

Specific Absorption Rate (SAR) Test Report

for

Giant Electronics Ltd.

on the

Portable UHF FRS/GMRS PTT Radio Transceiver

Model Number: T8220

Test Report: EME-040937

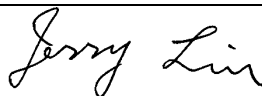
Date of Report: Nov. 25, 2004

Date of test: Nov. 24, 2004

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Accredited for testing to FCC Part 15

Tested by: Kevin Chen	
Reviewed by: Jerry Liu	

Review Date: Nov. 26, 2004

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STATEMENT OF COMPLIANCE

The Giant sample device, model # T8220 was evaluated in accordance with the requirements for compliance testing defined in FCC OET Bulletin 65, Supplement C (Edition 01-01). Testing was performed at the Intertek Testing Services facility in Hsinchu, Taiwan.

The EUT was evaluated in a face-held configuration with the front of the radio placed parallel to the outer surface of the planar. A 2.5cm separation distance was maintained between the front side of the EUT and the outer surface of the planar phantom for the duration of the test.

The EUT was tested in a body-worn configuration with the rear of the radio placed parallel to outer surface of the planar phantom. The attached plastic belt-clip was touching the planar phantom. The EUT was evaluated for body-worn SAR with the microphone accessory.

For the evaluation, the dosimetric assessment system INDEXSAR SARA2 was used. The phantom employed was the box phantom of 2mm thick in one wall. The total uncertainty for the evaluation of the spatial peak SAR values averaged over a cube of 1g tissue mass had been assessed for this system to be $\pm 20.6\%$.

The device was tested at their maximum output power declared by the Giant.

The device was tested in unmodulated continuous transmit operation (Continuous Wave at 100% duty cycle) with the transmit key constantly depressed. For a push-to-talk device, the 50% duty cycle compensation reported assumes a transmit/ receive cycle of equal time base.

In summary, the maximum spatial peak SAR value for the sample device averaged over 1g was found to be:

Phantom	Position	SAR _{1g} , mW/g
6mm thick box phantom wall for face-held evaluation	EUT front to the phantom, 25 mm separation. 462MHz band _channel 4	0.892 mW/g.
6mm thick box phantom wall for body-worn evaluation	EUT rear to the phantom with the Belt-clip, 0 mm separation. 462MHz band _channel 4	1.191 mW/g.

In conclusion, the tested Sample device was found to be in compliance with the requirements defined in OET Bulletin 65, Supplement C (Edition 01-01) for body configurations.

1.0 Job Description

1.1 Client Information

The T8220 has been tested at the request of:

Company: Giant Electronics Ltd.
Elite Industrial Building, 135-137 Hoi Bun Road, Kwun Tong,
Kowloon, Hong Kong

1.2 Equipment under test (EUT)

Product Descriptions:

Equipment	Two Way Radio with FRS and GMRS		
Trade Name	Giant	Model No:	T8220
FCC ID	K7GT8220	S/N No.	Not Labeled
Category	Portable	RF Exposure	Uncontrolled Environment
Frequency Band	462.5625 – 462.7125 MHz for FRS 467.5625 – 467.7125 MHz for FRS 462.5625 – 462.7125 MHz for GMRS 462.5500 – 462.7250 MHz for GMRS	System	F3E

EUT Antenna Description			
Type	Integral/ helix	Configuration	Fixed
Dimensions	73 mm length	Gain	-1.8 dBi
Location	Embedded		

Use of Product : Walkie-Talkie

Manufacturer: Giant

Production is planned: ☒ Yes, ☐ No

EUT receive date: Oct. 4, 2004

EUT received condition: Good operating condition prototype

Test start date: Nov. 24, 2004

Test end date: Nov. 24, 2004

1.3 Test plan reference

FCC Rule: Part 2.1093, FCC's OET Bulletin 65, Supplement C (Edition 01-01) and IEEE 1528

1.4 System test configuration

1.4.1 System block diagram & Support equipment

Support Equipment				
Item #	Equipment	Brand	Model No.	S/N
1	N/A	N/A	N/A	N/A



1.4.2 Test Position

See the photographs as section 2.2

1.4.3 Test Condition

During tests the worst-case data (max RF coupling) was determined with following conditions:

Usage	Operates with a built-in test mode by client	Distance between antenna axis at the joint and the liquid surface:	For head, EUT front to phantom, 25 mm separation. For body, EUT rear with belt-clip to phantom, 0 mm separation	
Simulating human Head/ Body	Head and Body	EUT Battery	Fully-charged with 3 Nickel-Metal batteries	
E.R.P. for 462MHz Band	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
	Mid Channel – 4	462.6375	31.2	31.2
E.R.P. for 467MHz Band	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
	Mid Channel – 11	467.6375	26.4	26.5

The spatial peak SAR values were assessed for middle operating channels, defined by the manufacturer.

The EUT has built-in test mode that used to evaluate SAR.

The EUT was transmitted continuously during the test (Continuous Wave at 100% duty cycle). For a push-to-talk device, the 50% duty cycle compensation reported assumes a transmit/ receive cycle of equal time base.

The EUT take Nickel-Metal batteries as its power source. Each test was proceeded with fully-charged batteries.

1.5 Modifications required for compliance

Intertek Testing Services implemented no modifications.

1.6 Additions, deviations and exclusions from standards

The phantom employed was the box phantom of 6 mm thick in vertical wall.

2.0 SAR Evaluation

2.1 SAR Limits

The following FCC limits for SAR apply to devices operate in General Population/Uncontrolled Exposure environment:

EXPOSURE (General Population/Uncontrolled Exposure environment)	SAR (W/kg)
Average over the whole body	0.08
Spatial Peak (1g)	1.60
Spatial Peak for hands, wrists, feet and ankles (10g)	4.00

2.2 Configuration Photographs

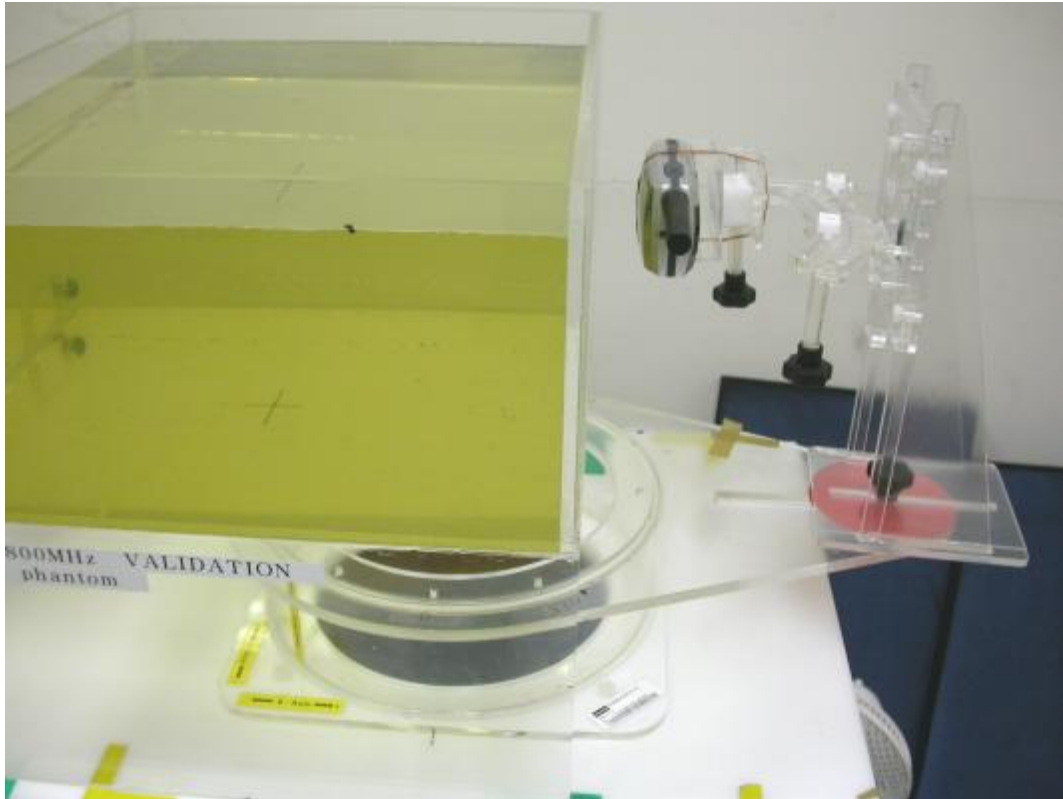
SAR Measurement Test Setup

Test System

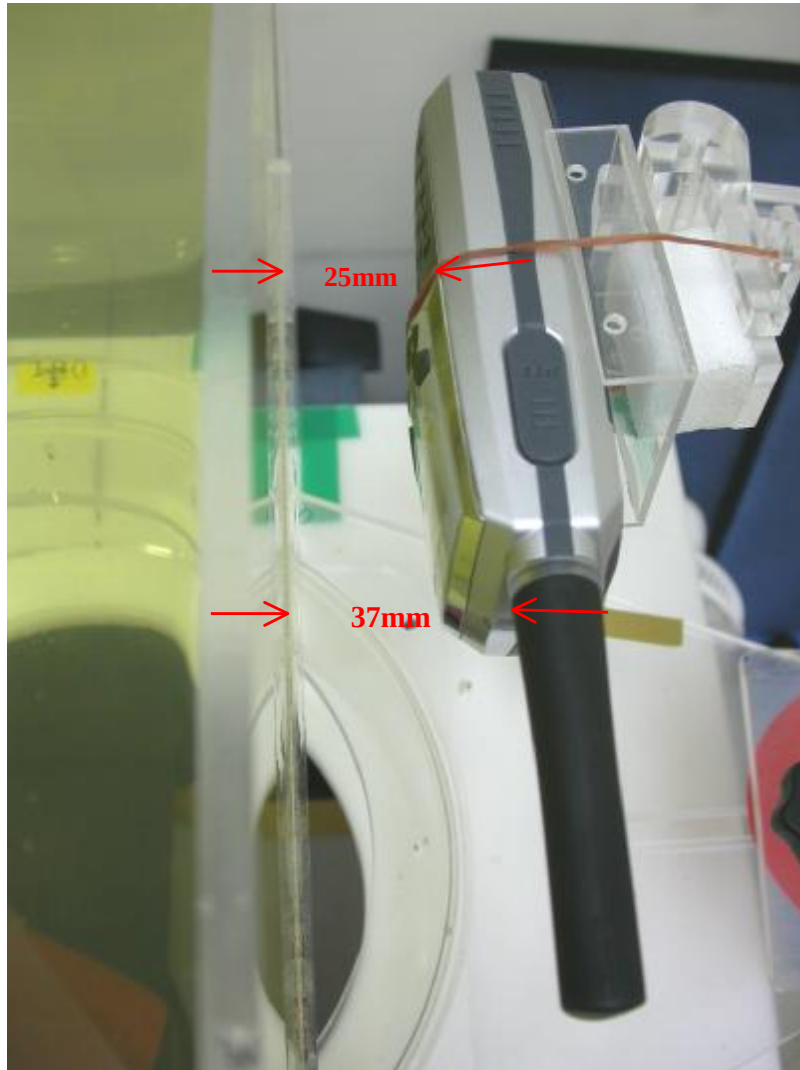


SAR Measurement Test Setup

For head, EUT front to phantom, 25 mm separation

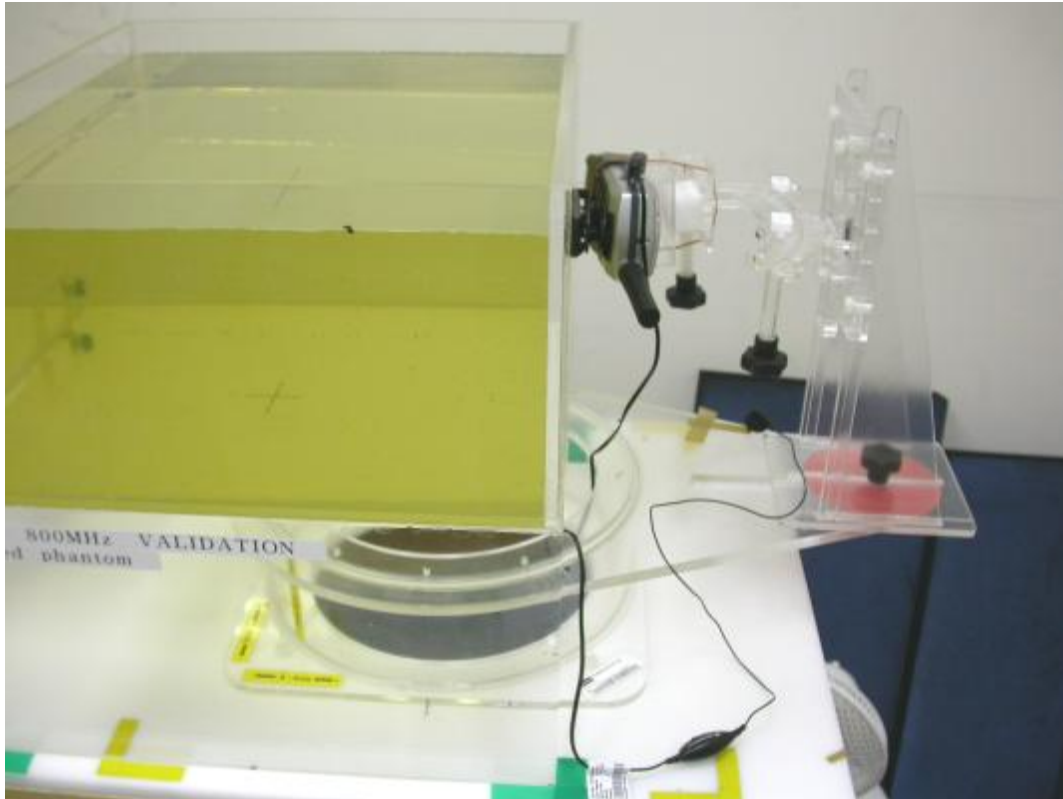


For head, EUT front to phantom, 25 mm separation – Zoom In



SAR Measurement Test Setup

For body, EUT rear with belt-clip and microphone to phantom, 0 mm separation



For body, EUT rear with belt-clip and microphone to phantom, 0 mm separation-Zoon In



2.3 SAR measurement system

Robot system specification

The SAR measurement system being used is the IndexSAR SARA2 system, which consists of a Mitsubishi RV-E2 6-axis robot arm and controller, IndexSAR probe and amplifier and SAM phantom Head Shape. The robot is used to articulate the probe to programmed positions inside the phantom head to obtain the SAR readings from the DUT.

The system is controlled remotely from a PC, which contains the software to control the robot and data acquisition equipment. The software also displays the data obtained from test scans.

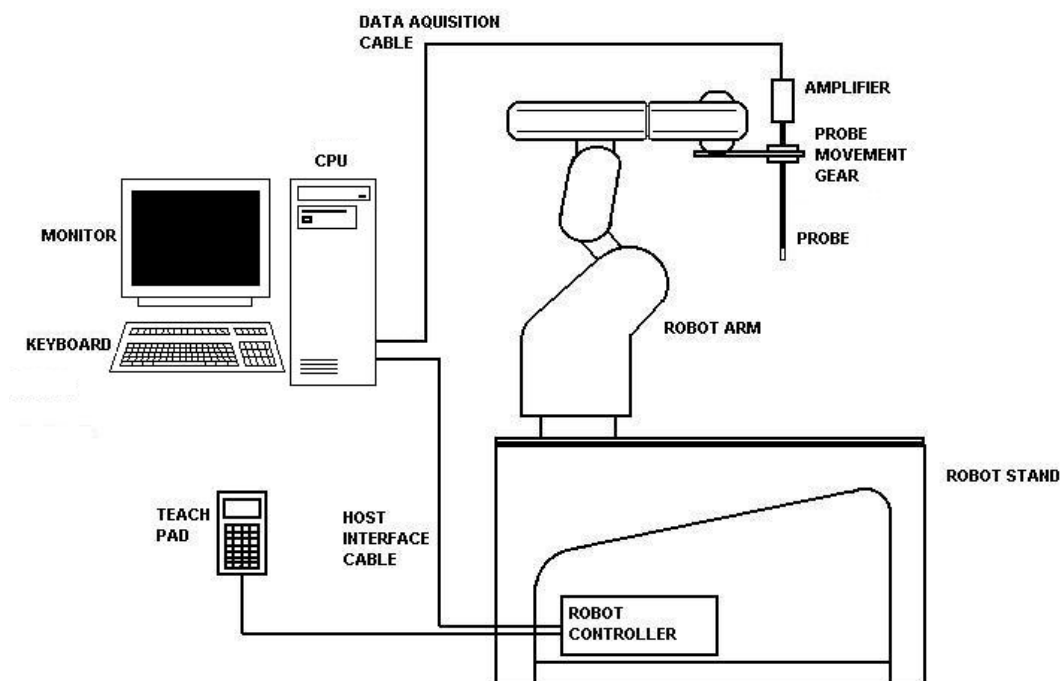


Figure 1: Schematic diagram of the SAR measurement system

The position and digitised shape of the phantom heads are made available to the software for accurate positioning of the probe and reduction of set-up time.

The SAM phantom heads are individually digitised using a Mitutoyo CMM machine to a precision of 0.02mm. The data is then converted into a shape format for the software, providing an accurate description of the phantom shell. In operation, the system first does an area (2D) scan at a fixed depth within the liquid from the inside wall of the phantom. When the maximum SAR point has been found, the system will then carry out a 3D scan centred at that point to determine volume averaged SAR level.

The first 2 measurements points in a direction perpendicular to the surface of the phantom during the zoom scan and closest to the phantom surface, were only 3.5mm and the probe is kept at greater than half a diameter from the surface.

2.4 SAR measurement system validation

Prior to the assessment, the system was verified to the $\pm 10\%$ of the specifications by using the system validation equipments. The validation was performed at 450 MHz on the bottom side of box phantom.

Procedures

The SAR evaluation was performed with the following procedures:

- a. The SAR distribution was measured at the exposed side of the bottom of the box phantom and was measured at a distance of 8 mm from the inner surface of the shell. The feed power was 1/5 W.
- b. The dimension for this cube is 32 mm x 32 mm x 34 mm was assessed by measuring 5 x 5 x 7 points. On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure:
 - i) The data at the surface were extrapolated, since the center of the dipoles is 2.7 mm away from the tip of the probe and the distance between the surface and the lowest measurement point is 5 mm. The extrapolation was based on a least square algorithm. A polynomial of the fourth order was calculated through the points in Z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.
 - ii) The maximum interpolated value was searched with a straightforward algorithm. Around this maximum, the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3-D spline interpolation algorithm. The 3-D spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y and z directions). The volume was integrated with the trapezoidal algorithm. 1000 points (10 x 10 x 10) were interpolated to calculate the average.
 - iii) All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

The test scan procedure for system validation also apply to the general scan procedure except for the set-up position. For general scan, the EUT was placed at the side of phantom. For validation scan, the dipole antenna was placed at the bottom of phantom

2.4.1 System Validation result

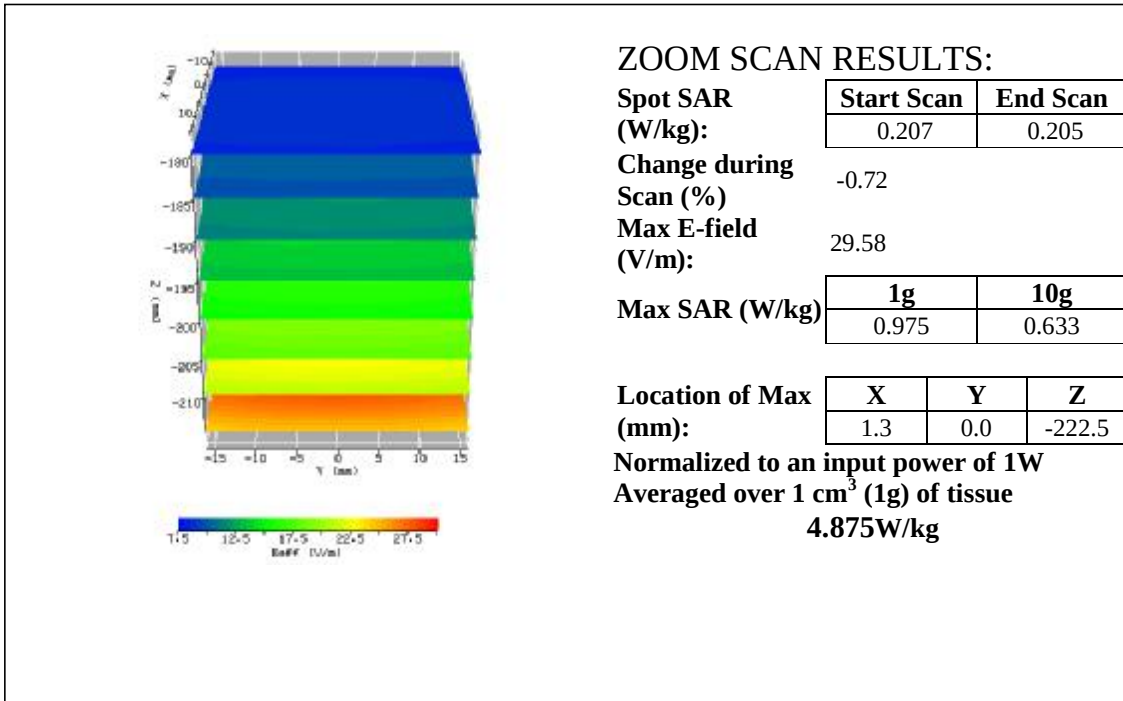
System Validation (450 MHz Head)				
Frequency MHz	Operating Mode	Target SAR _{1g} (mW/g)	Measured SAR _{1g} (mW/g)	Deviation (±10%)
450	CW	4.9	4.875	-0.51%

Please see the plot below:

Date / Time:	2004/10/5	Position:	bottom of phantom
Filename:	450 system validation.txt	Phantom:	HeadBox3-450.csv
Device Tested:	450 system validation	Head Rotation:	0
Antenna:	450 dipole antenna	Test Frequency:	450MHz
Shape File:	none.csv	Power Level:	23dBm

Probe:	0149			
Cal File:	SN0149_450_CW_HEAD			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.344	.344	.344
Amp Gain:	2			
Averaging:	1			
Batteries Replaced:	-			

Liquid:	15.5cm
Type:	450MHz Head
Conductivity:	0.885
Relative Permittivity:	44.638
Liquid Temp (deg C):	22.2
Ambient Temp (deg C):	22
Ambient RH (%):	45
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor=1	



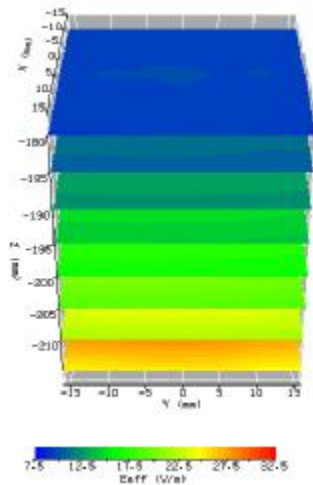
2.4.2 System Performance Check result

System performance check (450 MHz Head)				
Frequency MHz	Operating Mode	Target SAR _{1g} (mW/g)	Measured SAR _{1g} (mW/g)	Deviation (±10%)
450	CW	4.9	4.94	0.82%

Please see the plot below:

Date:	2004/11/23	Position:	Bottom of phantom box
Filename:	450performance check.txt	Phantom:	HeadBox3-450.csv
Device Tested:	450 performance check	Head Rotation:	0
Antenna:	450 MHz dipole	Test Frequency:	450 MHz
Shape File:	none.csv	Power Level:	23 dBm

Probe:	0149	Liquid:	15.5cm
Cal File:	SN0149_450_CW_HEAD	Type:	450 MHz head
Cal Factors:		Conductivity:	0.881
		Relative Permittivity:	44.451
		Liquid Temp (deg C):	22.5
		Ambient Temp (deg C):	23
Amp Gain:	2	Ambient RH (%):	51
Averaging:	1	Density (kg/m3):	1000
Batteries		Software Version:	2.3VPM
Replaced:		Crest Factor=1	



ZOOM SCAN RESULTS:

Spot SAR	Start Scan	End Scan
(W/kg):	0.222	0.226

Change during Scan (%) 3.64

Max E-field (V/m): 31.01

Max SAR (W/kg)	1g	10g
	0.988	0.685

Location of Max (mm):	X	Y	Z
	-1.2	-1.2	-222.5

Normalized to an input power of 1W
Averaged over 1 cm³ (1g) of tissue
4.94W/kg

2.5 Test Result

The results on the following page(s) were obtained when the device was tested in the condition described in this report. Detailed measurement data and plots, which reveal information about the location of the maximum SAR with respect to the device, are reported in Appendix A.

Measurement Results

Trade Name:	Giant	Model No.:	T8220
Serial No.:	Not Labeled	Test Engineer:	Kevin Chen
TEST CONDITIONS			
Ambient Temperature	23 °C	Relative Humidity	51 %
Test Signal Source	Test Mode (transmitted continuously)	Signal Modulation	F3E
Output Power Before SAR Test	See page 6	Output Power After SAR Test	See page 6
Test Duration	23 min. each scan	Number of Battery Change	3

Test Mode: Head evaluation

EUT Position							
Channel (MHz)	Operating Mode	Crest Factor	Description	Distance (mm)	Measured SAR _{1g} (mW/g)		Plot Number
					Duty Cycle		
					100%	50%	
462.6375	F3E	1	Front to phantom	25	1.784	0.892	1
467.6375	F3E	1	Front to phantom	25	0.744	0.372	2

Test Mode: Body evaluation with belt-clip and microphone

EUT Position							
Channel (MHz)	Operating Mode	Crest Factor	Description	Distance (mm)	Measured SAR _{1g} (mW/g)		Plot Number
					Duty Cycle		
					100%	50%	
462.6375	F3E	1	Rear to phantom	0	2.382	1.191	3
467.6375	F3E	1	Rear to phantom	0	1.086	0.543	4

3.0 Test Equipment

3.1 Equipment List

The Specific Absorption Rate (SAR) tests were performed with the INDEXSAR SARA2 SYSTEM.

The following major equipment/components were used for the SAR evaluations:

SAR Measurement System			
EQUIPMENT	SPECIFICATIONS	S/N #	LAST CAL. DATE
Balanced Validation dipole	450MHz	0065	10/2003
Controller	Mitsubishi CR-E116	F1008007	N/A
Robot	Mitsubishi RV-E2	EA009002	N/A
	Repeatability: ± 0.04 mm; Number of Axes: 6		
E-Field Probe	IXP-050	0149	05/13/2004
	Frequency Range: Probe outer diameter: 5.2 mm; Length: 350 mm; Distance between the probe tip and the dipole center: 2.7 mm		
Data Acquisition	SARA2	N/A	N/A
	Processor: Pentium 4; Clock speed: 1.5GHz; OS: Windows XP; I/O: two RS232; Software: SARA2 ver. 2.3VPM		
Phantom	6mm wall thickness box phantom	N/A	N/A
	Shell Material: clear Perspex; Thickness: 6 ± 0.1 mm; Capacity: 333 x 333 x 170 (W x L x D) mm ³ ; Dielectric constant: less than 2.85 above 500MHz;		
Device holder	Material: clear Perspex	N/A	N/A
	Dielectric constant: less than 2.85 above 500MHz		
Simulated Tissue	Mixture	N/A	11/23/2004
	Please see section 3.2 for details		
RF Power Meter	Boonton 4231A with 51011-EMC power sensor	79401-32482	03/21/2004
	Frequency Range: 0.03 to 8 GHz, <24dBm		
Vector Network Analyzer	HP 8753B HP 85046A	2807J04037 2729A01958	07/04/2004
	300k to 3GHz		
Signal Generator	R&S SMR27	100036	09/19/2004
	10M to 27GHz, <120dBuV		
Crystal Detector	Agilent 8472B	MY42240243	N/A
	10MHz to 18GHz		
Two Channel Digital Storage Oscilloscope	Tektronix TDS1012	C031679	08/16/2004

3.2 Tissue Simulating Liquid

The head and body tissue parameters should be used to test operating frequency band of transmitters. When a transmission band overlaps with one of the target frequencies, the tissue dielectric parameters of the tissue medium at the middle of a device transmission band should be within $\pm 5\%$ of the parameters specified at that target frequency.

3.2.1 Body Tissue Simulating Liquid for evaluation test

Body Ingredients Frequency (450 MHz)	
Water	51.16%
Salt	1.49%
Sugar	46.78%
HEC (Hydroxyethyl Cellulose)	0.52%
Bactericide	0.05%

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e _r / Relative Permittivity			s / Conductivity (mho/m)			r *(kg/m ³)
		measured	target	△(±5%)	measured	target	△(±5%)	
450	22.5	57.497	56.7	1.41%	0.951	0.94	1.17%	1000

* Worst-case assumption

3.2.2 Head Tissue Simulating Liquid for System performance Check and evaluation test

Head Ingredients Frequency (450 MHz)	
Water	38.56%
Salt	3.95%
Sugar	56.32%
HEC (Hydroxyethyl Cellulose)	0.98%
Bactericide	0.19%

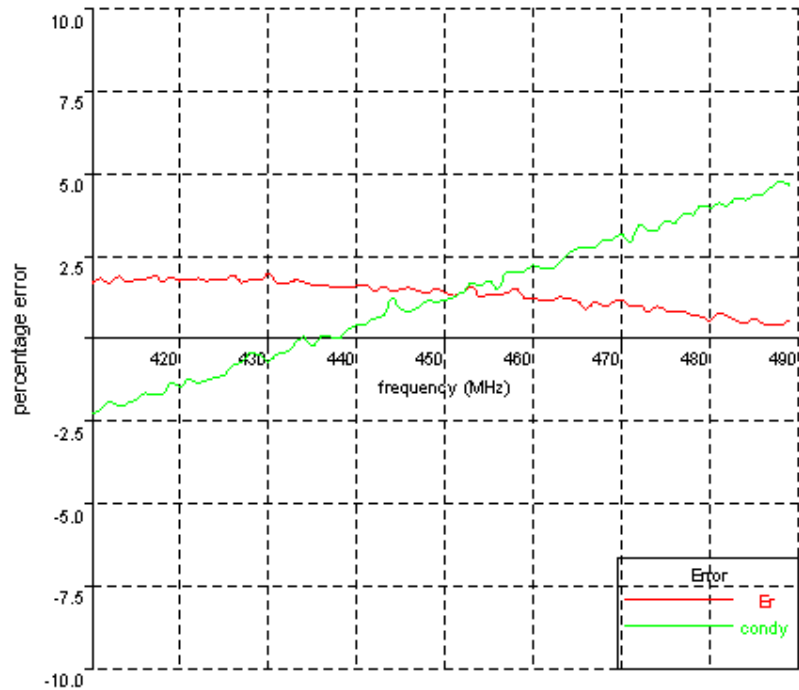
The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e _r / Relative Permittivity			s / Conductivity (mho/m)			r *(kg/m ³)
		measured	target	△(±5%)	measured	target	△(±5%)	
450	22.5	44.451	43.5	2.19%	0.881	0.87	1.26%	1000

* Worst-case assumption

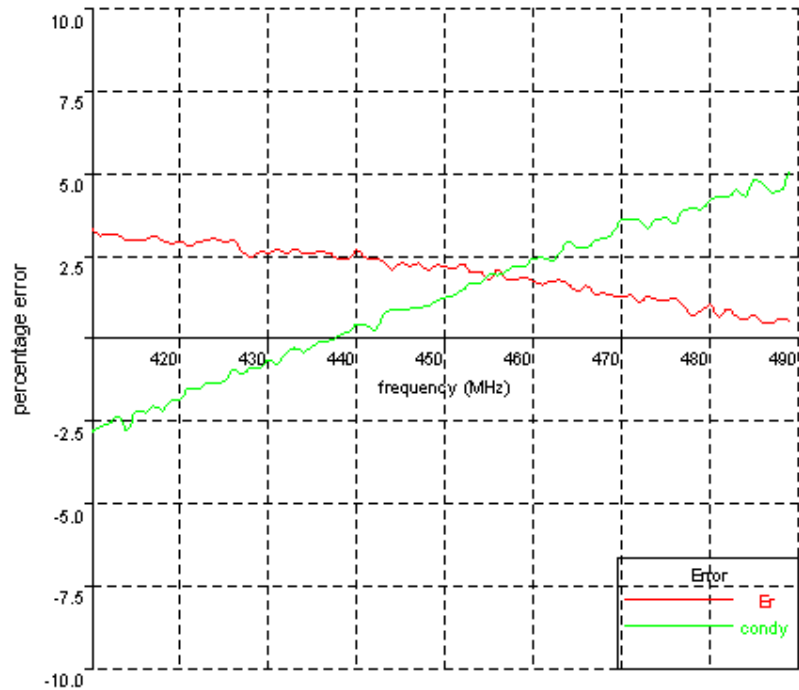
3.2.3 Body Liquid results

Date: 23 Nov. 2004	Temperature: 22.5 °C	Type: 450 MHz/ Body (FCC)	Tested by: Kevin
410, 58.0740491303, -0.9133912772		450, 57.4969858422, -0.9508580847	
411, 58.1310161531, -0.9147533002		451, 57.4350124171, -0.9519439378	
412, 58.0411826885, -0.9170803619		452, 57.4934480681, -0.9534440303	
413, 58.1501410819, -0.9159558288		453, 57.5822565478, -0.9560914139	
414, 58.046003524, -0.9168226976		454, 57.4026148765, -0.9556459472	
415, 58.0624567097, -0.9182017198		455, 57.4454119097, -0.956880173	
416, 58.0673946645, -0.9199632327		456, 57.4363386613, -0.9546329842	
417, 58.1151747523, -0.919863523		457, 57.450524889, -0.9596527243	
418, 58.0110998135, -0.91993736		458, 57.5371699131, -0.9593836879	
419, 58.0637720836, -0.9233830536		459, 57.3555782896, -0.9599081578	
420, 58.0052047074, -0.9221215895		460, 57.3506999437, -0.9617617417	
421, 58.0045704205, -0.9246027058		461, 57.3205076222, -0.9606937988	
422, 58.018896996, -0.9236792325		462, 57.3042544377, -0.9610885848	
423, 57.9661502057, -0.9244271359		463, 57.3583756271, -0.9628606598	
424, 57.9945582575, -0.9255789032		464, 57.3302688769, -0.9654483609	
425, 57.9661397651, -0.9261679151		465, 57.2781481399, -0.9669844643	
426, 58.0258204936, -0.929453576		466, 57.146334969, -0.9674460933	
427, 57.8996217337, -0.9302307351		467, 57.2607880255, -0.9675818599	
428, 57.9423342446, -0.9330591004		468, 57.1814016236, -0.9696537697	
429, 57.9237933424, -0.9325177262		469, 57.245141513, -0.9697654402	
430, 58.0275962983, -0.9307490626		470, 57.2842031029, -0.9713675745	
431, 57.8535936405, -0.9330609532		471, 57.1718888467, -0.9691362734	
432, 57.8252442236, -0.9338497964		472, 57.1718888467, -0.9741998912	
433, 57.8798574634, -0.9364702062		473, 57.0785176379, -0.9728240312	
434, 57.8370726206, -0.938484702		474, 57.1604344652, -0.9728432149	
435, 57.7610978879, -0.9359894499		475, 57.0784126939, -0.9757333726	
436, 57.7632032799, -0.9387949835		476, 57.060148237, -0.9748200035	
437, 57.7348981561, -0.9387827959		477, 57.067081045, -0.9777549104	
438, 57.7115155223, -0.9385236876		478, 56.9851932303, -0.9775499041	
439, 57.7038725744, -0.9413958425		479, 56.9690351239, -0.9803176341	
440, 57.7059758806, -0.9423466084		480, 56.8921269265, -0.9797794417	
441, 57.7108835183, -0.9429114283		481, 57.0177821188, -0.9811344017	
442, 57.5973451511, -0.9447712502		482, 56.9659454733, -0.9803847464	
443, 57.6608494991, -0.9452818889		483, 56.8800560747, -0.982697207	
444, 57.5753814232, -0.9507930833		484, 56.8372023073, -0.9823238095	
445, 57.5938004282, -0.9476687041		485, 56.9139325304, -0.9838351906	
446, 57.6171259174, -0.9472186412		486, 56.8209826072, -0.98405036	
447, 57.5484313914, -0.9486443229		487, 56.7889991214, -0.9864026014	
448, 57.5132419527, -0.9505316262		488, 56.782099258, -0.9877372034	
449, 57.562664145, -0.9504725779		489, 56.8377989585, -0.9871210256	
		490, 56.7185330783, -0.9879243577	



3.2.4 Head Liquid results

Date: 23 Nov. 2004	Temperature: 23.0 °C	Type: 450 MHz/ head (FCC)	Tested by: Kevin
410, 45.436592083, -0.8455191621		450, 44.4505312594, -0.8808831696	
411, 45.3449339223, -0.8466770924		451, 44.4236997561, -0.8814774681	
412, 45.3465867452, -0.8476943212		452, 44.4782669847, -0.8830741737	
413, 45.3148915848, -0.8494799205		453, 44.3628532862, -0.8848880914	
414, 45.2408848257, -0.8457059415		454, 44.3644703122, -0.8850236091	
415, 45.2247596833, -0.8510428687		455, 44.2532838089, -0.8873322244	
416, 45.2319031344, -0.8505698305		456, 44.3782077361, -0.8873159854	
417, 45.2707717451, -0.8520998092		457, 44.2544501001, -0.8884210152	
418, 45.1858555439, -0.8510302477		458, 44.245847427, -0.8898963103	
419, 45.1343547804, -0.8538303806		459, 44.2567757292, -0.8897220785	
420, 45.1431292988, -0.8541553189		460, 44.2133172446, -0.8920215933	
421, 45.0870061457, -0.8568404292		461, 44.1589939323, -0.8922042116	
422, 45.1107466731, -0.8568017678		462, 44.1925364611, -0.8913273537	
423, 45.1361448535, -0.8583799709		463, 44.2018403215, -0.8935858302	
424, 45.1399834827, -0.8583248818		464, 44.1384133502, -0.8967574532	
425, 45.079044505, -0.8587354414		465, 44.0551394109, -0.8952019214	
426, 45.0973015181, -0.8618761192		466, 44.1146138491, -0.8951759498	
427, 44.929666726, -0.8607507797		467, 43.9969362764, -0.8973512111	
428, 44.8397492949, -0.8623857339		468, 44.0038857873, -0.8978367969	
429, 44.9057383408, -0.8623799904		469, 43.9731291126, -0.8991793583	
430, 44.8687287541, -0.86431668		470, 43.9444510025, -0.9030110231	
431, 44.9181990788, -0.8633476557		471, 43.9622485051, -0.9030773624	
432, 44.8415709957, -0.8661996377		472, 43.865037282, -0.9029606454	
433, 44.8966515106, -0.8674891884		473, 43.9399084331, -0.9010570989	
434, 44.830593452, -0.8663974106		474, 43.8914276437, -0.9035068156	
435, 44.8233165971, -0.8681914712		475, 43.8736516155, -0.9038244434	
436, 44.8162369527, -0.8691498252		476, 43.8951532153, -0.9023604805	
437, 44.7926434093, -0.8695409433		477, 43.7962668598, -0.9059537198	
438, 44.6890708568, -0.8708441985		478, 43.6617554801, -0.9065502796	
439, 44.6906997734, -0.8718235607		479, 43.7120184328, -0.9064710723	
440, 44.7925412174, -0.8738413417		480, 43.7887569247, -0.9088417944	
441, 44.6786532245, -0.873632341		481, 43.6291666789, -0.9100544032	
442, 44.6551321121, -0.8722806157		482, 43.7142565075, -0.9098377446	
443, 44.6074881287, -0.8758953036		483, 43.6244826612, -0.9119838041	
444, 44.4863340333, -0.8776911615		484, 43.5740591461, -0.9102717568	
445, 44.559017294, -0.8775592684		485, 43.6259925051, -0.9147607693	
446, 44.4972406371, -0.8778815396		486, 43.5295248258, -0.914012872	
447, 44.5290318828, -0.8782062363		487, 43.5205334169, -0.9115837013	
448, 44.4338064702, -0.878539758		488, 43.5685172795, -0.9120782899	
449, 44.484601522, -0.8798868575		489, 43.5401030465, -0.917013703	
		490, 43.4952340666, -0.9160222919	



3.3 E-Field Probe and 450 Balanced Dipole Antenna Calibration

Probe calibration factors and dipole antenna calibration are included in Appendix C.

4.0 Measurement Uncertainty

The uncertainty budget has been determined for the INDEXSAR SARA2 measurement system according to IEEE P1528 documents [3] and is given in the following table. The extended uncertainty (95% confidence level) was assessed to be 20.6 % for SAR measurement, and the extended uncertainty (95% confidence level) was assessed to be 20.2 % for system performance check.

Table 1 Exposure Assessment Uncertainty

Example of measurement uncertainty assessment SAR measurement

(blue entries are site-specific)

a	b			c	d	e		f	g	h	i
Uncertainty Component	Sec.	Tol. (+/-)			Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	$\sqrt{3}$	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	$\sqrt{3}$	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	$\sqrt{3}$	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	$\sqrt{3}$	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	$\sqrt{3}$	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	$\sqrt{3}$	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	$\sqrt{3}$	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	$\sqrt{3}$	1.73	1	1	4.62	4.62
Test Sample Related											
Test Sample Positioning	E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Device Holder Uncertainty	E4.1		2	2.00	N	1	1.00	1	1	2.00	2.00
Output Power Variation	6.6.2		5	5.00	R	$\sqrt{3}$	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (shape and thickness)	E3.1		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.5	10.3
Expanded uncertainty	(95% Confidence Level)				k=2					20.6	20.3

Table 2 System Check (Verification)

Example of measurement uncertainty assessment for system performance check

(blue entries are site-specific)

a	b			c	d	e		f	g	h	i
Uncertainty Component	Sec.	Tol. (+/-)			Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	√3	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	√3	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	√3	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	√3	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	√3	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	√3	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	√3	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	√3	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	√3	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	√3	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	√3	1.73	1	1	4.62	4.62
Dipole											
Dipole axis to liquid distance	8, E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Input power and SAR drift measurement	8, 6.6.2		5	5.00	R	√3	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (thickness)	E3.1		4	4.00	R	√3	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.3	10.1
Expanded uncertainty	(95% Confidence Level)				k=2					20.2	19.9

5.0 Measurement Traceability

All measurements described in this report are traceable to Chinese National Laboratory Accreditation (CNLA) standards or appropriate national standards.

6.0 Warning Label Information - USA

See user manual.

7.0 References

- [1] ANSI, *ANSI/IEEE C95.1-1999: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3kHz to 300 GHz*, The Institute of electrical and Electronics Engineers, Inc., New York, NY 10017, 1999

- [2] Federal Communications Commission, "Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields", Supplement C to OET Bulletin 65, Washington, D.C. 20554, 1997

- [3] IEEE Standards Coordinating Committee 34, "IEEE Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques", IEEE Std 1528TM-2003

8.0 Document History

Revision/ Job Number	Writer Initials	Date	Change
N/A	S.L.	Nov. 25, 2004	Original document

APPENDIX A - SAR Evaluation Data

Power drift is the measurement of power drift of the device over one complete SAR scan.

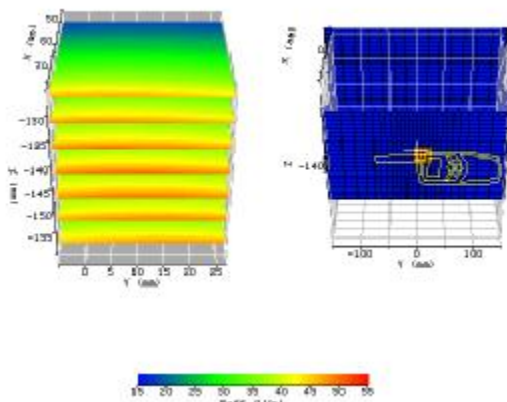
To assess the drift of the power of the device under test, a SAR measurement was made in the middle of the zoom scan volume at the start of the scan and a measurement at this point was then also made after the measurement scan. The difference between the two measurements should be less than 5%.

Plot #1(1/2)

Date:	2004/11/24	Position:	Front to phantom 25mm
Filename:	CH4(Head)041015.txt	Phantom:	HeadBox2-test.csv
Device Tested:	T8220	Head Rotation:	0
Antenna:	Integral (Helix) Antenna	Test Frequency:	CH4_462.6375 MHz
Shape File:	T8220Front.csv	Power Level:	31.2 dBm

Probe:	0149			
Cal File:	SN0149_450_CW_HEAD			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.344	.344	.344
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	3			

Liquid:	15.5cm
Type:	450 MHz head
Conductivity:	0.881
Relative Permittivity:	44.451
Liquid Temp (deg C):	22.6
Ambient Temp (deg C):	23
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor=1	

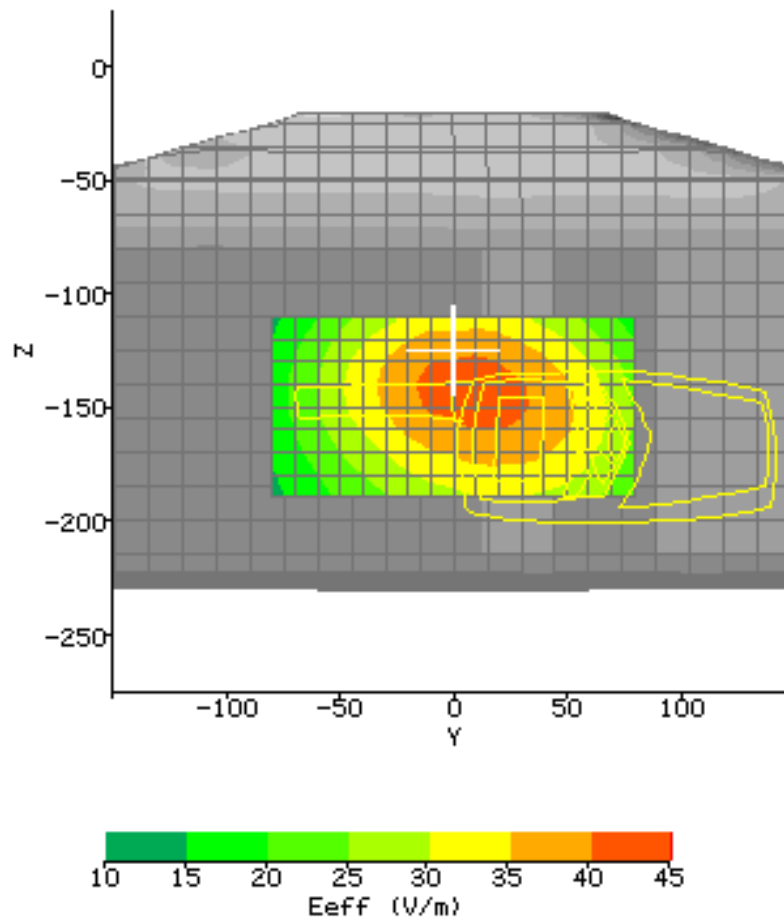
		ZOOM SCAN RESULTS:	
Spot SAR		Start Scan	End Scan
(W/kg):		0.844	0.835
Change during			
Scan (%)	-3.23		
Max E-field			
(V/m):	47.22		
Max SAR (W/kg)		1g	10g
		1.784	1.385
Location of Max		X	Y
(mm):		78.0	-4.9
			Z
			-145.1

Plot #1(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-80.0	80.0	16.0
Z	-190.0	-110.0	8.0



Plot #2(1/2)

Date:	2004/11/24	Position:	Front to phantom 25mm
Filename:	CH11(Head)041015.txt	Phantom:	HeadBox2-test.csv
Device Tested:	T8220	Head Rotation:	0
Antenna:	Integral (Helix) Antenna	Test Frequency:	467.6375 MHz
Shape File:	T8220Front.csv	Power Level:	26.4 dBm

Probe:	0149			
Cal File:	SN0149_450_CW_HEAD			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.344	.344	.344
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	3			

Liquid:	15.5cm
Type:	450 MHz head
Conductivity:	0.881
Relative Permittivity:	44.451
Liquid Temp (deg C):	22.6
Ambient Temp (deg C):	23
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor=1	

The figure displays two 3D surface plots of a rectangular volume. The left plot shows the electric field magnitude (E-field) in V/m, with a color scale ranging from 10.5 (blue) to 27.5 (red). The right plot shows the Specific Absorption Rate (SAR) in W/kg, with a color scale ranging from 0.399 (blue) to 0.378 (red). Both plots are oriented with the X-axis (mm) from -100 to 100, the Y-axis (mm) from 0 to 25, and the Z-axis (mm) from -160 to 80. A color bar at the bottom indicates the E-field magnitude scale.

ZOOM SCAN RESULTS:

Spot SAR

(W/kg):

Change during

Scan (%)

Max E-field

(V/m):

Max SAR (W/kg)

Location of Max

(mm):

Start Scan

0.399

End Scan

0.378

-2.38

34.50

1g

0.744

10g

0652

X

Y

Z

78.0

-4.8

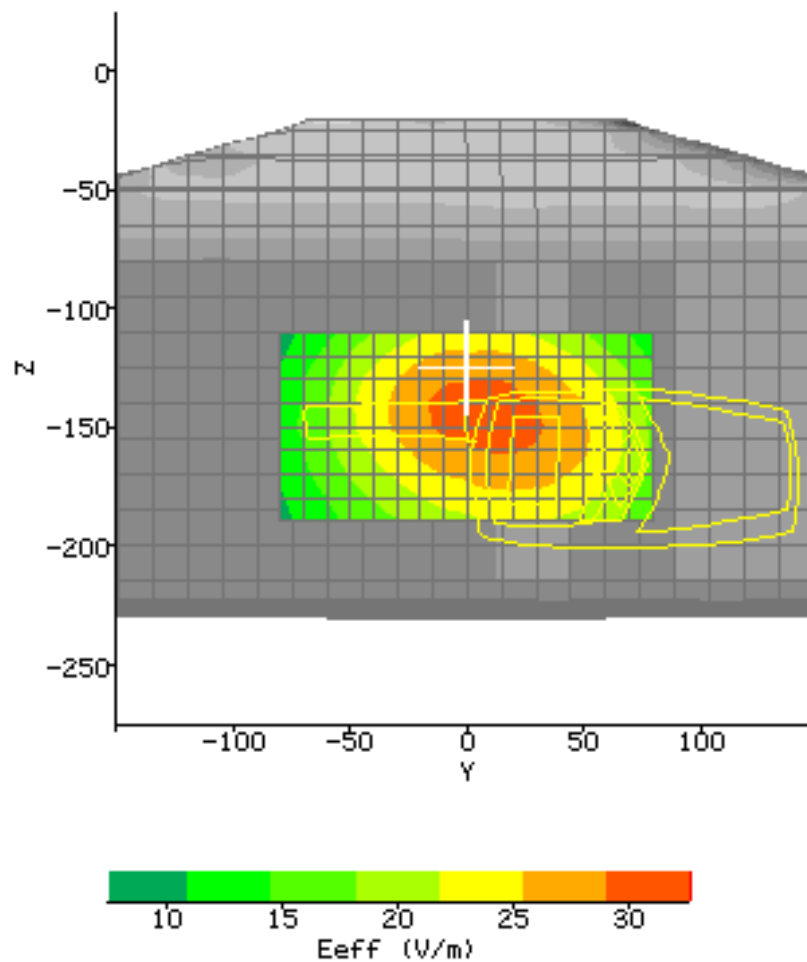
-146.9

Plot #2(2/2)

AREA SCAN:

Scan Extent:

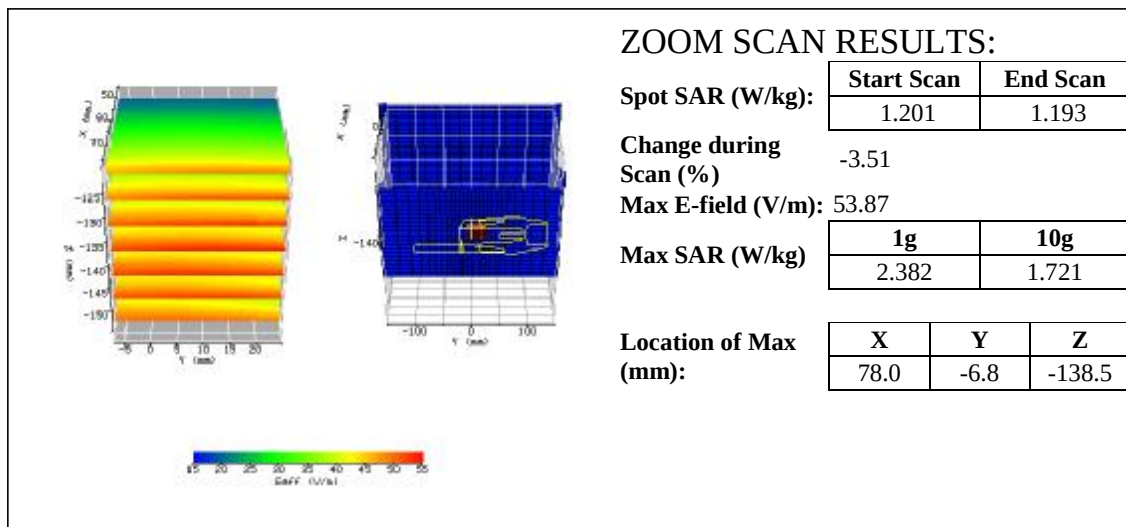
	Min	Max	Steps
Y	-80.0	80.0	16.0
Z	-190.0	-110.0	8.0



Plot #3(1/2)

Date:	2004/11/24	Position:	Rear to phantom with Belt Clip
Filename:	T8220-CH4_rear.txt	Phantom:	HeadBox2-test.csv
Device Tested:	T8220	Head Rotation:	0
Antenna:	Integral (Helix) Antenna	Test Frequency:	CH4_462.6375 MHz
Shape File:	T8220Rear.csv	Power Level:	31.2 dBm

Probe:	0149	Liquid:	15.5cm
Cal File:	SN0149_450_CW_BODY	Type:	450 MHz body
Cal Factors:		Conductivity:	0.951
		Relative Permittivity:	57.497
		Liquid Temp (deg C):	22.2
		Ambient Temp (deg C):	23
Amp Gain:	2	Ambient RH (%):	55
Averaging:	1	Density (kg/m3):	1000
Batteries	3	Software Version:	2.3VPM
Replaced:		Crest Factor=1	

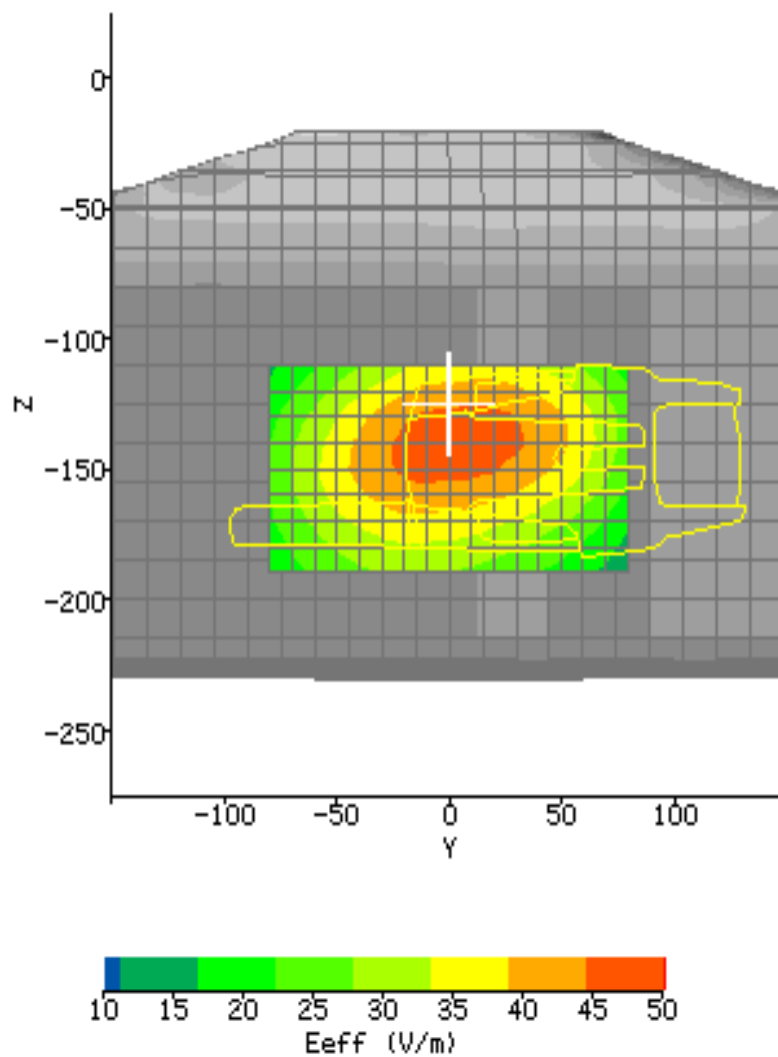


Plot #3(2/2)

AREA SCAN:

Scan Extent:

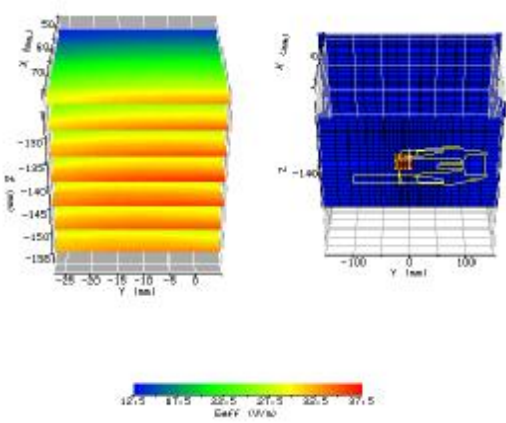
	Min	Max	Steps
Y	-80.0	80.0	16.0
Z	-190.0	-110.0	8.0



Plot #4(1/2)

Date:	2004/11/24	Position:	Rear to phantom with Belt Clip
Filename:	T8220-CH11_rear.txt	Phantom:	HeadBox2-test.csv
Device Tested:	T8220	Head Rotation:	0
Antenna:	Integral (Helix) Antenna	Test Frequency:	CH11_467.6375 MHz
Shape File:	T8220Rear.csv	Power Level:	26.4 dBm

Probe:	0149	Liquid:	15.5cm
Cal File:	SN0149_450_CW_BODY	Type:	450 MHz body
Cal Factors:		Conductivity:	0.951
		Relative Permittivity:	57.497
		Liquid Temp (deg C):	22.2
		Ambient Temp (deg C):	23
Amp Gain:	2	Ambient RH (%):	55
Averaging:	1	Density (kg/m3):	1000
Batteries	3	Software Version:	2.3VPM
Replaced:		Crest Factor=1	

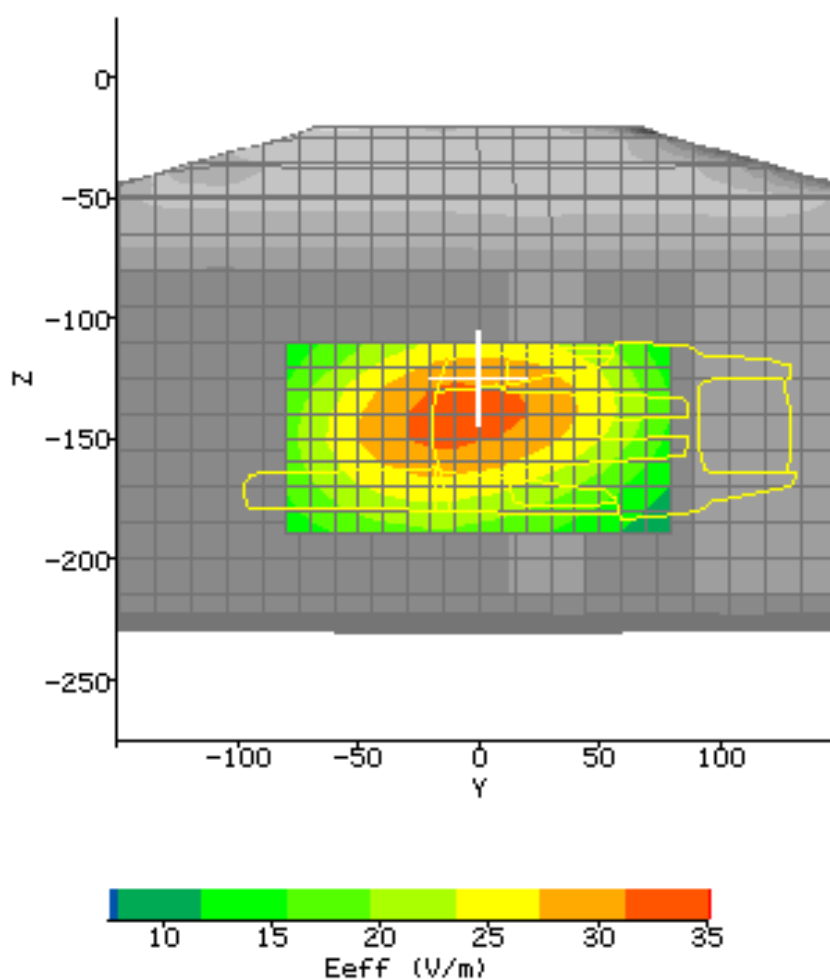
		ZOOM SCAN RESULTS:	
Spot SAR (W/kg):	Start Scan		End Scan
	0.555		0.532
Change during Scan (%)	-2.47		
Max E-field (V/m):	35.02		
Max SAR (W/kg)	1g		10g
	1.086		0.777
Location of Max (mm):	X	Y	Z
	78.2	-26.9	-141.0

Plot #4(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-80.0	80.0	16.0
Z	-190.0	-110.0	8.0



APPENDIX B - Photographs

(External)



(External)



(Battery)



(Battery)



(Belt-clip)



(Belt-clip)



(earphone)



APPENDIX C - E-Field Probe and 450MHz Balanced Dipole Antenna Calibration Data



**IMMERSIBLE SAR PROBE
CALIBRATION REPORT**

Part Number: IXP – 050

S/N 0149

May 2004



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INTRODUCTION

This Report presents measured calibration data for a particular Indexsar SAR probe (S/N 0149) and describes the procedures used for characterisation and calibration.

Indexsar probes are characterised using procedures that, where applicable, follow the recommendations of CENELEC [1] and IEEE [2] standards. The procedures incorporate techniques for probe linearisation, isotropy assessment and determination of liquid factors (conversion factors). Calibrations are determined by comparing probe readings with analytical computations in canonical test geometries (waveguides) using normalised power inputs.

Each step of the calibration procedure and the equipment used is described in the sections below.

CALIBRATION PROCEDURE

1. Equipment Used

For the first part of the characterisation procedure, the probe is placed in an isotropy measurement jig as pictured in Figure 1. In this position the probe can be rotated about its axis by a non-metallic belt driven by a stepper motor.

The probe is attached via its amplifier and an optical cable to a PC. A schematic representation of the test geometry is illustrated in Figure 2.

A balanced dipole (900 MHz) is inserted horizontally into the bracket attached to a second belt (Figure 1). The dipole can also be rotated about its axis. A cable connects the dipole to a signal generator, via a directional coupler and power meter. The signal generator feeds an RF amplifier at constant power, the output of which is monitored using the power meter. The probe is positioned so that its sensors line up with the rotation center of the source dipole. By recording output voltage measurements of each channel as both the probe and the dipole are rotated, data are obtained from which the spherical isotropy of the probe can be optimised and its magnitude determined.

The calibration process requires E-field measurements to be taken in air, in 900 MHz simulated brain liquid and at other frequencies/liquids as appropriate.

2. Linearising probe output

The probe channel output signals are linearised in the manner set out in Refs [1] and [2]. The following equation is utilized for each channel:

$$U_{lin} = U_{o/p} + U_{o/p}^2 / DCP \quad (1)$$

where U_{lin} is the linearised signal, $U_{o/p}$ is the raw output signal in voltage units and DCP is the diode compression potential in similar voltage units.

DCP is determined from fitting equation (1) to measurements of U_{lin} versus source feed power over the full dynamic range of the probe. The DCP is a characteristic of the schottky diodes used as the sensors. For the IXP-050 probes with CW signals the DCP values are typically 0.10V (or 20 in the voltage units used by Indexsar software, which are $V*200$).

3. Selecting channel sensitivity factors to optimise isotropic response

The basic measurements obtained using the calibration jig (Fig 1) represent the output from each diode sensor as a function of the presentation angle of the source (probe and dipole rotation angles). The directionality of the orthogonally-arranged sensors can be checked by analysing the data using dedicated Indexsar software, which displays the data in 3D format as in Figure 3. The left-hand side of this diagram shows the individual channel outputs after linearisation (see above). The program uses these data to balance the channel outputs and then applies an optimisation process, which makes fine adjustments to the channel factors for optimum isotropic response.

The next stage of the process is to calibrate the Indexsar probe to a W&G EMR300 E-field meter in air. The principal reasons for this are to obtain conversion factors applicable should the probe be used in air and to provide an overall measure of the probe sensitivity.

A multiplier is applied to factors to bring the magnitudes of the average E-field measurements as close as possible to those of the W&G probe.

The following equation is used (where linearised output voltages are in units of $V*200$):

$$E_{air}^2 (V/m) = U_{linx} * Air Factor_x + U_{liny} * Air Factor_y + U_{linz} * Air Factor_z \quad (2)$$

It should be noted that the air factors are not separately used for normal SAR testing. The IXP-050 probes are optimised for use in tissue-simulating liquids and do not behave isotropically in air.

4. 900 MHz Liquid Calibration

Conversion factors for use when the probes are immersed in tissue-simulant liquids at 900 MHz are determined either using a waveguide or by comparison to a reference probe that has been calibrated by NPL. Waveguide procedures are described later. The summary sheet indicates the method used for the probe S/N 0149.

The conversion factor, referred to as the 'liquid factor' is also applied to the measurements of each channel. The following equation is used (where output voltages are in units of $V*200$):

$$E_{liq}^2 (V/m) = U_{linx} * Air Factor_x * Liq Factor_x + U_{liny} * Air Factor_y * Liq Factor_y + U_{linz} * Air Factor_z * Liq Factor_z \quad (3)$$

A 3D representation of the spherical isotropy for probe S/N 0149 using these factors is shown in Figure 3.

The rotational isotropy can also be determined from the calibration jig measurements and is reported as the 900MHz isotropy in the summary table. Note that waveguide measurements can also be used to determine rotational isotropy (Fig. 5).

The design of the cells used for determining probe conversion factors are waveguide cells is shown in Figure 4. The cells consist of a coax to waveguide transition and an open-ended section of waveguide containing a dielectric separator. Each waveguide cell stands in the upright position and is filled with liquid within 10 mm of the open end. The separator provides a liquid seal and is designed for a good electrical transition from air filled guide to liquid filled guide. The choice of cell depends on the portion of the frequency band to be examined and the choice of liquid used. The depth of liquid ensures there is negligible radiation from the waveguide open top and that the probe calibration is not influenced by reflections from nearby objects. The return loss at the coaxial connector of the filled waveguide cell is measured initially using a network analyser and this information is used subsequently in the calibration procedure. The probe is positioned in the centre of the waveguide and is adjusted vertically or rotated using stepper motor arrangements. The signal generator is connected to the waveguide cell and the power is monitored with a coupler and a power meter. A fuller description of the waveguide method is given below.

The liquid dielectric parameters used for the probe calibrations are listed in the Tables below. The final calibration factors for the probe are listed in the summary chart.

WAVEGUIDE MEASUREMENT PROCEDURE

The calibration method is based on setting up a calculable specific absorption rate (SAR) in a vertically-mounted WG8 (R22) waveguide section [1]. The waveguide has an air-filled, launcher section and a liquid-filled section separated by a matching window that is designed to minimise reflections at the liquid interface. A TE_{01} mode is launched into the waveguide by means of a N-type-to-waveguide adapter. The power delivered to the liquid section is calculated from the forward power and reflection coefficient measured at the input to the waveguide. At the centre of the cross-section of the waveguide, the local spot SAR in the liquid as a function of distance from the window is given by functions set out in IEEE1528 as below:

Because of the low cutoff frequency, the field inside the liquid nearly propagates as a TEM wave. The depth of the medium (greater than three penetration depths) ensures that reflections at the upper surface of the liquid are negligible. The power absorbed in the liquid is determined by measuring the waveguide forward and reflected power. Equation (4) shows the relationship between the SAR at the cross-sectional center of the lossy waveguide and the longitudinal distance (z) from the dielectric separator

$$SAR(z) = \frac{4(P_f - P_b)}{r abd} e^{-2z/d} \quad (4)$$

where the density ρ is conventionally assumed to be 1000 kg/m^3 , ab is the cross-sectional area of the waveguide, P_f and P_b are the forward and reflected power inside the lossless section of the waveguide, respectively. The penetration depth d , which is the reciprocal of the waveguide-mode attenuation coefficient, is determined from a scan along the z -axis and compared with the theoretical value determined from Equation (5) using the measured dielectric properties of the lossy liquid.

$$d = \left[\text{Re} \left\{ \sqrt{(p/a)^2 + j\omega\mu_0 (s + j\omega\epsilon_0\epsilon_r)} \right\} \right]^{-1}. \quad (5)$$

Table A.1 of [1] can be used for designing calibration waveguides with a return loss greater than 30 dB at the most important frequencies used for personal wireless communications. Values for the penetration depth for these specific fixtures and tissue-simulating mixtures are also listed in Table A.1.

According to [1], this calibration technique provides excellent accuracy, with standard uncertainty of less than 3.6% depending on the frequency and medium. The calibration itself is reduced to power measurements traceable to a standard calibration procedure. The practical limitation to the frequency band of 800 to 2500 MHz because of the waveguide size is not severe in the context of compliance testing.

CALIBRATION FACTORS MEASURED FOR PROBE S/N 0149

The probe was calibrated at 900, 1800, 1900 and 2450MHz MHz in liquid samples representing both brain liquid and body fluid at these frequencies. The calibration was for CW signals only, and the axis of the probe was parallel to the direction of propagation of the incident field i.e. end-on to the incident radiation. The axial isotropy of the probe was measured by rotating the probe about its axis in 10 degree steps through 360 degrees in this orientation.

The reference point for the calibration is in the centre of the probe's cross-section at a distance of 2.7 m from the probe tip in the direction of the probe amplifier. A value of 2.7 mm should be used for the tip to sensor offset distance in the software.

It is important that the diode compression point and air factors used in the software are the same as those quoted in the results tables, as these are used to convert the diode output voltages to a SAR value.

DIELECTRIC PROPERTIES OF LIQUIDS

The dielectric properties of the brain and body tissue-simulant liquids employed for calibration are listed in the tables below. The measurements were performed prior to each waveguide test using an Indexsar DiLine measurement kit, which uses the TEM method as recommended in [2].

AMBIENT CONDITIONS

Measurements were made in the open laboratory at $22 \pm 2.0^\circ\text{C}$. The temperature of the liquids in the waveguide used was measured using a mercury thermometer.

RESPONSE TO MODULATED SIGNALS

To measure the response of the probe and amplifier to modulated signals, the probe is held vertically in a liquid-filled waveguide.

An RF amplifier is allowed to warm up and stabilise before use. A spectrum analyser is used to demonstrate that the peak power of the RF amplifier for the CW signals and the pulsed signals are within 0.1dB of each other when the signal generator is switched from CW to modulated output. Subsequently, the power levels recorded are read from a power meter when a CW signal is being transmitted.

The test sequence involves manually stepping the power up in regular (e.g. 2 dB) steps from the lowest power that gives a measurable reading on the SAR probe up to the maximum that the amplifiers can deliver.

At each power level, the individual channel outputs from the SAR probe are recorded at CW and then recorded again with the modulation setting. The results are entered into a spreadsheet. Using the spreadsheets, the modulated power is calculated by applying a factor to the measured CW power (e.g. for GSM, this factor is 9.03dB). This process is repeated 3 times with the response maximised for each channel sensor in turn.

The probe channel output signals are linearised in the manner set out in Section 1 above using equation (1) with the DCPs determined from the linearisation procedure. Calibration factors for the probe are used to determine the E-field values corresponding to the probe readings using equation (3). SAR is determined from the equation

$$\text{SAR (W/kg)} = E_{\text{liq}}^2 \text{ (V/m)} * \sigma \text{ (S/m)} / 1000 \quad (6)$$

Where σ is the conductivity of the simulant liquid employed.

Using the spreadsheet data, the DCP value for linearising each of the individual channels (X, Y and Z) is assessed separately. The corresponding DCP values are listed in the summary page of the calibration factors for each probe.

Figure 7 shows the linearised probe response to GSM signals, Figure 8 the response to GPRS signals (GSM with 2 timeslots) and Figure 9 the response to CDMA IS-95A and W-CDMA signals.

Additional tests have shown that the modulation response is similar at 1800MHz and is not affected by the orientation between the source and the probe.

VPM (Virtual Probe Miniaturisation)

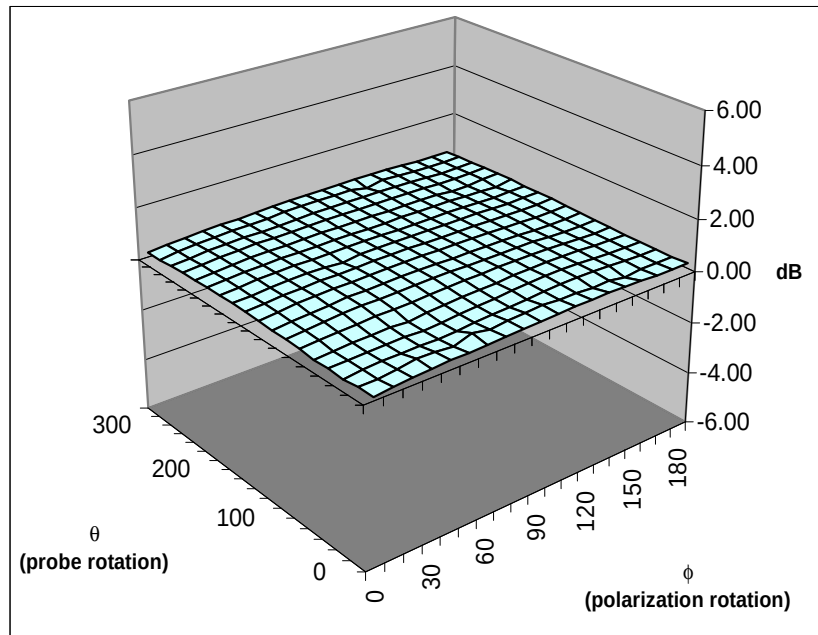
SAR probes with 3 diode-sensors in an orthogonal arrangement are designed to display an isotropic response when exposed to a uniform field. However, the probes are ordinarily used for measurements in non-uniform fields and isotropy is not assured when the field gradients are significant compared to the dimensions of the tip containing the three orthogonally-arranged dipole sensors.

It becomes increasingly important to assess the effects of field gradients on SAR probe readings when higher frequencies are being used. For Indexsar IXP-050 probes, which are of 5mm tip diameter, field gradient effects are minor at GSM frequencies, but are major above 5GHz. Smaller probes are less affected by field gradients and so probes, which are significantly less than 5mm diameter, would be better for applications above 5GHz.

The IndexSAR report IXS0223 describes theoretical and experimental studies to evaluate the issues associated with the use of probes at arbitrary angles to surfaces and field directions. Based upon these studies, the procedures and uncertainty analyses referred to in P1528 are addressed for the full range of probe presentation angles.

In addition, generalized procedures for correcting for the finite size of immersible SAR probes are developed. Use of these procedures enables application of schemes for virtual probe miniaturization (VPM) – allowing probes of a specific size to be used where physically-smaller probes would otherwise be required.

Given the typical dimensions of 3-channel SAR probes presently available, use of the VPM technique extends the satisfactory measurement range to higher frequencies.



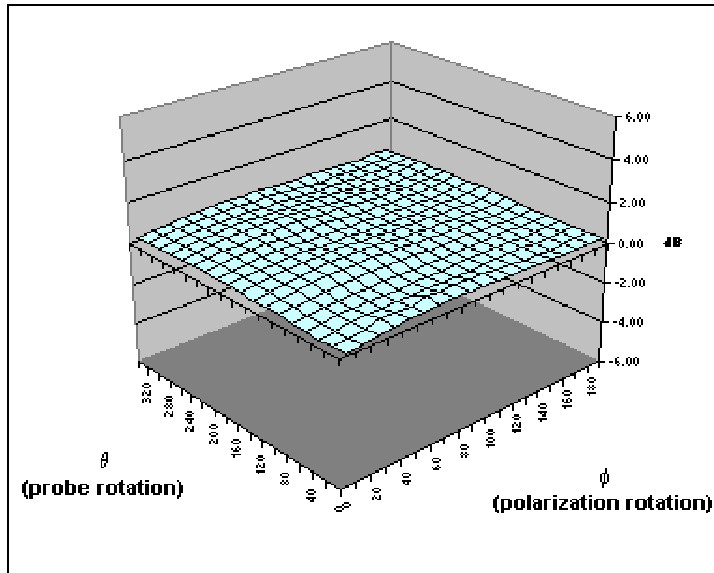
Surface Isotropy diagram of IXP-050 Probe S/N 0149 at 900MHz after VPM

Probe tip radius	1.25
X Ch. Angle to red dot	7

Frequency	Head		Body	
	Bdy. Corr. – f(0)	Bdy. Corr. – d(mm)	Bdy. Corr. – f(0)	Bdy. Corr. – d(mm)
900	0.2	1.0	0.31	2.0
1800	0.2	2.0	0.27	1.6
1900	0.19	1.7	0.3	1.4
2450	0.24	2.0	0.72	2.0

SUMMARY OF CALIBRATION FACTORS FOR PROBE IXP-050 S/N 0149

Spherical isotropy measured at 900 MHz 0.28 (+/-) dB



	X	Y	Z	
Air factors	365	444	414	(V*200)
DCPs	20	20	20	(V*200)
GSM	13.4	9.6	7.9	(V*200)
CDMA	20	20	20	(V*200)

f (MHz)	Axial isotropy (+/- dB)		SAR conversion factors (liq/air)		Notes
	BRAIN	BODY	BRAIN	BODY	
450	0.08	0.07	0.344	0.360	1,2,3
835	0.08	0.07	0.344	0.360	1,2,3
900	0.08	0.07	0.344	0.360	1,2,3
1800	0.10	0.11	0.438	0.477	1,2,3
1900	0.11	0.12	0.441	0.504	1,2,3
2450	0.11	0.11	0.504	0.561	1,2,3

Notes				
1)	Calibrations done at 22C +/- 2C			
2)	Waveguide calibration			
3)	Checked using box-phantom validation test			

(the graph shows a simple, spreadsheet representation of surface shown in 3D in Figure 3 below)

PROBE SPECIFICATIONS

Indexsar probe 0149, along with its calibration, is compared with CENELEC and IEEE standards recommendations (Refs [1] and [2]) in the Tables below. A listing of relevant specifications is contained in the tables below:

Dimensions	S/N 0149	CENELEC [1]	IEEE [2]
Overall length (mm)	350		
Tip length (mm)	10		
Body diameter (mm)	12		
Tip diameter (mm)	5.2	8	8
Distance from probe tip to dipole centers (mm)	2.7		

Dynamic range	S/N 0149	CENELEC [1]	IEEE [2]
Minimum (W/kg)	0.01	<0.02	0.01
Maximum (W/kg)	>35	>100	100
N.B. only measured to 35 W/kg			

Linearity of response	S/N 0149	CENELEC [1]	IEEE [2]
Over range 0.01 – 100 W/kg (+/- dB)	0.125	0.50	0.25

Isotropy (measured at 900MHz)	S/N 0149	CENELEC [1]	IEEE [2]
Axial rotation with probe normal to source (+/- dB) at 900, 1800, 1900 and 2450 MHz	0.12 Max (See table above)	0.5	0.25
Spherical isotropy covering all orientations to source (+/- dB)	0.28	1.0	0.50

Construction	Each probe contains three orthogonal dipole sensors arranged on a triangular prism core, protected against static charges by built-in shielding, and covered at the tip by PEEK cylindrical enclosure material. No adhesives are used in the immersed section. Outer case materials are PEEK and heat-shrink sleeving.
Chemical resistance	Tested to be resistant to glycol and alcohol containing simulant liquids but probes should be removed, cleaned and dried when not in use.

REFERENCES

- [1] CENELEC, EN 50361, July 2001. Basic Standard for the measurement of specific absorption rate related to human exposure to electromagnetic fields from mobile phones.
- [2] IEEE 1528, Recommended practice for determining the spatial-peak specific absorption rate (SAR) in the human body due to wireless communications devices: Experimental techniques.

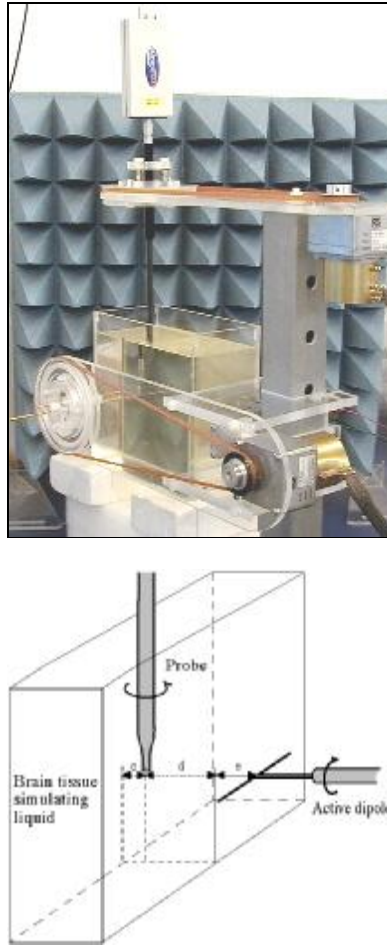


Figure 1. Spherical isotropy jig showing probe, dipole and box filled with simulated brain liquid (see Ref [2], Section A.5.2.1)

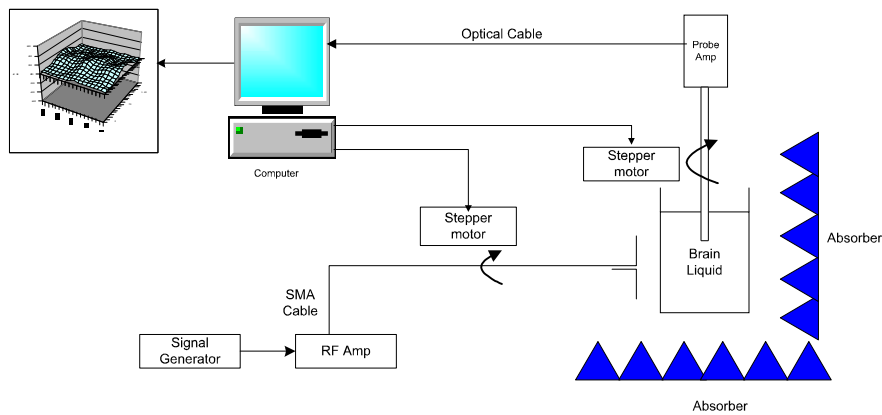


Figure 2. Schematic diagram of the test geometry used for isotropy determination

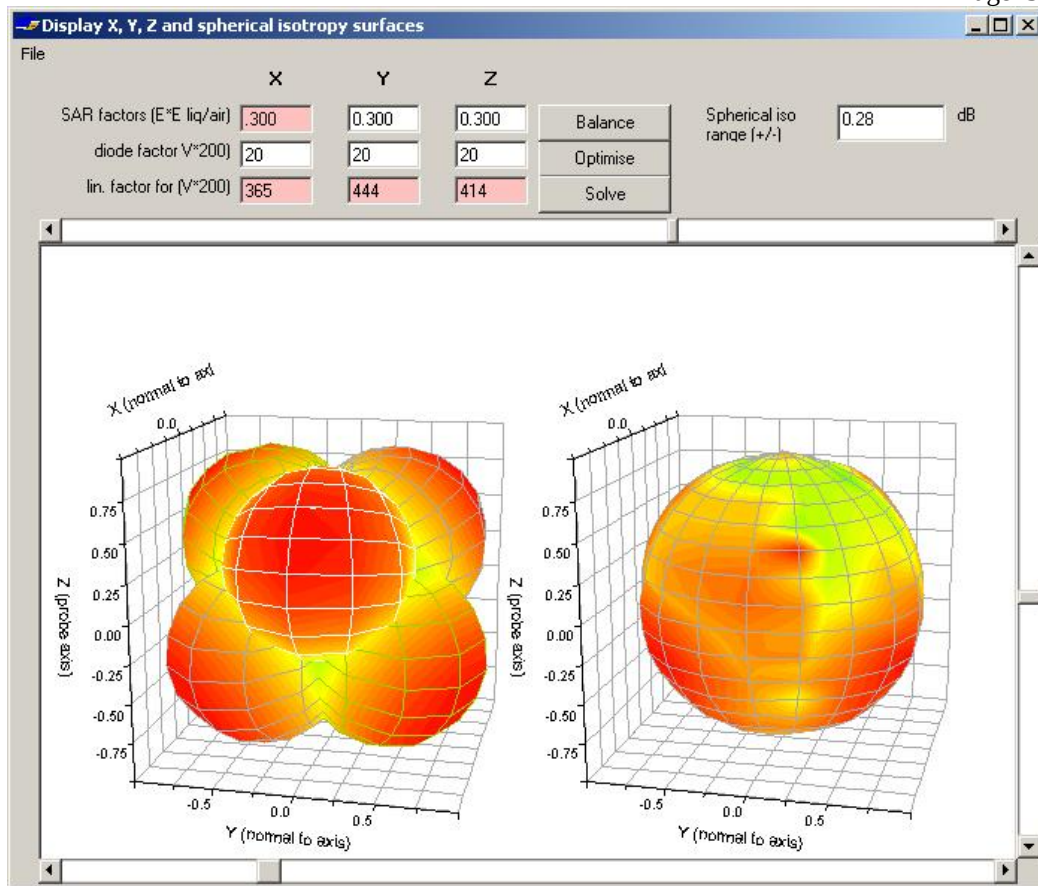


Figure 3. Graphical representation of the probe response to fields applied from each direction. The diagram on the left shows the individual response characteristics of each of the three channels and the diagram on the right shows the resulting probe sensitivity in each direction. The colour range in the figure images the lowest values as blue and the maximum values as red. For the probe S/N 0149, this range is (+/-) 0.28 dB. The probe is more sensitive to fields parallel to the axis and less sensitive to fields normal to the probe axis.

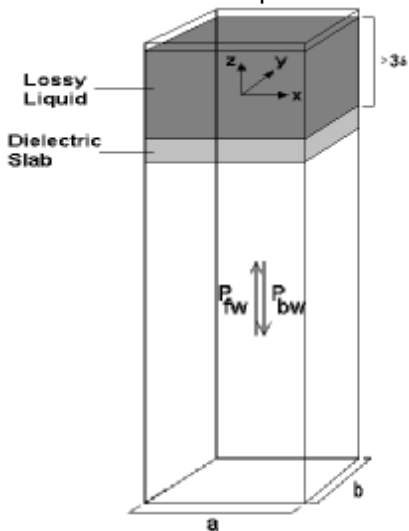


Figure 4. Geometry used for waveguide calibration (after Ref [2]. Section A.3.2.2)

IXP-050 S/N 0149

11-May-04

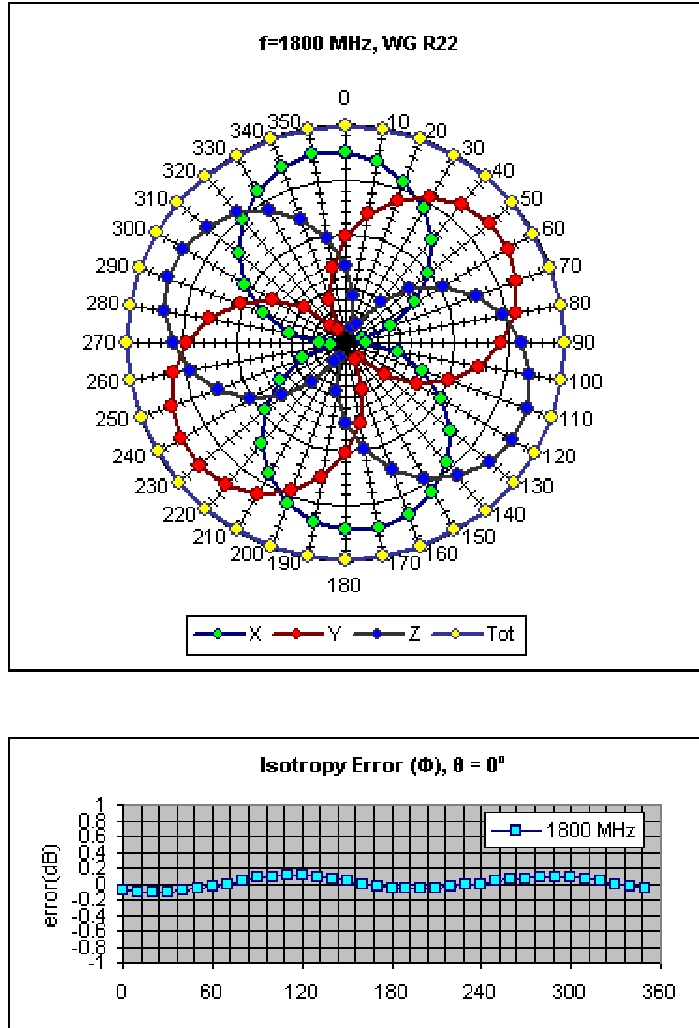


Figure 5. Example of the rotational isotropy of probe S/N 0149 obtained by rotating the probe in a liquid-filled waveguide at 1800 MHz. Similar distributions are obtained at the other test Frequencies (900 and 2450 MHz) both in brain liquids and body fluids (see summary table).

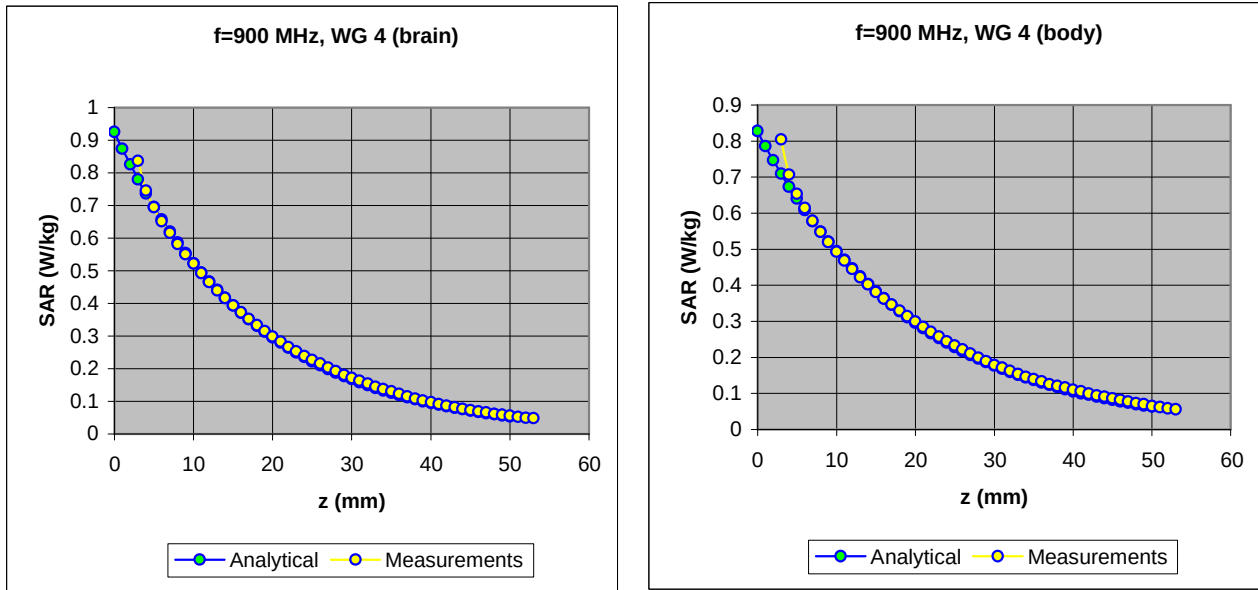
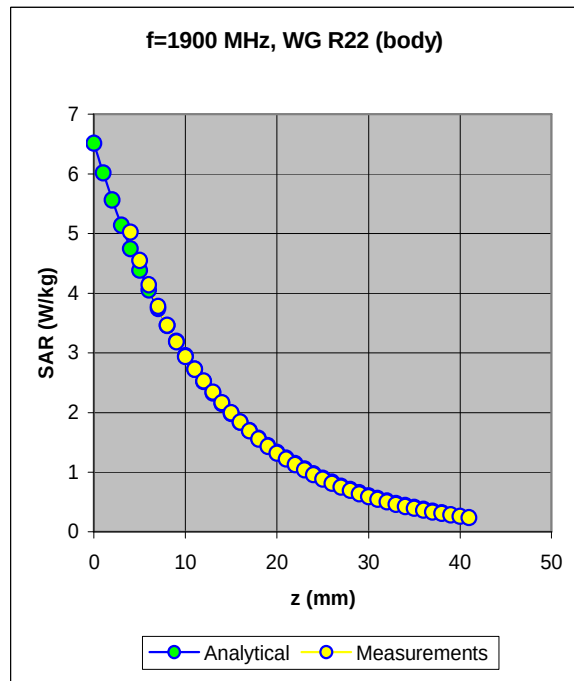
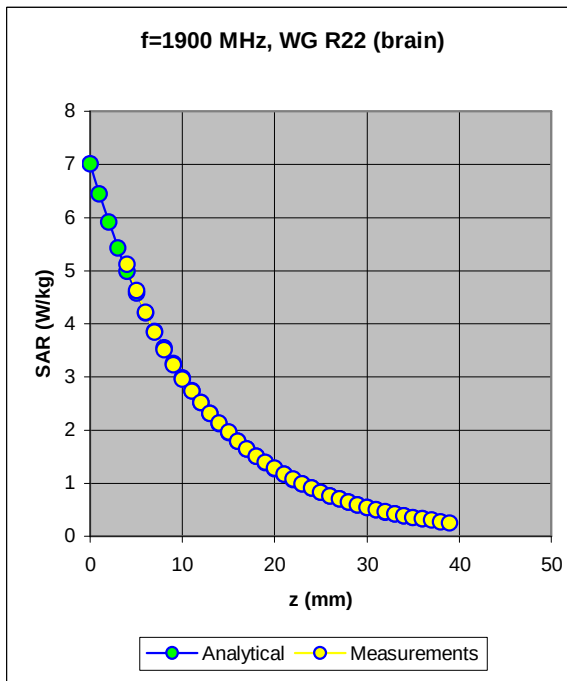
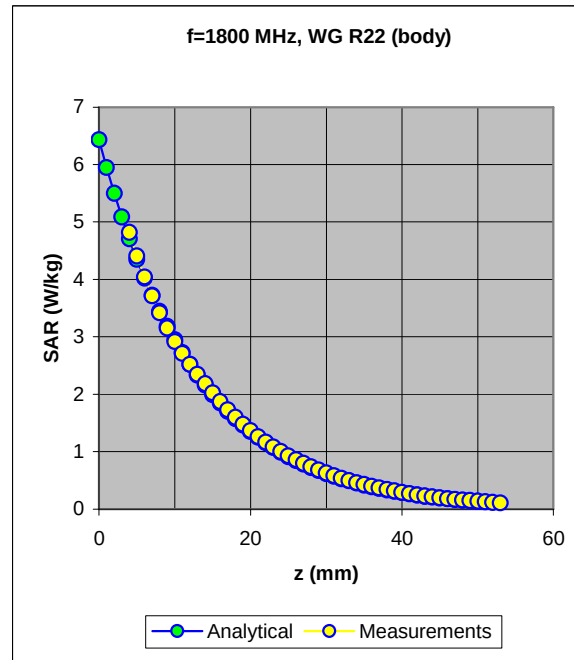
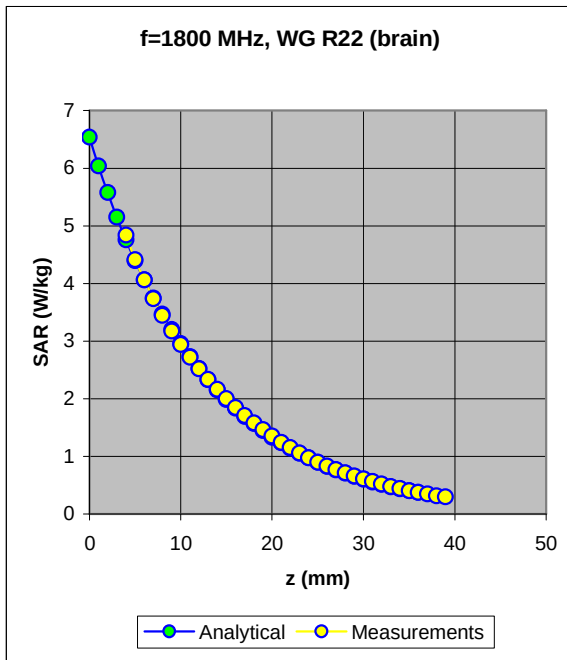


Figure 6. The measured SAR decay function along the centreline of the WG4 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.



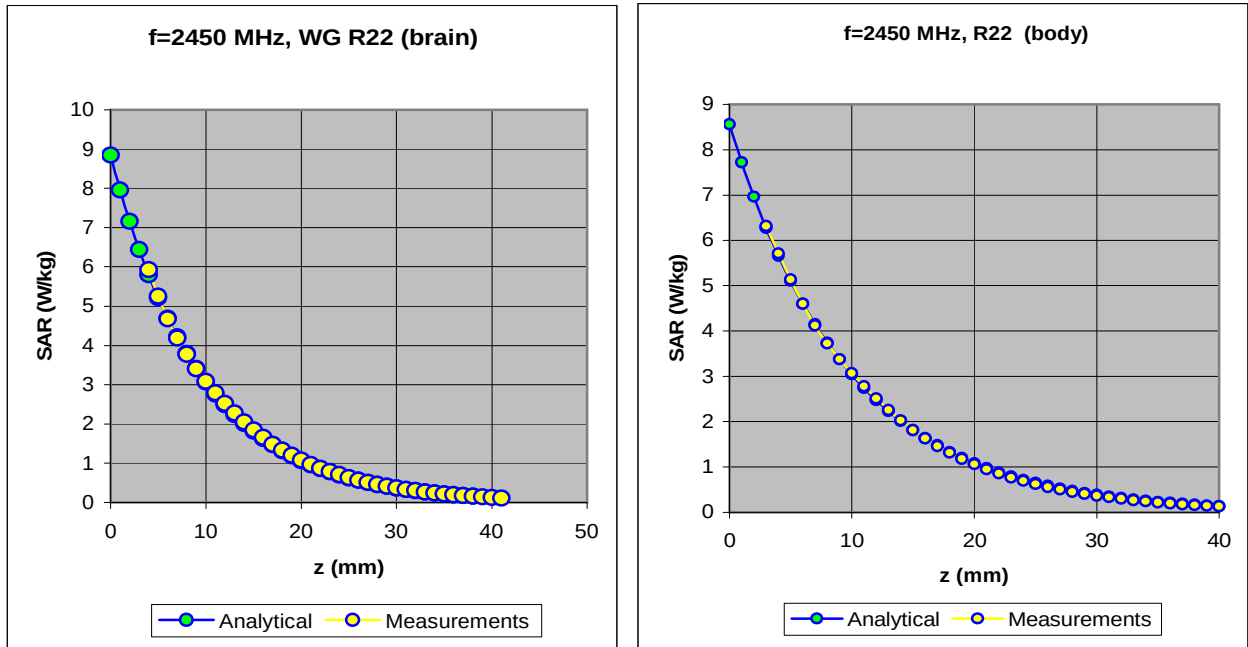


Figure 7. The measured SAR decay function along the centreline of the R22 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.

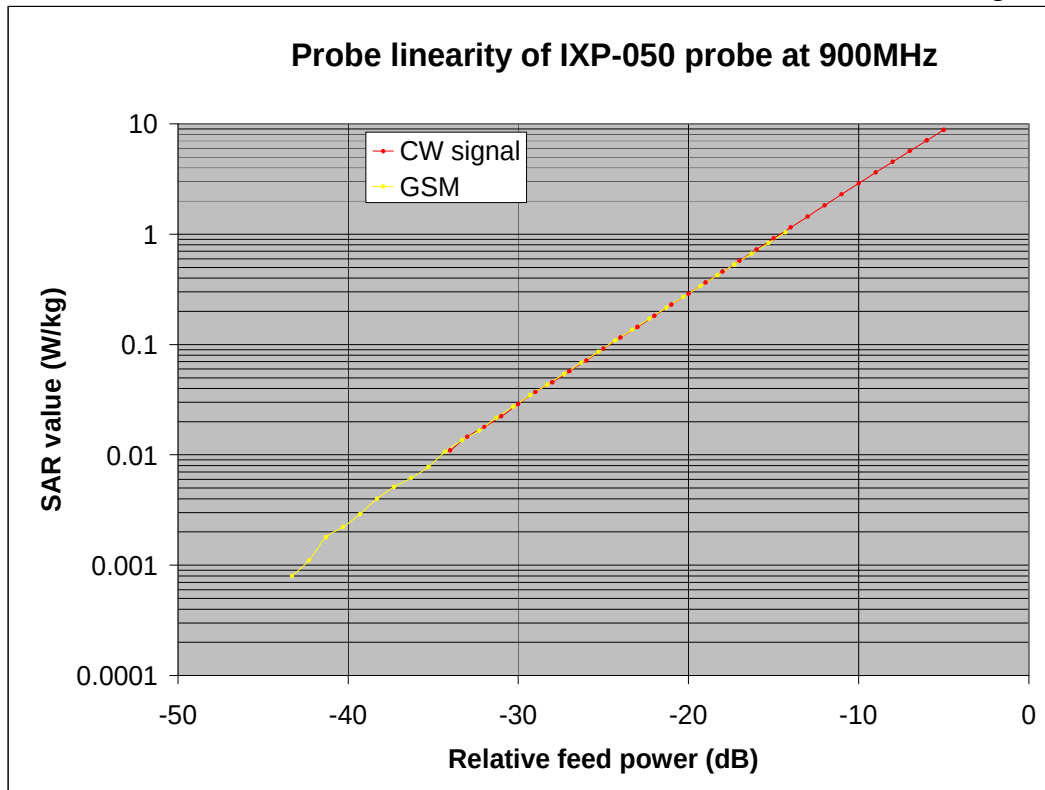


Figure 8. The GSM response of an IXP-050 probe at 900MHz

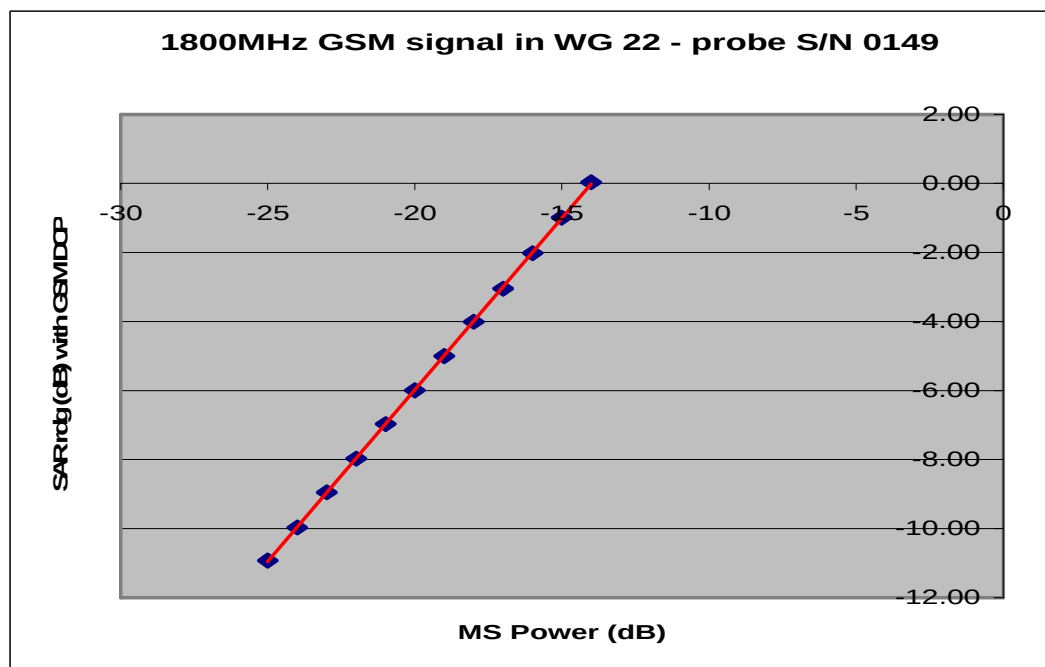


Figure 8a. The actual GSM response of IXP-050 probe S/N 0149 at 1800MHz

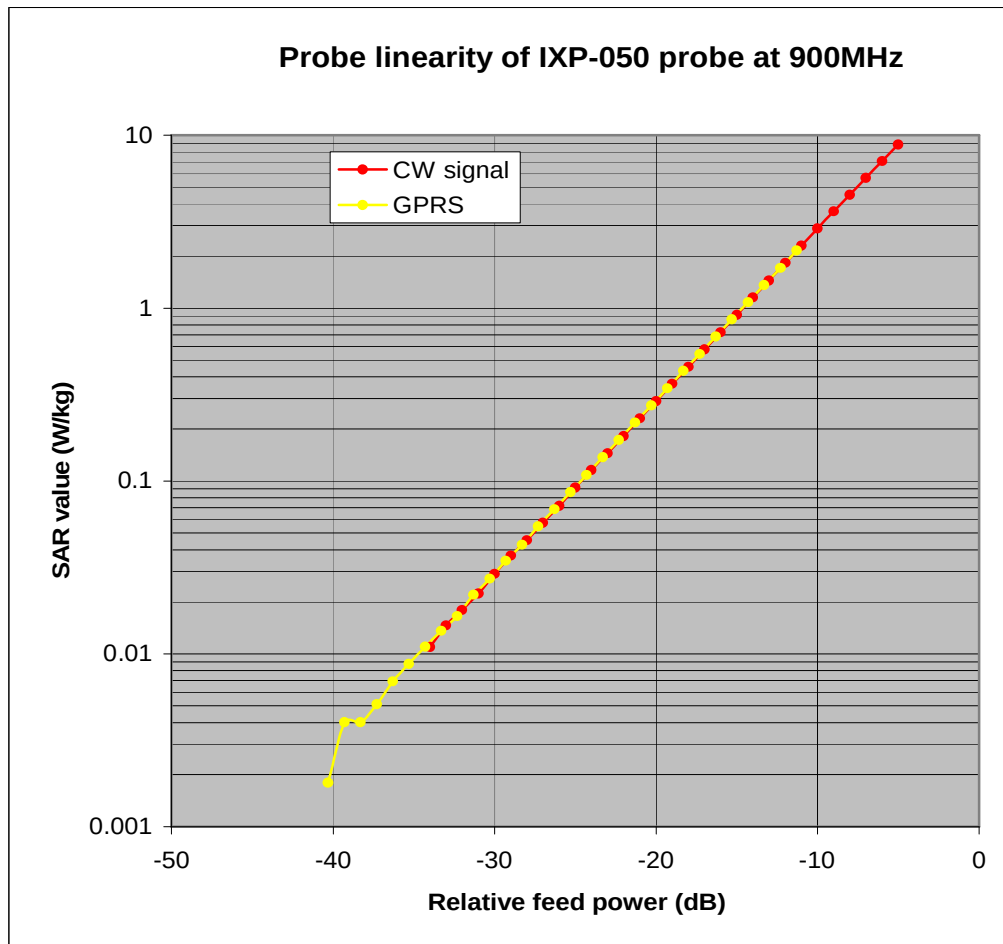


Figure 9. The GPRS response of an IXP-050 probe at 900MHz.

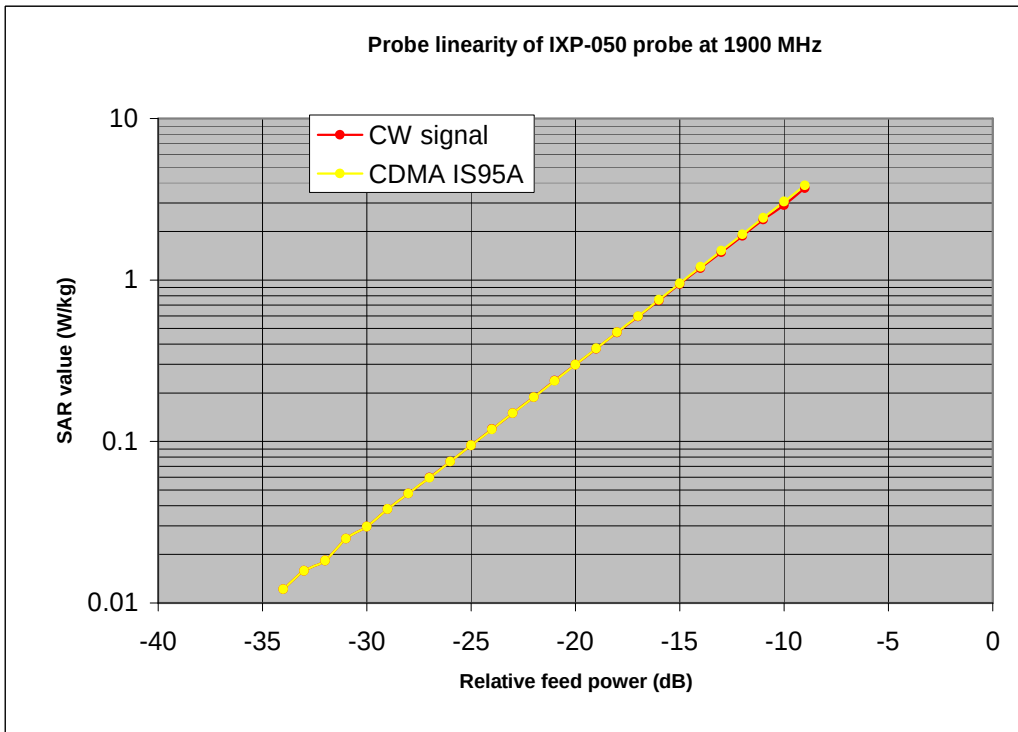
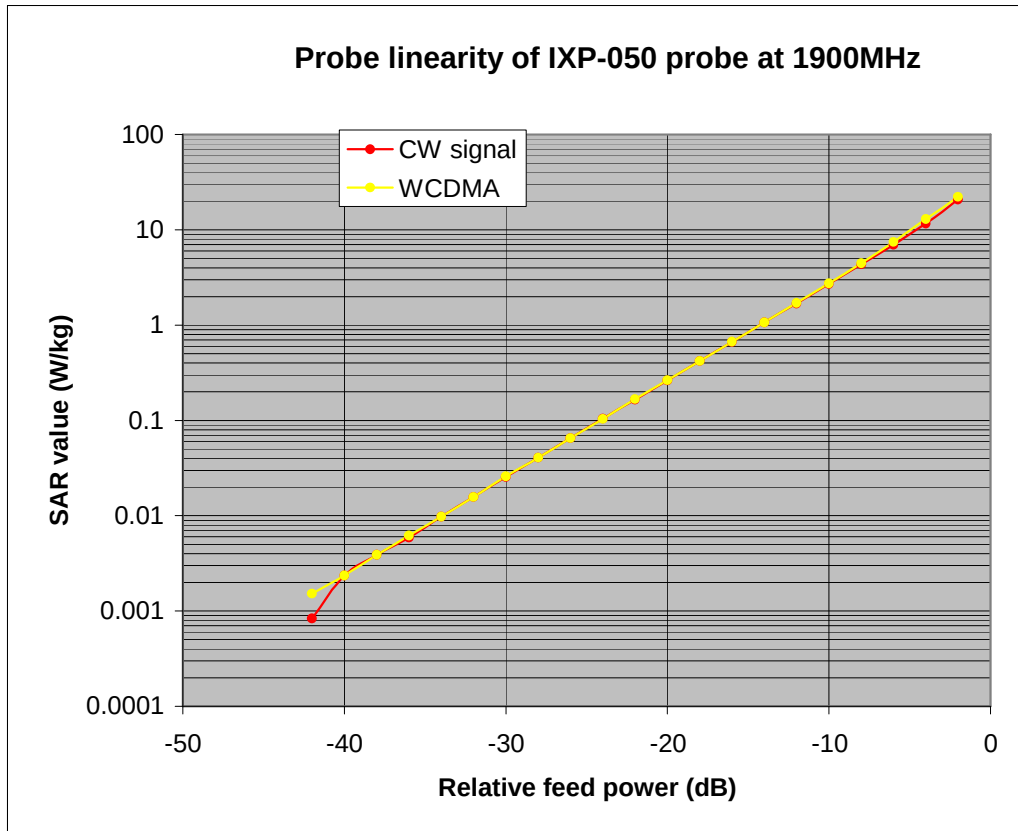


Figure 10. The CDMA response of an IXP-050 probe at 1900MHz.

Table indicating the dielectric parameters of the liquids used for calibrations at each frequency

<i>Liquid used</i>	<i>Relative permittivity (measured)</i>	<i>Conductivity (S/m) (measured)</i>
<i>900 MHz BRAIN</i>	<i>40.92</i>	<i>0.99</i>
<i>900 MHz BODY</i>	<i>57.27</i>	<i>1.045</i>
<i>1800 MHz BRAIN</i>	<i>40.63</i>	<i>1.37</i>
<i>1800 MHz BODY</i>	<i>52.89</i>	<i>1.53</i>
<i>1900 MHz BRAIN</i>	<i>40.33</i>	<i>1.47</i>
<i>1900 MHz BODY</i>	<i>52.84</i>	<i>1.55</i>
<i>2450 MHz BRAIN</i>	<i>40.73</i>	<i>1.82</i>
<i>2450 MHz BODY</i>	<i>54.56</i>	<i>2.04</i>

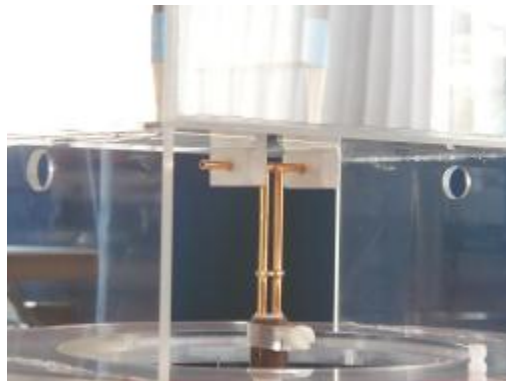


Report No. SN0065_450
October 2003

INDEXSAR
450MHz validation Dipole
Type IXD-045 S/N 0065

Performance measurements

- MI Manning



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Calibration / Conformance statement
Balanced Validation dipole

Type:	IXD-045 450MHz
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Manufacturer:	IndexSAR, UK
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Serial Number:	0065
----------------	------

Place of Calibration:	IndexSAR, UK
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IndexSAR Limited hereby declares that the IXD series dipole named above has been checked for conformity to the specifications given in the draft IEEE 1528 and CENELEC En 50361 standards on the date shown below.

Date of Calibration/Check:	October 2003
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The dipole named above should be periodically re-checked using the procedures set out in the dipole calibration document. It is important that the cautions regarding handling of the dipoles (given in the calibration document) are adhered to.

Next Calibration Date:	October 2005
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The calibration measurements were carried out using the methods described in the calibration document. Where applicable, the standards used in the calibration process are traceable to the UK's National Physical Laboratory.

Calibrated By:	
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Approved By:	
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1. Measurement Conditions

Measurements were performed using a box-shaped phantom made of PMMA with dimensions designed to meet the accuracy criteria for reasonably-sized phantoms that do not have liquid capacities substantially in excess of the volume of liquid required to fill the Indexsar upright SAM phantoms used for SAR testing of handsets against the ear.

An HP 8753B vector network analyser was used for the return loss measurements.

The dipole was placed in a special holder made of low-permittivity, low-loss materials. This holder enables the dipole to be positioned accurately in the centre of the base of the Indexsar box-phantom used for flat-surface testing and validation checks.

The validation dipoles are supplied with special spacers made from a low-permittivity, low-loss foam material. These spacers are fitted to the dipole arms to ensure that, when the dipole is offered up to the phantom surface, the spacing between the dipole and the liquid surface is accurately aligned according to the guidance in the relevant standards documentation. The spacers are rectangular with a central hole equal to the dipole arm diameter and dimensioned so that the longer side can be used to ensure a spacing of 15mm from the liquid in the phantom (for tests at 900MHz and below) and the shorter side can be used for tests at 1800MHz and above to ensure a spacing of 10mm from the liquid in the phantom. The spacers are made on a CNC milling machine with an accuracy of 1/40th mm but they may suffer wear and tear and need to be replaced periodically. The material used is Rohacell, which has a relative permittivity of approx. 1.05 and a negligible loss tangent.

The apparatus supplied by Indexsar for dipole validation tests thus includes:

Balanced dipoles for each frequency required are dimensioned according to the guidelines given in IEEE 1528 [1]. The dipoles are made from semi-rigid 50 Ohm co-ax, which is joined by soldering and is gold-plated subsequently. The constructed dipoles are easily deformed, if mis-handled, and periodic checks need to be made of their symmetry.

Rohacell foam spacers designed for presenting the dipoles to 2mm thick PMMA box phantoms. These components also suffer wear and tear and should be replaced when the central hole is a loose-fit on the dipole arms or if the edges are too worn to ensure accurate alignment. The standard spacers are dimensioned for use with 2mm wall thickness (additional spacers are available for 4mm wall thickness).

2. Typical SAR Measurement

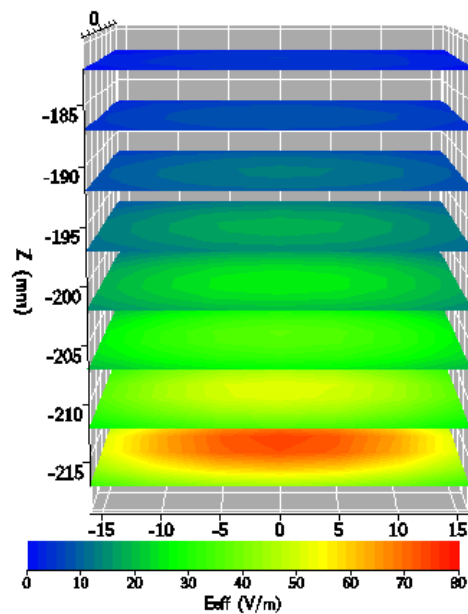
A SAR validation check is performed with the box-phantom located on the SARA2 phantom support base on the SARA2 robot system. Tests are then conducted at a feed power level of approx. 0.25W. The actual power level is recorded and used to normalise the results obtained to the standard input power conditions of 1W (forward power). The ambient temperature is 23°C +/- 1°C and the relative humidity is around 67% during the measurements.

The phantom is filled with a 450MHz brain liquid using a recipe from [1], which has the following electrical parameters (measured using an Indexsar DiLine kit) at 450MHz +/-10%:

Relative Permittivity **43.5**
Conductivity **0.87 S/m**

The SARA2 software version 0.421N is used with an Indexsar probe previously calibrated using waveguides.

The 3D measurements made using the dipole at the bottom of the phantom box is shown below:



The results, normalised to an input power of 1W (forward power) are typically:

Averaged over 1 cm³ (1g) of tissue **4.9 W/kg**
Averaged over 10cm³ (10g) of tissue **3.3 W/kg**

These results can be compared with Table 8.1 in [1]. The agreement is within 10%.

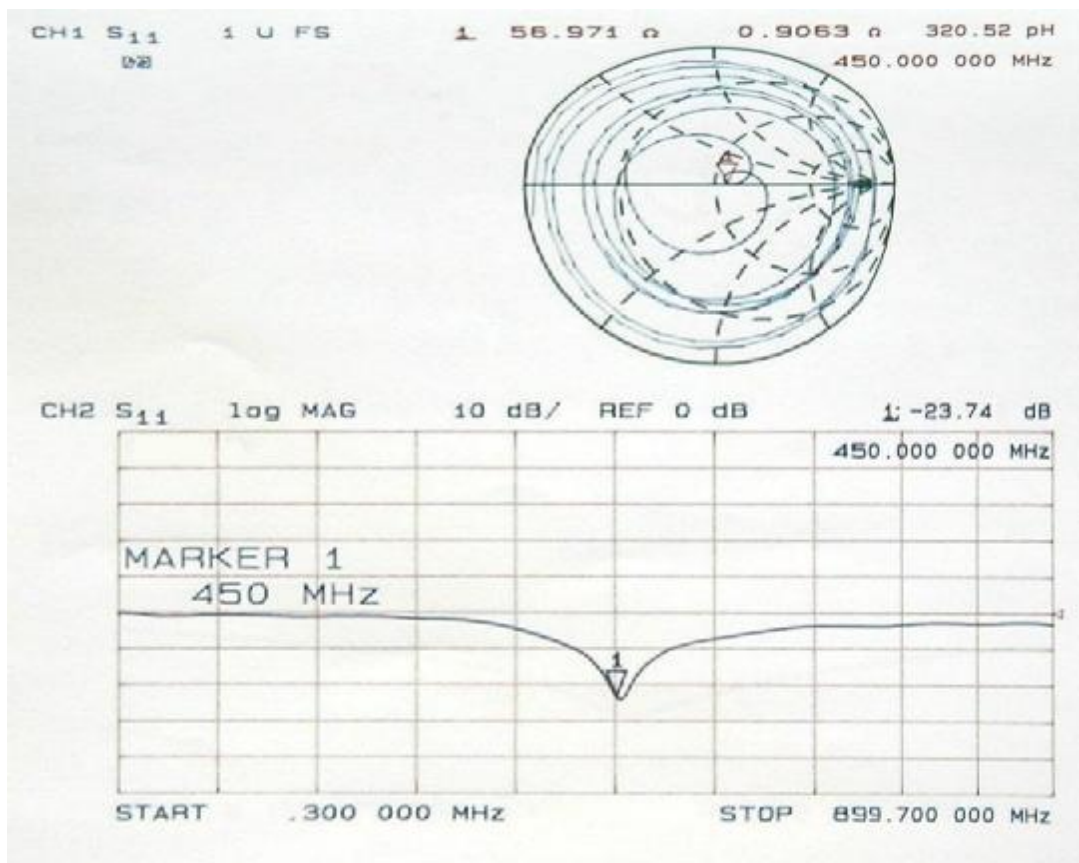
3. Dipole impedance and return loss

The dipoles are designed to have low return loss ONLY when presented against a lossy-phantom at the specified distance. A Vector Network Analyser (VNA) was used to perform a return loss measurement on the specific dipole when in the measurement-location against the box phantom. The distance was as specified in the standard i.e. 10mm from the liquid (for 450MHz). The Indexsar foam spacers (described above) were used to ensure this condition during measurement.

The impedance was measured at the SMA-connector with the network analyser.
The following parameters were measured:

Dipole impedance at 450 MHz $\text{Re}\{Z\} = 56.971 \Omega$
 $\text{Im}\{Z\} = 0.9063 \Omega$

Return loss at 450MHz **-23.74 dB**



4. Dipole handling

The dipoles are made from standard, copper-sheathed coaxial cable. In assembly, the sections are joined using ordinary soft-soldering. This is necessary to avoid excessive heat input in manufacture, which would destroy the polythene dielectric used for the cable. The consequence of the construction material and the assembly technique is that the dipoles are fragile and can be deformed by rough handling. Conversely, they can be straightened quite easily as described in this report.

If a dipole is suspected of being deformed, a normal workshop lathe can be used as an alignment jig to restore the symmetry. To do this, the dipole is first placed in the headstock of the lathe (centred on the plastic or brass spacers) and the headstock is rotated by hand (do NOT use the motor). A marker (lathe tool or similar) is brought up close to the end of one dipole arm and then the headstock is rotated by 0.5 rev. to check the opposing arm. If they are not balanced, judicious deformation of the arms can be used to restore the symmetry.

If a dipole has a failed solder joint, the dipole can be fixed down in such a way that the arms are co-linear and the joint re-soldered with a reasonably-powerful electrical soldering iron. Do not use gas soldering irons. After such a repair, electrical tests must be performed as described below.

Please note that, because of their construction, the dipoles are short-circuited for DC signals.

5. Tuning the dipole

The dipole dimensions are based on calculations that assumed specific liquid dielectric properties. If the liquid dielectric properties are somewhat different, the dipole tuning will also vary. A pragmatic way of accounting for variations in liquid properties is to 'tune' the dipole (by applying minor variations to its effective length). For this purpose, Indexsar can supply short brass tube lengths to extend the length of the dipole and thus 'tune' the dipole. It cannot be made shorter without removing a bit from the arm. An alternative way to tune the dipole is to use copper shielding tape to extend the effective length of the dipole. Do both arms equally.

It should be possible to tune a dipole as described, whilst in place in the measurement position as long as the user has access to a VNA for determining the return loss.

6. References

[1] Draft recommended practice for determining the peak spatial-average specific absorption rate (SAR) in the human body due to wireless communications devices: Experimental Techniques.

[2] Calibration report on SAR probe IXP-050 S/N 0071 from National Physical Laboratory. Test Report EF07/2002/03/IndexSAR. Dated 20 February 2002.