

Exhibit 7. Measurement Procedures -- 47 CFR. 2.947

This exhibit presents a brief summary of how the measurements were made.

7.1. RF Power -- Pursuant to 47 CFR 2.1046

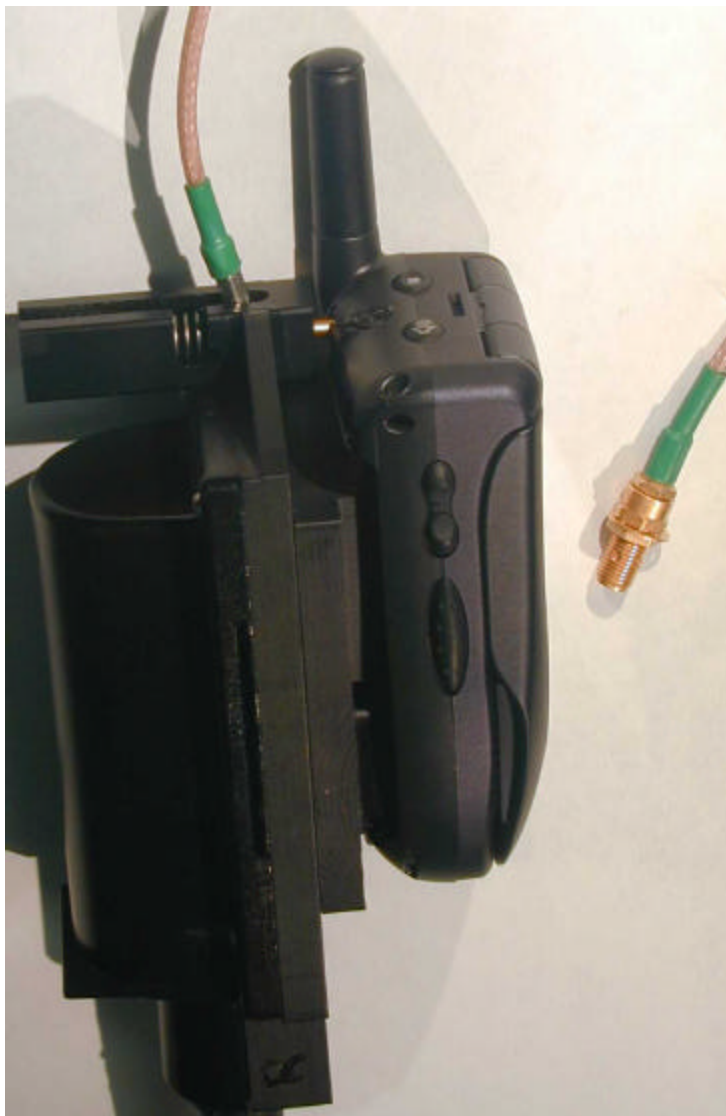
(a) Method of Output Power Measurement: Adaptation of TIA/EIA -603 clause 2.2.1 for Pulsed Measurements

The RF output power is not adjustable by the user. The output power is controlled by the radio in response to the received signal strength or by or special radio service software. To obtain RF output power data the radio was programmed to utilize the maximum RF and minimum RF output power setting. The RF test switch was then connected through an RF probe and a 30-dB attenuator to an RF power sensor. To correct the average reading power meter, a setting of the duty cycle on the RF power meter was set to 16.667% for reported 6:1 TDM test signals.

To obtain all conducted measurements a battery eliminator with RF Probe is used to connect to the RF test switch (J500), as pictured in Photograph 7-1. Power at the RF test switch is 0.2 dB greater than that delivered to the antenna, due to internal losses.



Photograph 7-1: i90c RF test switch.



Photograph 7-2: i90c with Battery Eliminator and RF test switch engaged.

(b) Method of Measurement for Effective Radiated Power: Proprietary

The ERP characteristic was measured while a radio was vertically mounted on a non-conducting platform/turntable in an RF Anechoic Chamber. Since the instrumentation for the measurement system RF Anechoic chamber did not support pulsed measurements the radio was set into a test mode that enabled transmission of a continuous wave (CW) signal. The power received at an antenna located at the end of the chamber was recorded on a spectrum analyzer for a complete 360-degree rotation. The same procedure was repeated for an 800 MHz sleeve reference dipole. The CW RF output power of the radio was measured by a conducted means to determine the necessary input power for the reference dipole (after compensation for interface, cable, and antenna losses). The maximum power levels measured were compared to determine the antenna gain of the radio antenna in reference to the standard dipole. This relative antenna gain was used to scale the maximum RF conducted output power and determine the maximum herein reported ERP.

7.2. Occupied Bandwidth -- Pursuant to 47 CFR 2.1049(b)

Method of Measurement: Per TIA/EIA-603-1 clause 2.2.11

- 1.) Set the radio for measurement of RF output power using the power test procedure in the service manual which employs a pseudo random data sequence per part 2.1049(h), and attach it to a spectrum analyzer through a 30 dB attenuator. The analyzer is to be set for peak detection with a video bandwidth of 3 times the resolution bandwidth setting, a span of 100 kHz, and a sweep period of 20 seconds.
- 2.) Using a 30 kHz resolution bandwidth to assure that essentially all of the transmitted energy is measured, obtain a "rainbow" curve and adjust the analyzer setting so that the crest of the curve lies at the 0 dB reference location.
- 3.) Reduce the resolution bandwidth to 300 Hz to characterize the transmitter emission on-channel and adjacent channels spectral performance characteristic.
- 4.) Overlay the applicable emission mask on the analyzer display.
- 5.) Compare the limit line with the low-resolution bandwidth trace and ensure that the low-resolution bandwidth trace never exceeds the limit line.

7.3. Radiated Spurious Emissions -- Pursuant to 47 CFR 2.1057(b)

Test Site:

The test site used is the Motorola Inc. Product Safety and Compliance EMC Laboratory, located at 1500 Gateway Blvd, Boynton Beach, Florida 33426 (FCC Registration: 100000 / Industry of Canada: IC3908 / ISO 25 certified). This region is reasonably free from RF interference. The radiated emission testing was performed for minimum and maximum powers in transmit mode.

Method of Measurement: EIA/TIA-603-1 clauses 2.2.12 and 5.2.12

The equipment is placed on the turntable, connected to a dummy RF load (a 50 ohm load was attached to the semi-rigid cable soldered to the main board) and placed in normal operation transmit mode of operation.

A broadband-receiving antenna located 3 meters from the transmitter receives any signal radiated from the transmitter and its operational accessories. The antenna is adjustable in height and can be rotated for horizontal or vertical polarization. A spectrum analyzer covering the necessary frequency range is used to detect and measure any radiation received by the antenna.

The transmitter's modulated pseudo random digital signal is monitored and adjusted to obtain peak reading of received signals wherever they occur in the spectrum by:

1. Rotating the transmitter under test.

2. Adjusting the antenna height.

The testing procedure is repeated for both horizontal and vertical polarization of the receiving antenna. Relative signal strength is indicated on the spectrum analyzer connected to this antenna. The spectrum analyzer resolution bandwidth was set to 10 kHz for emissions below 1 GHz, and 1 MHz for higher frequency emissions. To obtain actual radiated signal strength for each spurious and harmonic frequency observed a standard signal generator with calibrated output is connected to an antenna adjusted to that particular frequency. This antenna is substituted for the transmitter under test. The signal generator output level is adjusted until a reading identical to that obtained with the actual transmitter is observed on the spectrum analyzer. Signal strength is then derived from the generator and appropriate cable losses due to set up. Measured emissions for both maximum and minimum transmit power levels are recorded in tables in exhibit 6.

7.4. Frequency Stability -- Pursuant to 47 CFR 2.1055

Measuring the frequency accuracy of the iDEN time division multiplexed (TDM) transmitter needs special procedures for 3 reasons. The first reason is the short (15 ms) nature of its TDM pulses, which preclude the use of an ordinary, CW type, digital frequency counter. The second reason is software in the radio prevents the radio from transmitting its TDM pulses unless it is receiving a signal on the trunking system control channel. The third reason is to maintain the very high stability (greater than that required by part 90 rules) needed for system operation, the radio transmitter frequency is controlled by an automatic frequency control loop in the radio's receiver. This automatic frequency control loop locks onto the system forward control channel produced by a compatible FCC certified part 90 base station. This process results in electronically adjusting the initial frequency of the reference oscillator in the synthesizer section of the radio, which is used for both transmission and reception.

As a result, unlike traditional transceivers which do not frequency lock to a remote base station reference frequency, the transmitter frequency accuracy is essentially independent of the voltage and temperature induced variations of the subject transceiver's frequency reference oscillator. Rather, the transceiver frequency stability is that of the remote base station, but degraded by any inaccuracy in the transceiver frequency locking process. This inaccuracy is primarily attributed to reference oscillator AFC resolution.

By locking onto a base station meeting the requirements of 47 CFR 90.213 which is necessary for the transceiver to function, the transceiver transmitter inherits the inherent 1.5 PPM or better stability of the compatible base station. To assure attainment of the 2.5 PPM accuracy requirement of part 90.213 for this transceiver, the frequency error is measured when locked to a base station simulator.

Method of Measurement: (Proprietary)

Since the transmitter frequency is locked to the frequency of the compatible base station via the receiver in this transceiver, frequency accuracy data was measured with the transceiver locked onto a base station transmitter emulated by a Motorola R2660C Service Monitor as shown in Figure 7-1. This was done using the QUAD-16QAM time division duplex (TDD) characteristic of the transceiver wherein it was placed into a TDD mode of transmission as normally used to

make a call to a landline phone.

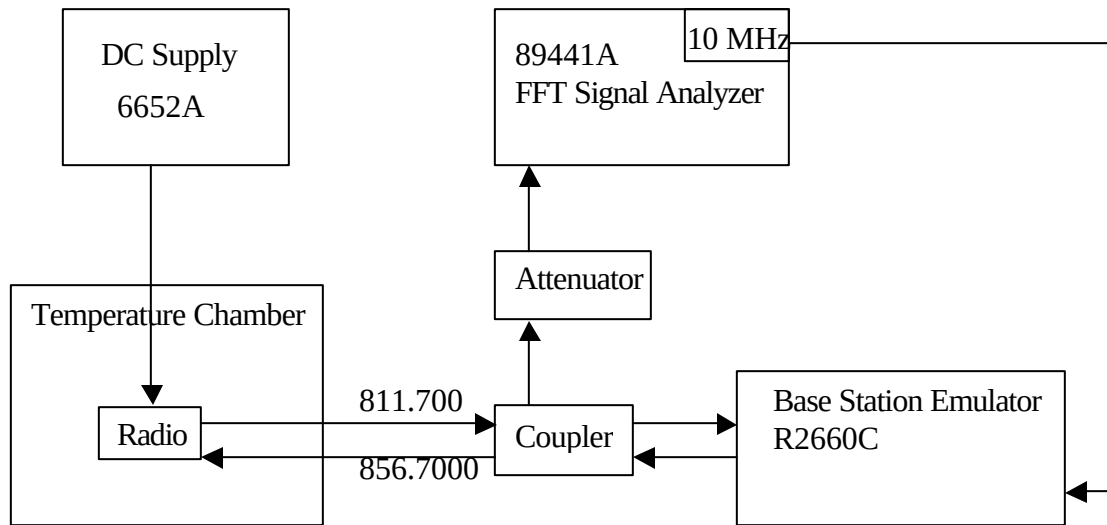


Figure 7-1: Transmit Frequency Measurement Setup

During the test the transceiver was receiving a very high accuracy forward control channel frequency signal from the compatible base station emulator and TDD transmitting a signal on the reverse control channel at a frequency 45 MHz lower corresponding to the normally assigned frequency separation. A Hewlett Packard model 89441A-signal analyzer was used to measure the centroid frequency of the emission. The frequency of the transceiver was measured as operating voltage or temperature was varied, and compared to the frequency of the assigned channel.

7.5 Power Line Conducted Spurious Voltage -- Pursuant 47 CFR 15.107

Test Site:

The test site used is the Motorola EMC Lab, located at 8000 West Sunrise Blvd, Plantation, Florida 33322 (FCC Registration: 91932 / Industry of Canada: IC3679 / ISO 25 certified).

Method of Measurement: EIA/TIA-603-1 clauses 2.1.3 and 5.1.3.3

Connect the receiver to the power line through a line stabilization network. A spectrum analyzer of nominal 50 Ω impedance to one terminal ("neutral") of the line stabilization network. Next the spectrum analyzer is tuned to search for spurious outputs from 450kHz to 30 MHz pursuant 47 CFR 15.107. All spurious outputs found are recorded. Finally the spectrum analyzer is connected to the other terminal ("phase") of the line stabilization network and all spurious outputs found are recorded. The power line conducted spurious emissions is the largest reading obtained.

7.6 Conducted Spurious Emissions – Pursuant 47 CFR 2.1051

Method of Measurement: Adaptation of TIA/EIA-603-1, clauses 2.2.12 and 5.2.12

The transmitter is operated at the highest power setting. It is terminated into a 50-ohm load and interfaced with a spectrum analyzer with sufficient dynamic range to permit the spurious emission level relative to the carrier level to be measured directly. Measurements are from the lowest radio frequency generated in the equipment to the tenth harmonic of the carrier, or as high as the state of the art permits, except for that region within 50 kHz of the carrier. The spectrum analyzer is set to use a resolution bandwidth of 10 kHz for spurious emissions below 1 GHz, and 1 MHz for higher frequency spurious emissions.

Because results for any measurement near the fundamental emission will be affected due to the shape factor of the analyzer filter, measurement of any spurious emissions within 750 kHz of the carrier are performed by using a narrow resolution bandwidth and integrating the readings over a 10 kHz bandwidth. This is a common technique used for measuring adjacent channel power, which requires that the analyzer have an adjacent channel power feature for automated measurement.

7.7 Measurement Equipment List ---- 47 CFR 2.947(d)

1. Spectrum Analyzer
 - A. H.P. 8563E
 - B. Rhode & Schwarz ESI26
 - C. Rhode & Schwarz FSEA
2. Vector Signal Analyzer
 - A. H.P. 89441A
3. Communications System Analyzer
 - A. Motorola R2660C MIRS Digital Communications System Analyzer
4. Oscilloscope
 - A. LeCroy, Model AP015, Oscilloscope
 - B. H.P. 10071A, 10:1 Voltage Probe
 - C. LeCroy, LC574AM, Current Probe
5. RF Signal Generator
 - A. Rhode and Schwarz SMP22
 - B. H.P. E4420A
6. Power Meter
 - A. H.P. 437B Power Meter
 - B. H.P. 8482A Power Sensor
7. Power Supply
 - A. Motorola Lithium Ion Battery, Kit #: SNN 5705A
 - A. DC Power Supply, H.P., Model: 3630A
 - B. Battery Charger, Model: SPN4716B
 - C. Battery Eliminator, 22000uF shunt capacitor / series .2 ohm resistor
8. RF Load
 - A. Weinschel Engineering, Model: 9305-30, 20 Watt, 30 dB Attenuator
 - B. Weinschel Engineering, Model: 9305-20, 20 Watt, 20 dB Attenuator

- C. Weinschel Engineering, Model: 9305-10, 20 Watt, 10 dB Attenuator
- D. Narda, Model: MOD766-30, 20 Watt, 30 dB Attenuator
- E. 50 ohm load, Model: FSC 96341
- 9. Filter
 - A. Trilithic, Model: X5HX1612-0-75-AA, High Pass Filter
 - B. Trilithic, Model: R9H1-1G4/8G-28A, High Pass Filter
- 10. Amplifier
 - A. Hewlett Packard RF Amplifier, Model: 8347A
 - B. Hewlett Packard Pre-Amplifier, Model: 8449B
- 11. Antenna
 - A. A. H. Systems, Inc., DRG Horn Antenna, Model: SAS-200/571
 - B. EMCO, Log-Periodic Antenna, Model: 3147
 - C. Chase, Bilog Antenna, Model: CBL6121
 - D. ETS, Log-Periodic Antenna, Model: 3148
 - E. ETS, Biconical Antenna, Model 3110B
- 12. Temperature Chamber
 - A. Tenney, Model: TJR
- 13. LISN
 - A. EMCO, Model: 3810/2NM, Line Impedance Stabilization Network
- 14. Antenna Positioning Mast / Turntable
 - A. Sunol Sciences Corp., Model: FM 2011, Turntable
 - B. Sunol Sciences Corp., Model: TLT95, Antenna Positioning Mast
 - C. Scientific Atlanta Antenna Analyzer System 2083A
- 15. Computer
 - A. HP, Model: Kayak XU800: Hyperlink Terminal, Desktop Computer
- 16. Programming Cable
 - A. RS232 Data Cable, Model :NKN6544A
- 17. Table
 - A. Wood Table
- 18. Test Site
 - A. OATS
 - 1. Groundplane
 - B. Anechoic Chamber, Emerson & Cummings 1203