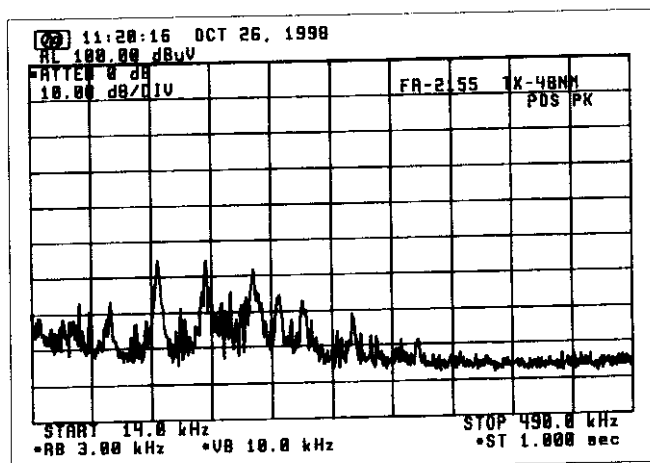
(Band : 14 kHz - 490 kHz, Limit at 1 nm = 0.1 $\mu\text{V/m}$ = -20 dB $\mu\text{V/m}$)



-26 dB $\mu\text{V/m}$

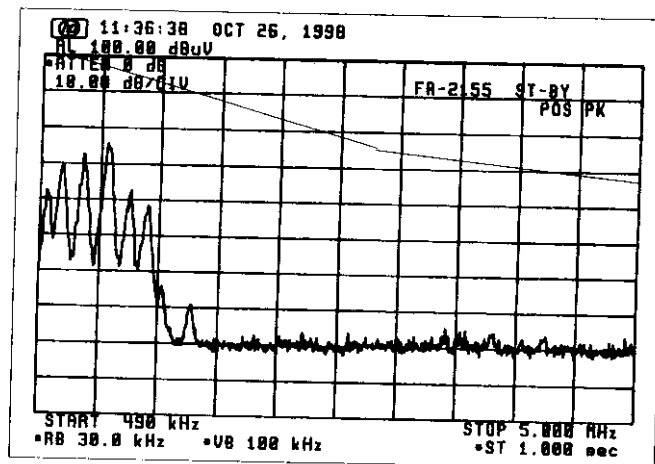
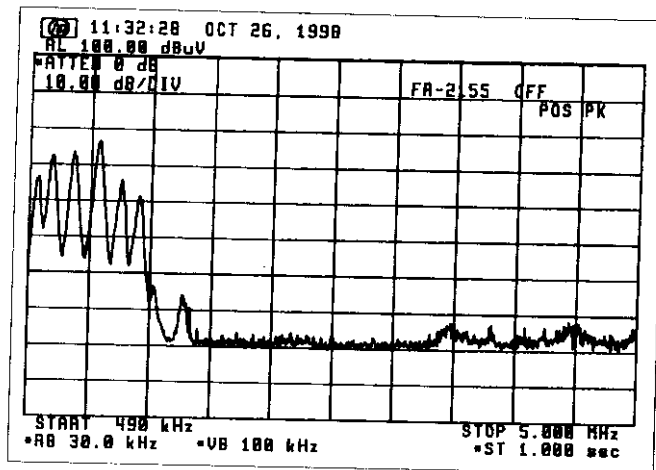


-26 dB $\mu\text{V/m}$



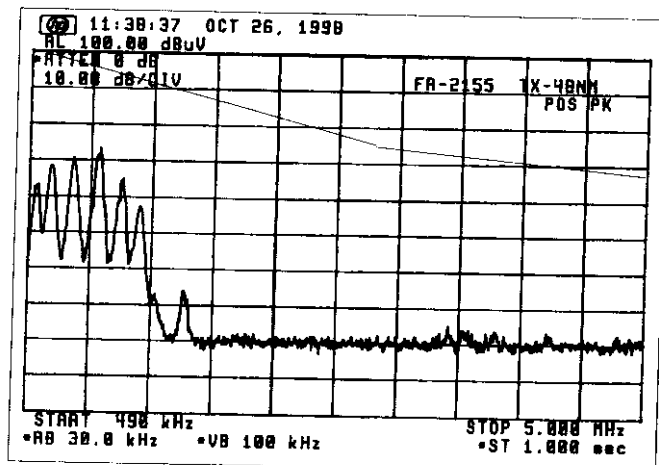
-26 dB $\mu\text{V/m}$

(Band : 490 kHz - 5 MHz, Limit at 1 nm = 0.1 μ V/m = -20 dB μ V/m)



Ref. level (dB μ V/m)
= 126 - 100 = 26 (at 0.5 MHz)
= 100 - 96 = 4 (at 3 MHz)
= 100 - 88 = 12 (at 5 MHz)

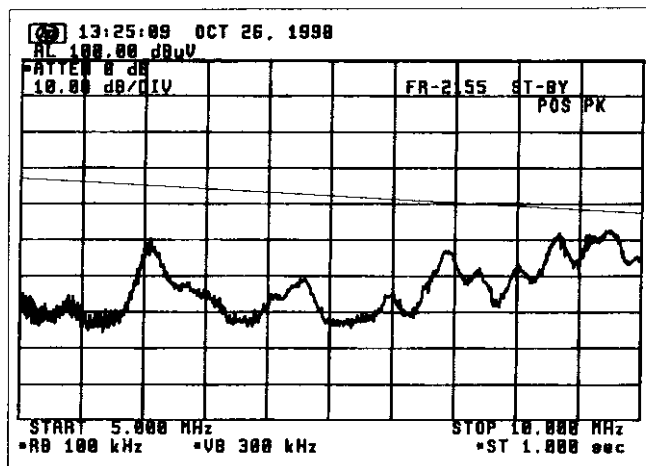
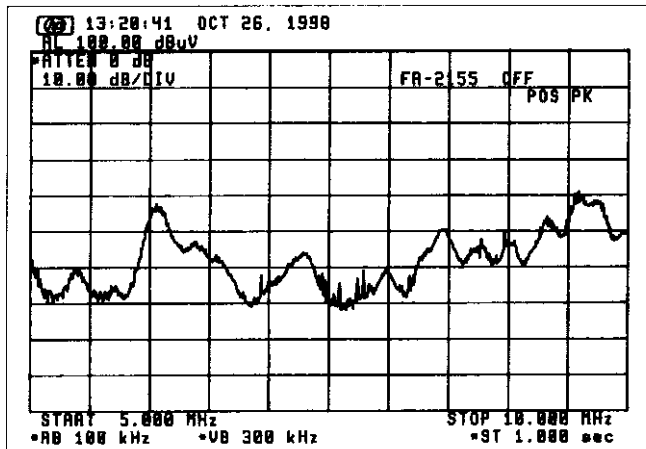
-20 dB μ V/m limit line



Ref. level (dB μ V/m)
= 126 - 100 = 26 (at 0.5 MHz)
= 100 - 96 = 4 (at 3 MHz)
= 100 - 88 = 12 (at 5 MHz)

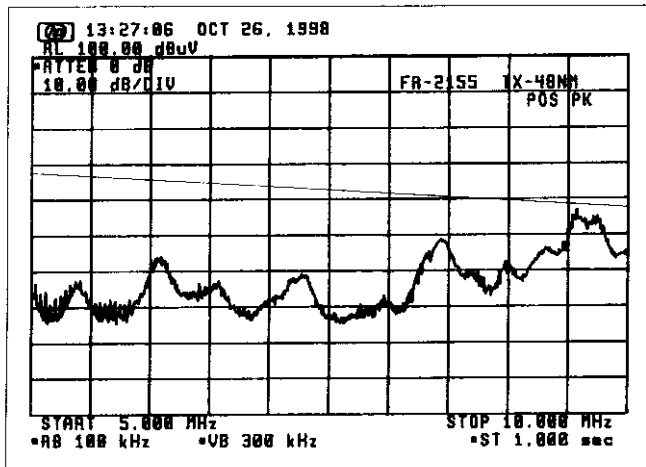
-20 dB μ V/m limit line

(Band : 5 MHz - 10 MHz, Limit at 1 nm = 0.1 μ V/m = -20 dB μ V/m)



Ref. level (dB μ V/m)
= 100 - 88 = 12 (at 5 MHz)
= 100 - 83 = 17 (at 7 MHz)
= 100 - 78 = 22 (at 10 MHz)

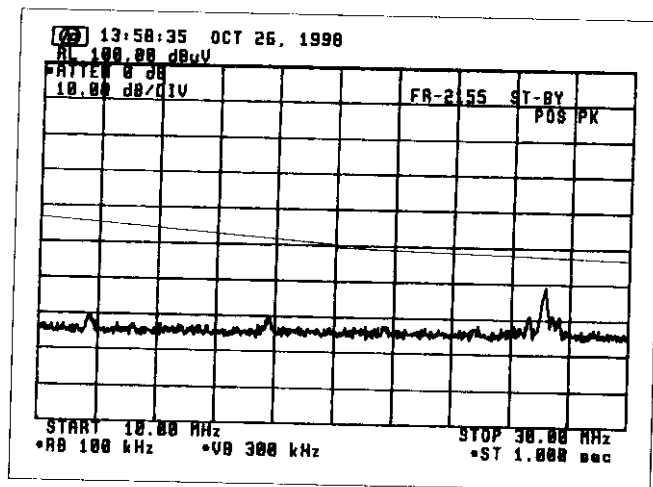
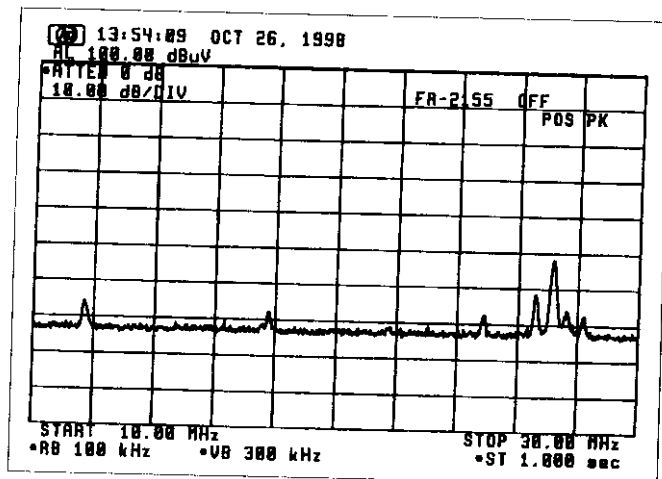
-20 dB μ V/m limit line



Ref. level (dB μ V/m)
= 100 - 88 = 12 (at 5 MHz)
= 100 - 83 = 17 (at 7 MHz)
= 100 - 78 = 22 (at 10 MHz)

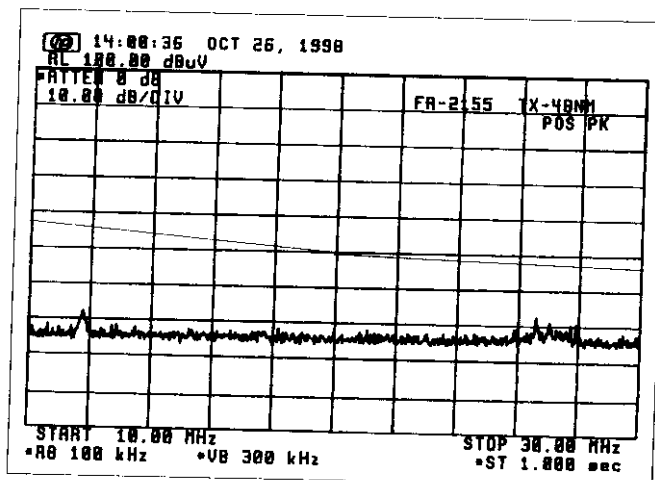
-20 dB μ V/m limit line

(Band : 10 MHz - 30 MHz, Limit at 1 nm = 0.1 $\mu\text{V/m}$ = -20 dB $\mu\text{V/m}$)



Ref. level (dB $\mu\text{V/m}$)
= 100 - 78 = 22 (at 10 MHz)
= 100 - 70 = 30 (at 20 MHz)
= 100 - 67 = 33 (at 30 MHz)

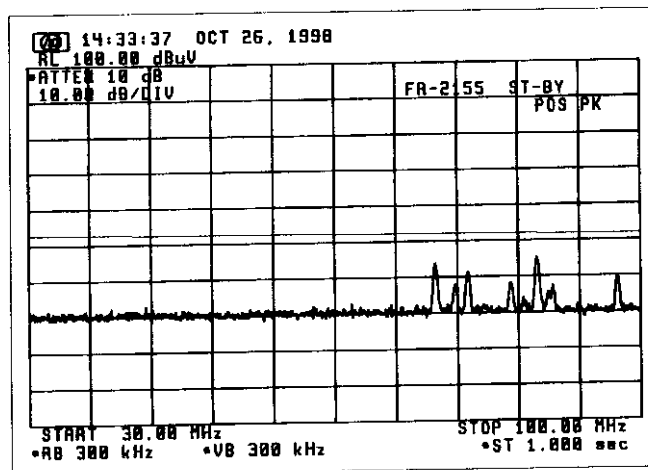
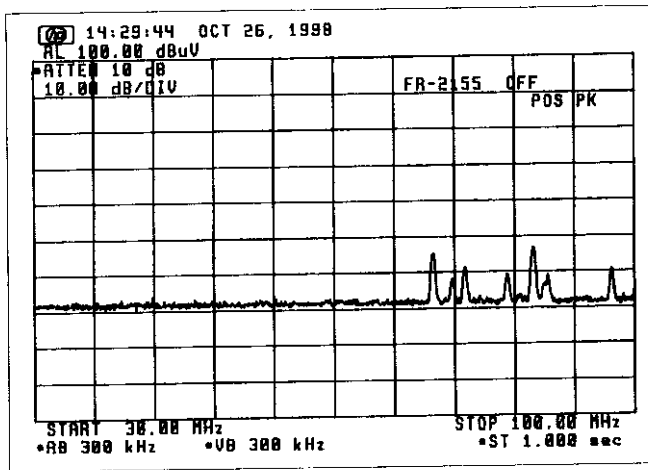
-20 dB $\mu\text{V/m}$ limit line



Ref. level (dB $\mu\text{V/m}$)
= 100 - 78 = 22 (at 10 MHz)
= 100 - 70 = 30 (at 20 MHz)
= 100 - 67 = 33 (at 30 MHz)

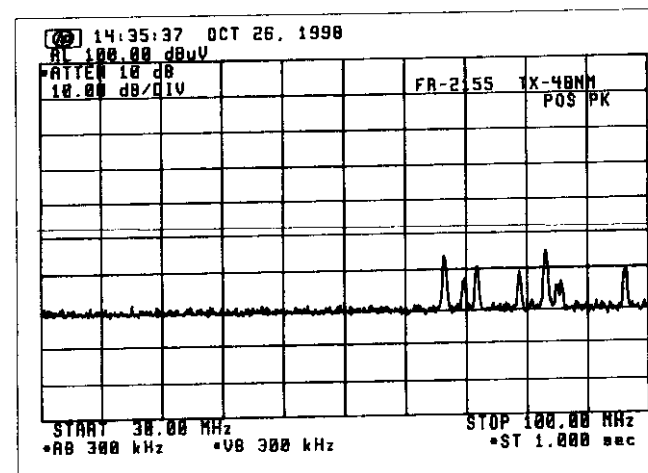
-20 dB $\mu\text{V/m}$ limit line

(Band : 30 MHz - 100 MHz, Limit at 1 nm = 0.1 $\mu\text{V/m}$ = -10.5 dB $\mu\text{V/m}$)



Ref. level (dB $\mu\text{V/m}$)
= 100 - 61 = 39

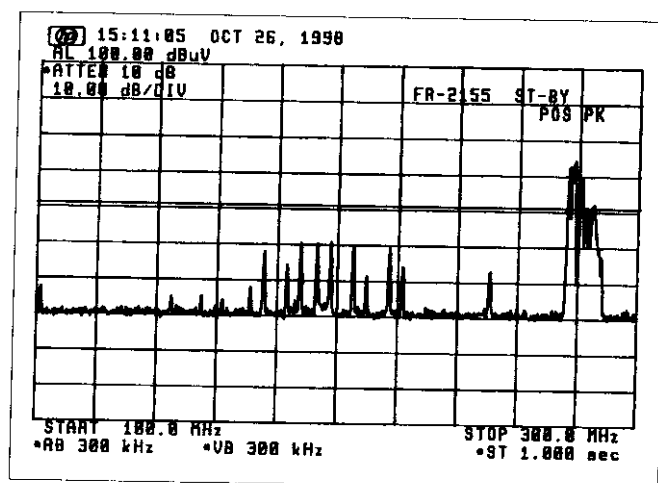
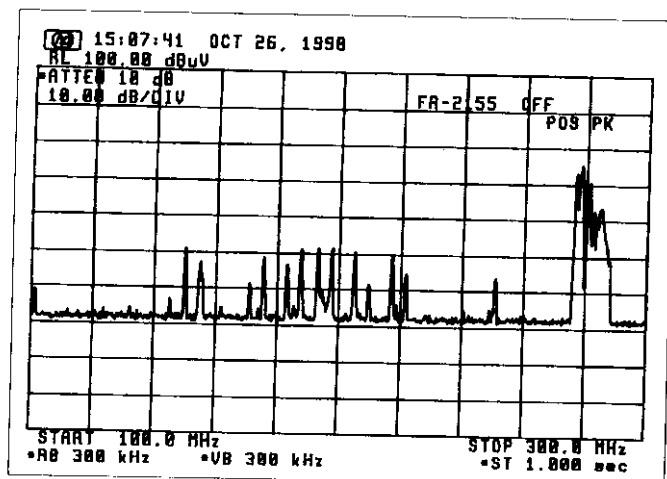
- 10.5 dB $\mu\text{V/m}$ limit line



Ref. level (dB $\mu\text{V/m}$)
= 100 - 61 = 39

- 10.5 dB $\mu\text{V/m}$ limit line

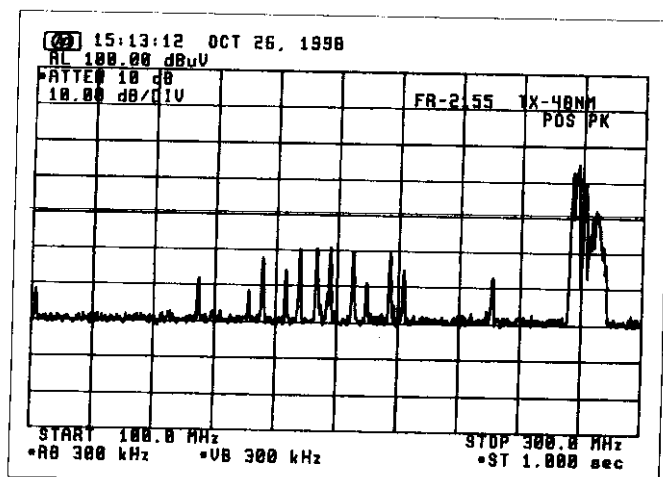
(Band : 100 MHz - 300 MHz, Limit at 1 nm = 0.1 $\mu\text{V}/\text{m}$ = -0 dB $\mu\text{V}/\text{m}$)



Ref. level (dB $\mu\text{V}/\text{m}$)
= 100 - 60 = 40

0 dB $\mu\text{V}/\text{m}$ limit line

All components above the limit
are from external noise or
signals, not from RADAR.

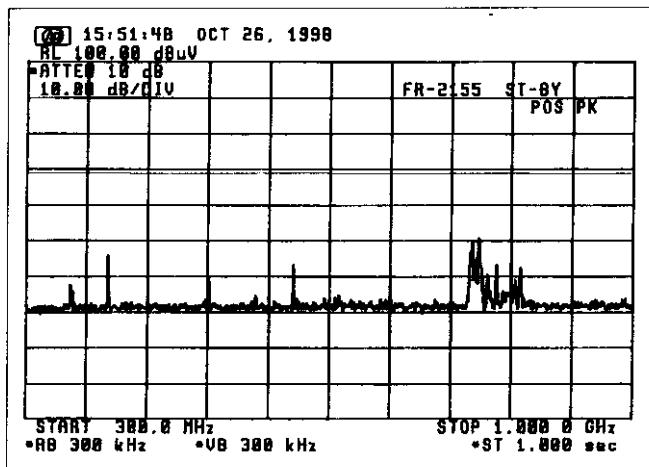
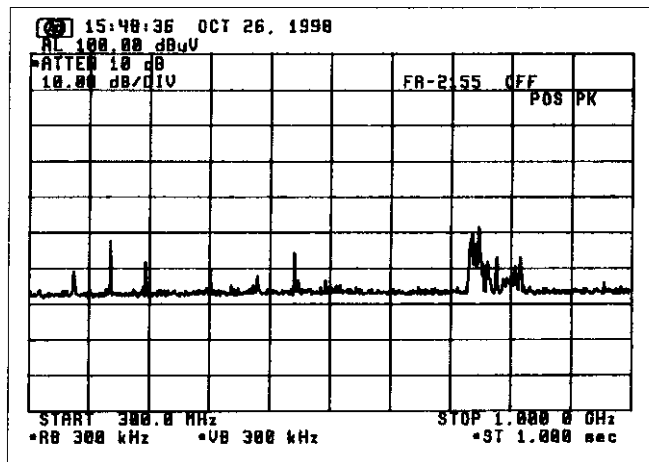


Ref. level (dB $\mu\text{V}/\text{m}$)
= 100 - 60 = 40

0 dB $\mu\text{V}/\text{m}$ limit line

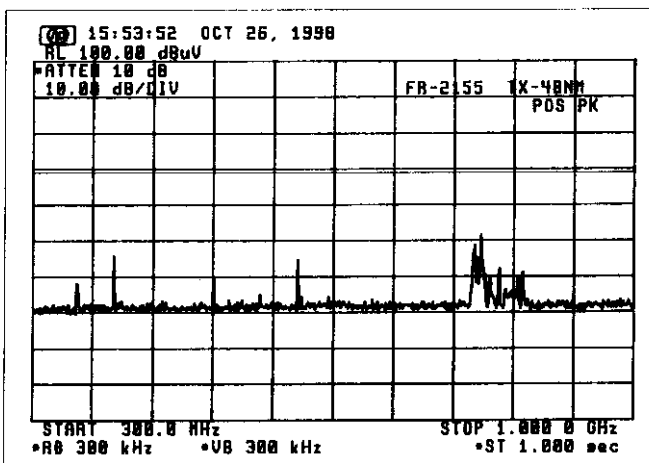
All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 300 MHz - 1 GHz, Limit at 1 nm = 3 μ V/m = -9.5 dB μ V/m)



Ref. level (dB μ V/m)
= 100 - 59.5 = 40.5

9.5 dB μ V/m limit line

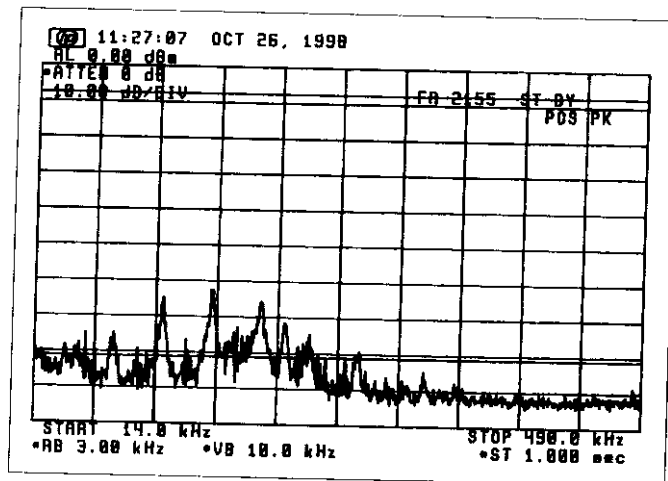
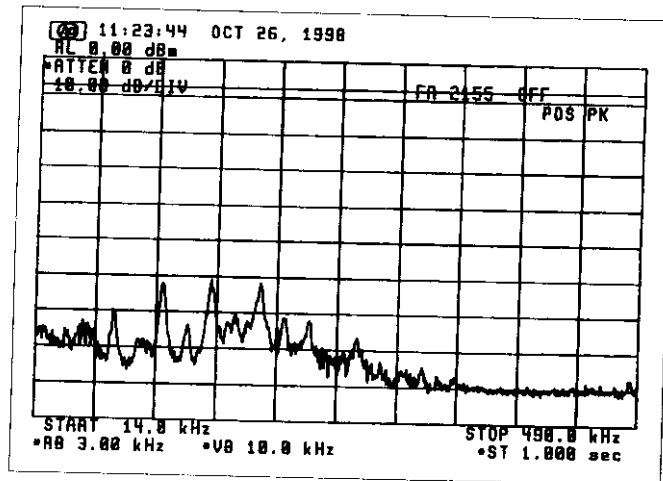


Ref. level (dB μ V/m)
= 100 - 59.5 = 40.5

9.5 dB μ V/m limit line

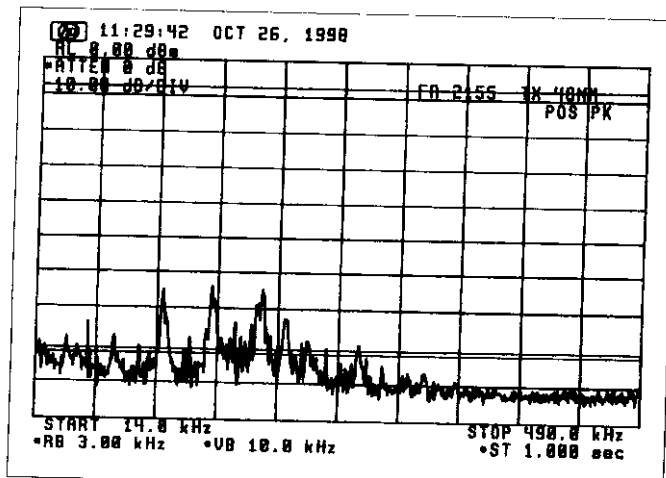
3. Power Input to an Artificial Antenna

(Band : 14 kHz - 490 kHz, Limit at 2 m = -81 dBm)



-81 dBm limit line

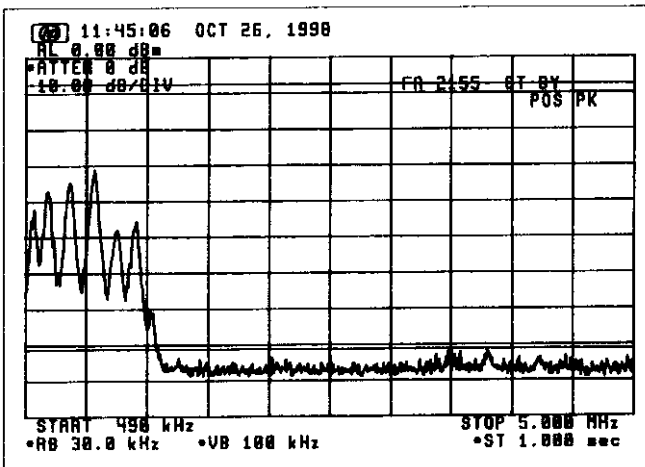
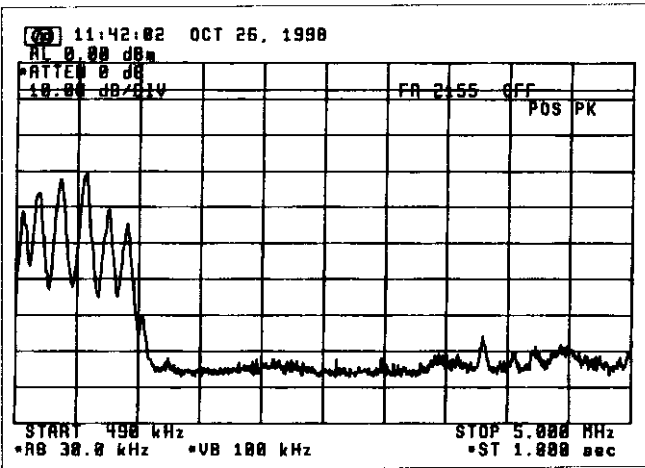
All components above the limit
are from external noise or
signals, not from RADAR.



-81 dBm limit line

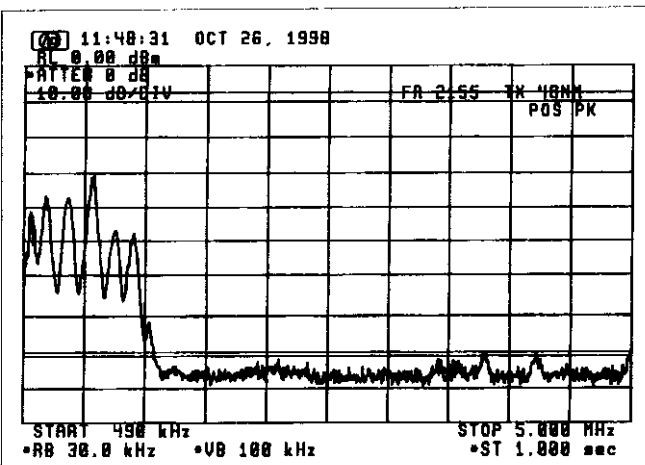
All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 490 kHz - 5 MHz, Limit at 2 m = -81 dBm)



-81 dBm limit line

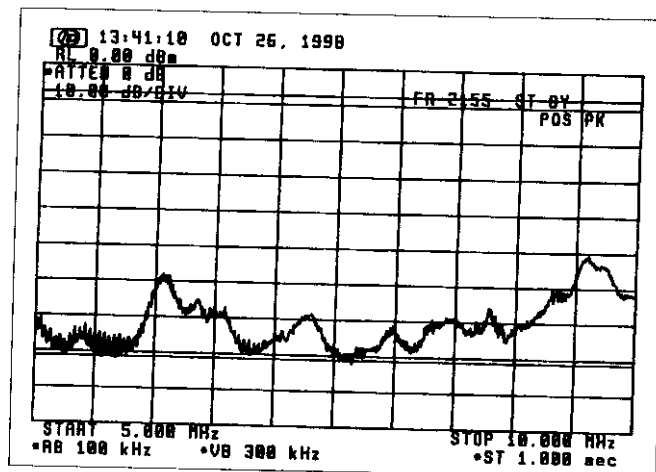
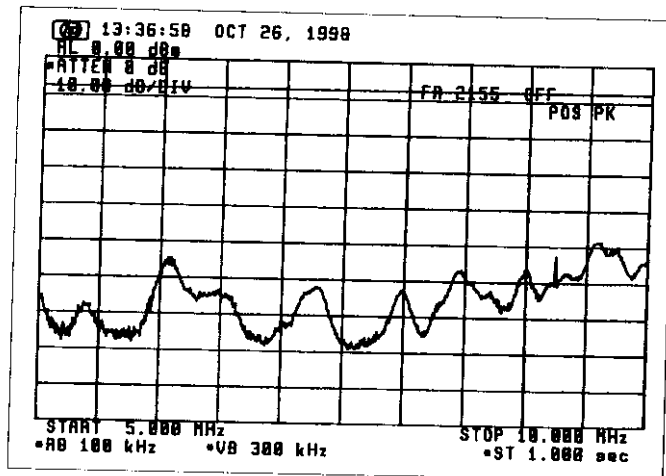
All components above the limit
are from external noise or
signals, not from RADAR.



-81 dBm limit line

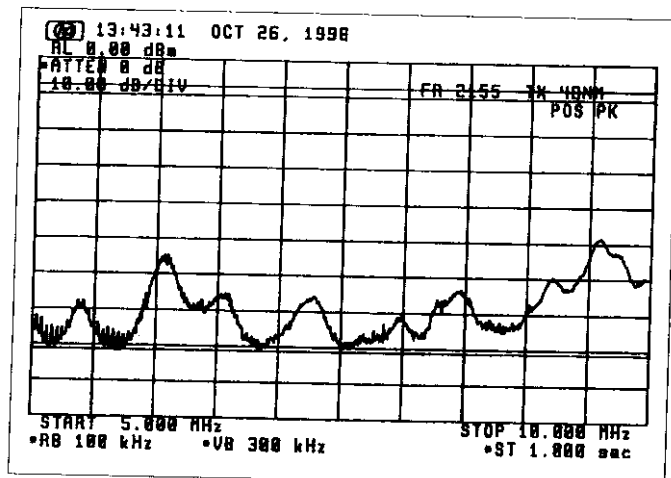
All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 5 MHz - 10 MHz, Limit at 2 m = -81 dBm)



-81 dBm limit line

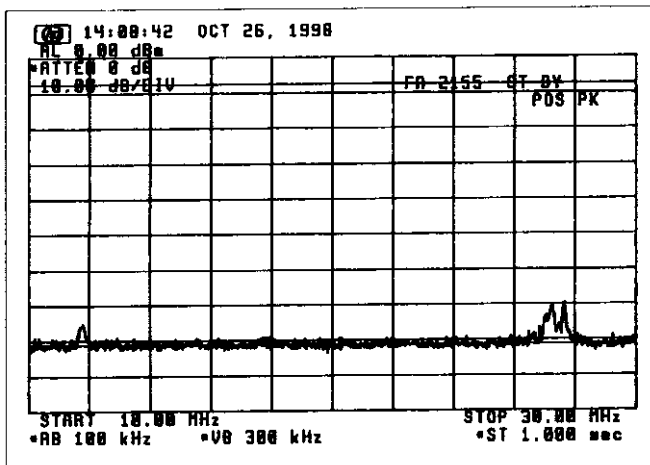
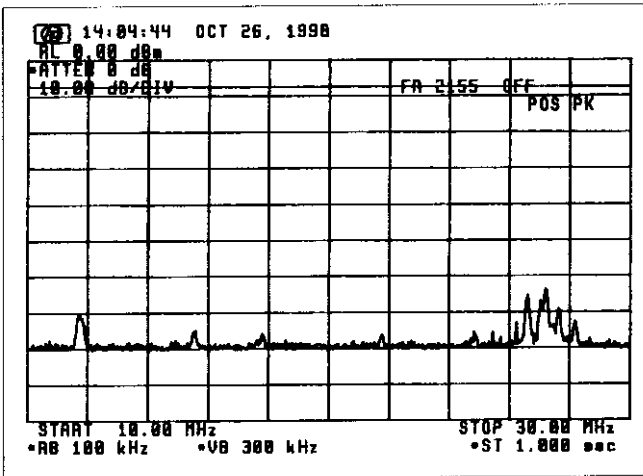
All components above the limit
are from external noise or
signals, not from RADAR.



-81 dBm limit line

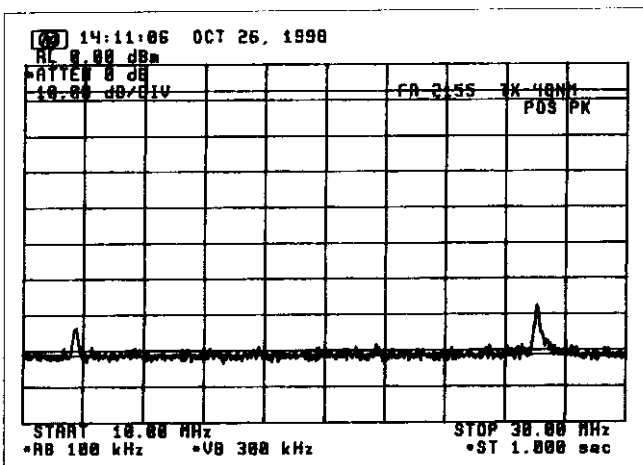
All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 10 MHz - 30 MHz, Limit at 2 m = -81 dBm)



-81 dBm limit line

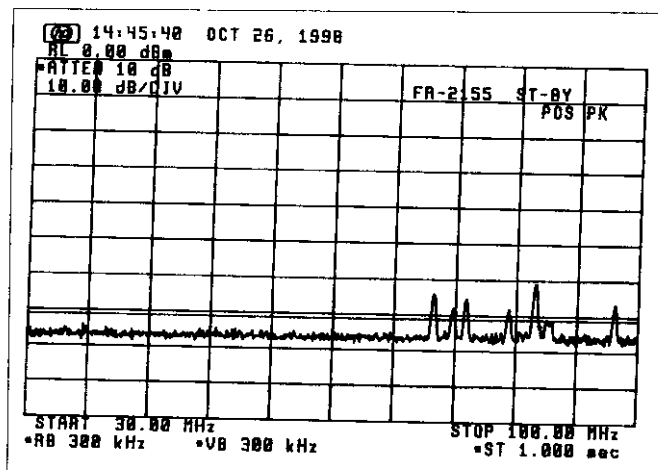
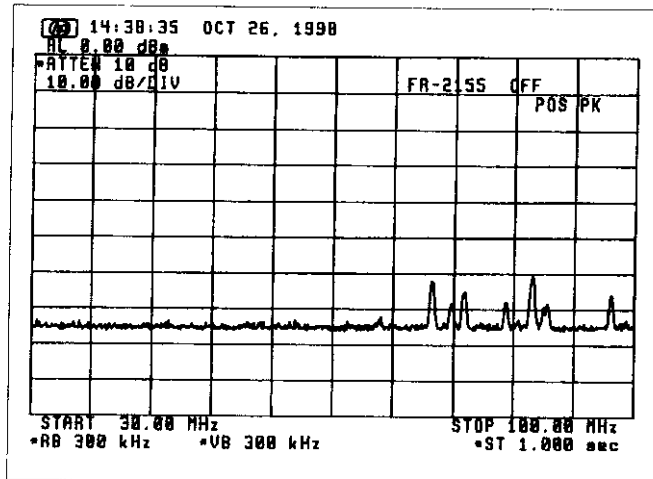
All components above the limit
are from external noise or
signals, not from RADAR.



-81 dBm limit line

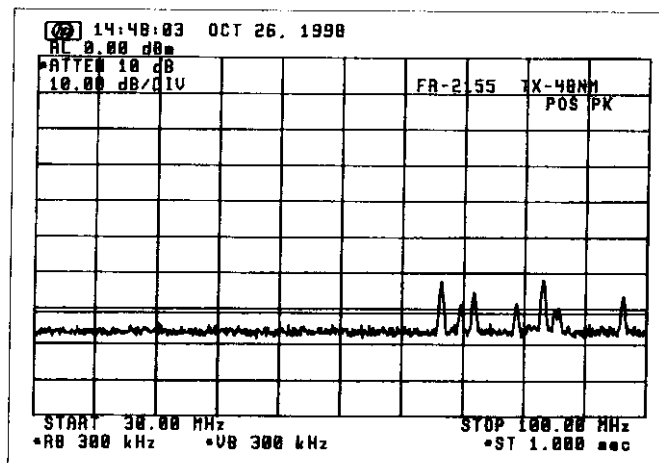
All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 30 MHz - 100 MHz, Limit at 2 m = -71 dBm)



-71 dBm limit line

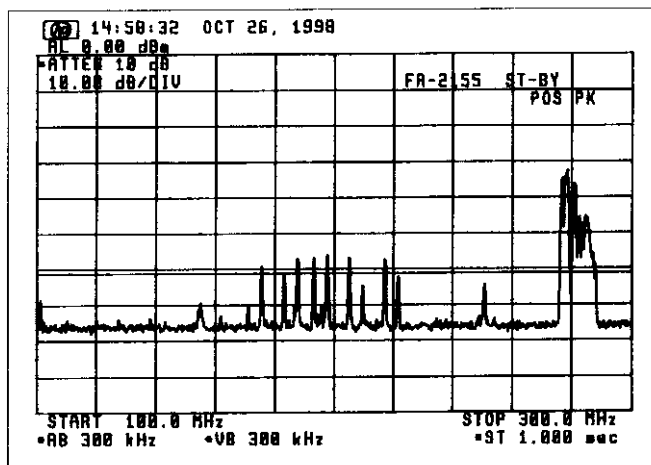
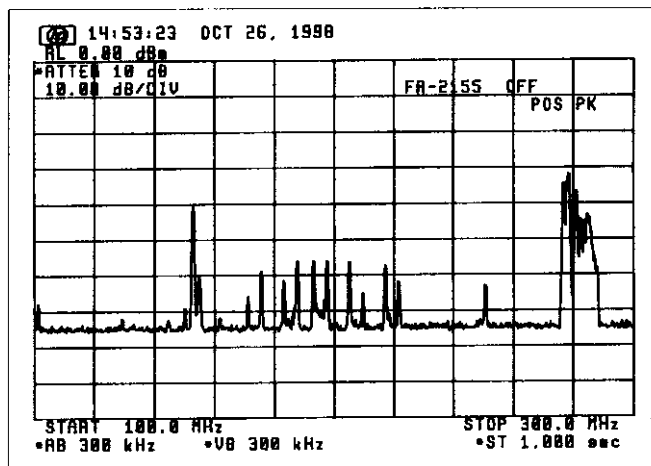
All components above the limit
are from external noise or
signals, not from RADAR.



-71 dBm limit line

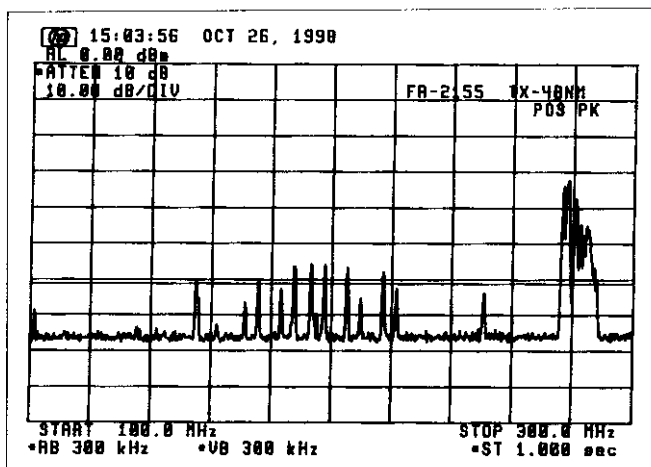
All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 100 MHz - 300 MHz, Limit at 2 m = -61 dBm)



-61 dBm limit line

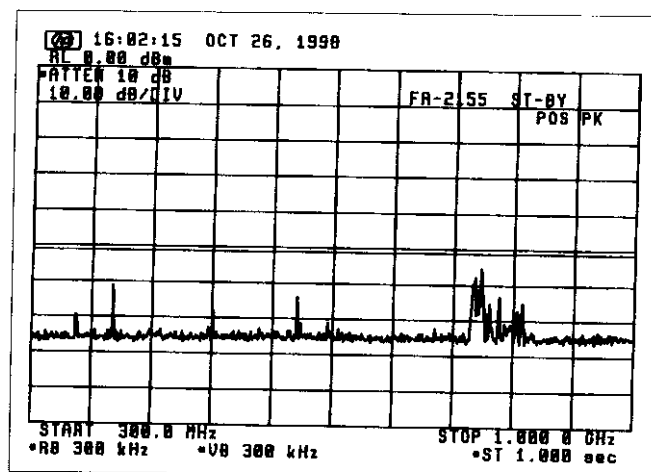
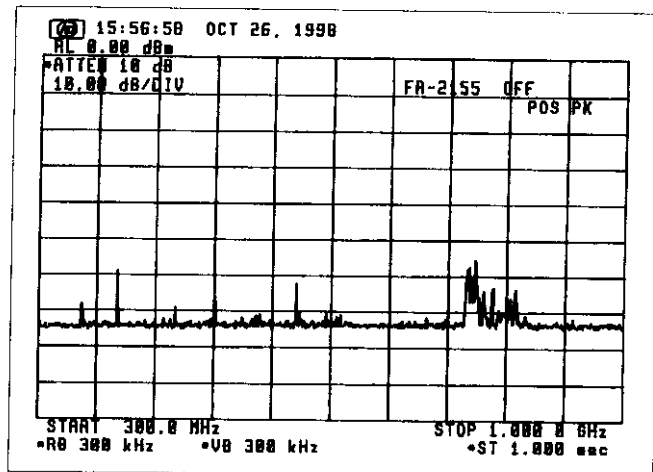
All components above the limit
are from external noise or
signals, not from RADAR.



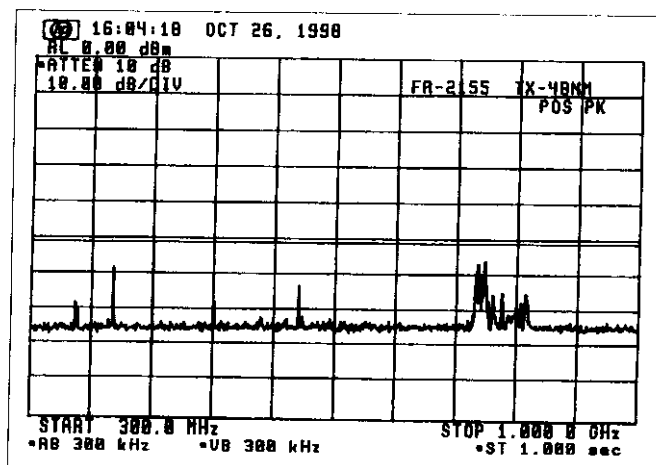
-61 dBm limit line

All components above the limit
are from external noise or
signals, not from RADAR.

(Band : 300 MHz - 1 GHz, Limit at 2 m = -51 dBm)



-51 dBm limit line



-51 dBm limit line

ATTACHMENT 4 [List of Test/Measuring Equipment]**3. RF Power Output**

<u>Model</u>	<u>Type</u>	<u>Serial no.</u>	<u>Mfr.</u>
Spectrum Analyzer	71210C	2927A02847	HP
Oscilloscope	TDS680B	B030202	Tektronix
Directional Coupler	----	R94471	Shimada
Voltage Divider	P6015	----	Tektronix
Current Transformer	2100	----	Pearson Electronics
Power Meter	436A	2410A19137	HP
Power Sensor	8481A	2349A39603	HP
Frequency Counter	TR5824A	41940036	Advantest
Frequency Meter	X532B	1441A00523	HP
Crystal Detector	423B	1822A24214	HP
Step Attenuator	8494B	1510A07310	HP
Step Attenuator	8495B	1350A04754	HP
Dummy Load	----	8411057	Shimada

4. Modulation Characteristics

<u>Model</u>	<u>Type</u>	<u>Serial no.</u>	<u>Mfr.</u>
Oscilloscope	TDS680B	B030202	Tektronix
Step Attenuator	8494B	1510A07310	HP
Step Attenuator	8495B	1350A04754	HP
Crystal Detector	423B	1822A24214	HP
Directional Coupler	-----	R94471	Shimada
Dummy Load	-----	8411057	Shimada
Voltage Divider	P6015	----	Tektronix
Spectrum Analyzer	71210C	2927A02847	HP

6. Spurious Emissions at Antenna Terminal

<u>Model</u>	<u>Type</u>	<u>Serial no.</u>	<u>Mfr.</u>
Spectrum Analyzer	71210C	2927A02847	HP
Attenuator (10 dB)	8491B	36122	HP
External Mixer:	11970K	2332A00589	HP
External Mixer:	11970A	2332A01187	HP
Directional Coupler	-----	R94471	Shimada
Dummy Load	-----	8411057	Shimada
Notch Filter			
Circulator	MA8L32#8	----	Microwave Associates
Bandpass filter	-----	R9904	Shimada
High Pass Filter	-----	-----	Furuno

7. Field Strength of Spurious Radiation

<u>Model</u>	<u>Type</u>	<u>Serial no.</u>	<u>Mfr.</u>
Broadband Rod Antenna	M 95010-1	0496	Advanced Electronics
Biconical Antenna	BIA-25	2650	Electro Metrics
Conical Log-Spiral Antenna	LCA-25	2886	Electro Metrics
Double Ridged Guide Horn Antenna :RGA-180	----	----	EMD
Horn Antenna:	----	----	Toshiba
Spectrum Analyzer:	71210C	2927A02847	HP
External Mixer:	11970K	2332A00589	HP
External Mixer:	11970A	2332A01187	HP
Notch Filter			
Circulator	MA8L32#8	----	Microwave Associates
Bandpass filter	-----	R9904	Shimada

8. Frequency Stability

<u>Model</u>	<u>Type</u>	<u>Serial no.</u>	<u>Mfr.</u>
Power Meter:	436A	2410A19137	HP
Power Sensor:	8481A	2349A39603	HP
Frequency Meter:	X532B	1441A00523	HP
Directional Coupler:	----	R94471	Shimada
Dummy Load:	----	8411057	Shimada
Environmental Chamber:	TBE-3HW5GE2F	3013000995	Tabai Espec

9. Suppression of Interference Aboard Ships

<u>Model</u>	<u>Type</u>	<u>Serial no.</u>	<u>Mfr.</u>
Spectrum Analyzer:	71210C	2927A02847	HP
6 m Whip Antenna	14 k - 10 MHz	----	Furuno
4 m Whip Antenna	10 - 30 MHz	----	Furuno
VHF Whip Antenna	30 - 300 MHz	150M-W2UM	Anten
UHF Whip Antenna	300 - 1000 MHz	----	Anten
RF Vector Impedance Meter:	4815A	2048A03354	HP
Spectrum Analyzer	TR4172	30690116	Advantest
Spectrum Analyzer	8566B	2637A03642	HP

