

Specific Absorption Rate (SAR) Test Report

for

Z-Com, Inc.

on the

54Mbps 802.11g USB Adapter

Model Number: XG-705A

Test Report: EME-050357

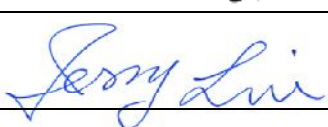
Date of Report: May 12, 2005

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Accredited for testing to FCC Part 15

Tested by: Kevin Chen	
Reviewed by: Jerry Liu	

Review Date: May 12, 2005

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STATEMENT OF COMPLIANCE

The Z-Com sample device, model # XG-705A was evaluated in accordance with the requirements for compliance testing defined in FCC OET Bulletin 65, Supplement C (Edition 01-01). Testing was performed at the Intertek Testing Services facility in Hsinchu, Taiwan.

For the evaluation, the dosimetric assessment system INDEXSAR SARA2 was used. The phantom employed was the box phantom of 2mm thick in each wall. The total uncertainty for the evaluation of the spatial peak SAR values averaged over a cube of 1g tissue mass had been assessed for this system to be $\pm 20.6\%$.

The device was tested at their maximum output power declared by the Z-Com.

In summary, the maximum spatial peak SAR value for the sample device averaged over 1g was found to be:

Phantom	Position (worst case)	SAR _{1g} W/kg
2mm thick box phantom wall	802.11b Mid channel EUT perpendicular to the phantom, 0 mm separation.	0.220 W/kg

In conclusion, the tested Sample device was found to be in compliance with the requirements defined in OET Bulletin 65, Supplement C (Edition 01-01) for body configurations.

1.0 Job Description

1.1 Client Information

The XG-705A has been tested at the request of:

Company: Z-Com, Inc.
7F-2, No. 9, Prosperity RD.I Science-Based Industrial Park,
Hsinchu, Taiwan

1.2 Equipment under test (EUT)

Product Descriptions:

Equipment	54Mbps 802.11g USB Adapter		
Trade Name	Z-Com.	Model No:	XG-705A
FCC ID	M4Y-XG705A	S/N No.	Not Labeled
Category	Portable	RF Exposure	Uncontrolled Environment
Frequency Band	2412 – 2462 MHz	System	DSSS, OFDM

EUT Antenna Description			
Type	Printed	Configuration	Fixed
Dimensions	0.5 x 2cm	Gain	1.0 dBi
Location	Embedded		

Use of Product : 54Mbps 802.11g USB Adapter

Manufacturer: Z-Com, Inc.

Production is planned: [X] Yes, [] No

EUT receive date: Apr. 16, 2005

EUT received condition: Good operating condition prototype

Test start date: Apr. 18, 2005

Test end date: Apr. 18, 2005

1.3 Test plan reference

FCC Rule: Part 2.1093, FCC's OET Bulletin 65, Supplement C (Edition 01-01) and IEEE 1528

1.4 System test configuration

1.4.1 Support equipment & System block diagram

Support Equipment				
Item #	Equipment	Brand	Model No.	S/N
1	Notebook PC	DELL	PP01L	CN-06P83-48643-33V-0112



EUT

1.4.2 Test Position

See the photographs as section 2.2

1.4.3 Test Condition

During tests the worst-case data (max RF coupling) was determined with following conditions:

Usage	Operates with a portable computer	Distance between antenna axis at the joint and the liquid surface:	Laptop is touching the Phantom in bottom position, separating 0mm in front position, separating 0mm and 15mm in rear position.	
Simulating human Head/ Body/Hand	Body	EUT Battery	Device is powered from host computer through battery.	
802.11b Conducted output Power	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
	Low Channel - 1	2412	18.39	-
	Mid Channel - 6	2437	18.32	18.31
	High Channel- 11	2462	18.07	-
802.11g Conducted output Power	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
	Low Channel - 1	2412	17.69	-
	Mid Channel - 6	2437	17.65	17.64
	High Channel- 11	2462	17.43	-

The spatial peak SAR values were assessed for lowest, middle and highest operating channels, defined by the manufacturer.

The conducted output power was measured before and after the test using a wideband peak power meter.

Run the test program “Prism Engineering Tool.exe” under Windows OS. The EUT was transmitted continuously during the test.

After verifying the maximum output power, we found the maximum output power was occurred at 11Mbps data rate in 802.11b and at 6 Mbps data rate in 802.11g.

All the test data were performed under the above transmission rate.

1.5 Modifications required for compliance

Intertek Testing Services implemented no modifications.

1.6 Additions, deviations and exclusions from standards

The phantom employed was the box phantom of 2mm thick in vertical wall.

2.0 SAR Evaluation

2.1 SAR Limits

The following FCC limits for SAR apply to devices operate in General Population/Uncontrolled Exposure environment:

EXPOSURE (General Population/Uncontrolled Exposure environment)	SAR (W/kg)
Average over the whole body	0.08
Spatial Peak (1g)	1.60
Spatial Peak for hands, wrists, feet and ankles (10g)	4.00

2.2 Configuration Photographs

SAR Measurement Test Setup

Test System



SAR Measurement Test Setup

Bottom side of Laptop facing phantom touching

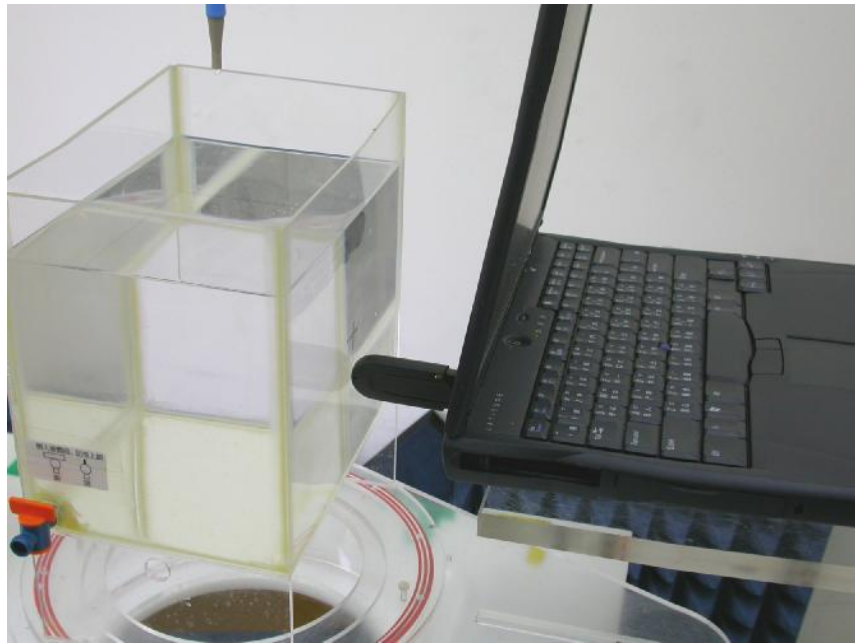


Bottom side of Laptop facing phantom touching-Zoon In



SAR Measurement Test Setup

EUT rear to phantom, 0 mm separation

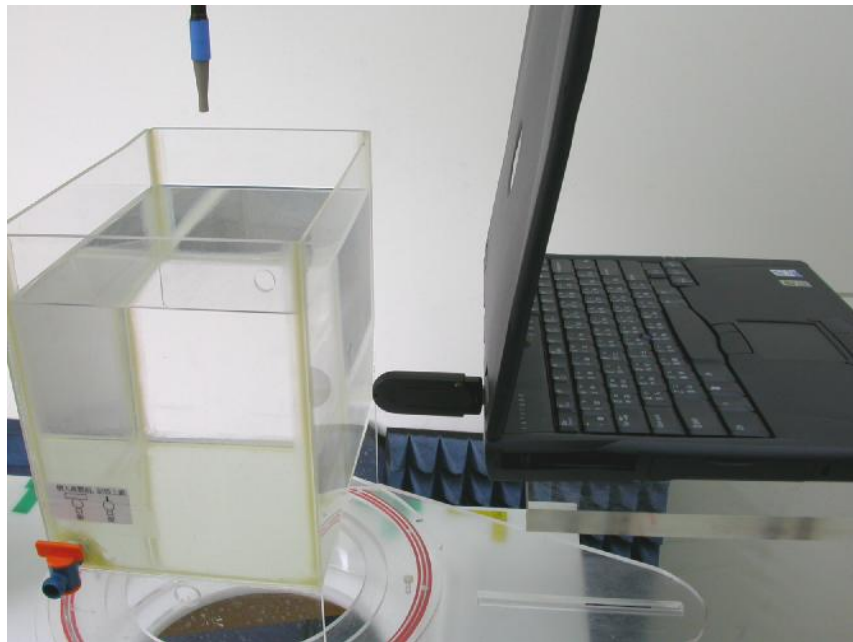


EUT perpendicular to phantom, 0 mm separation-Zoon In

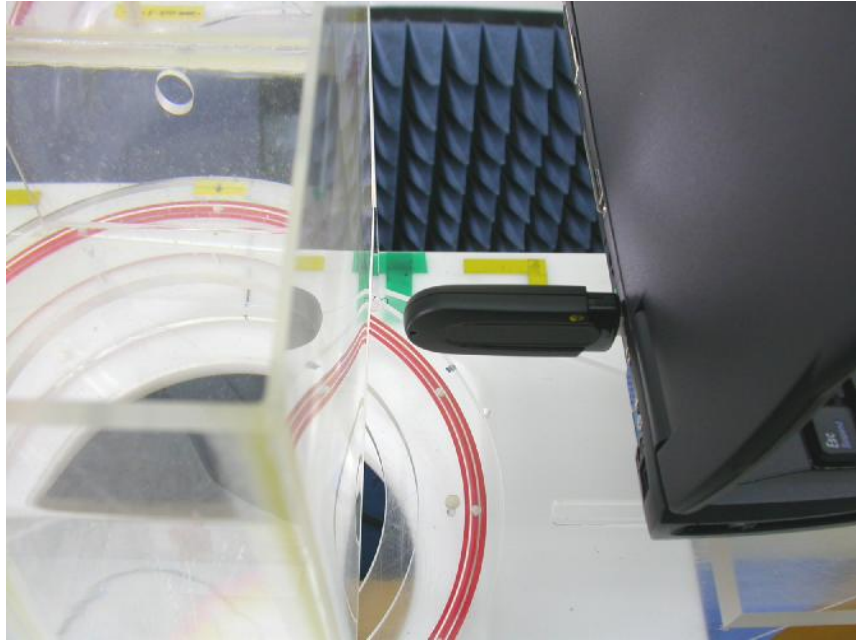


SAR Measurement Test Setup

EUT rear to phantom, 15 mm separation



EUT perpendicular to phantom, 15 mm separation-Zoon In



2.3 SAR measurement system

Robot system specification

The SAR measurement system being used is the IndexSAR SARA2 system, which consists of a Mitsubishi RV-E2 6-axis robot arm and controller, IndexSAR probe and amplifier and SAM phantom Head Shape. The robot is used to articulate the probe to programmed positions inside the phantom head to obtain the SAR readings from the DUT.

The system is controlled remotely from a PC, which contains the software to control the robot and data acquisition equipment. The software also displays the data obtained from test scans.

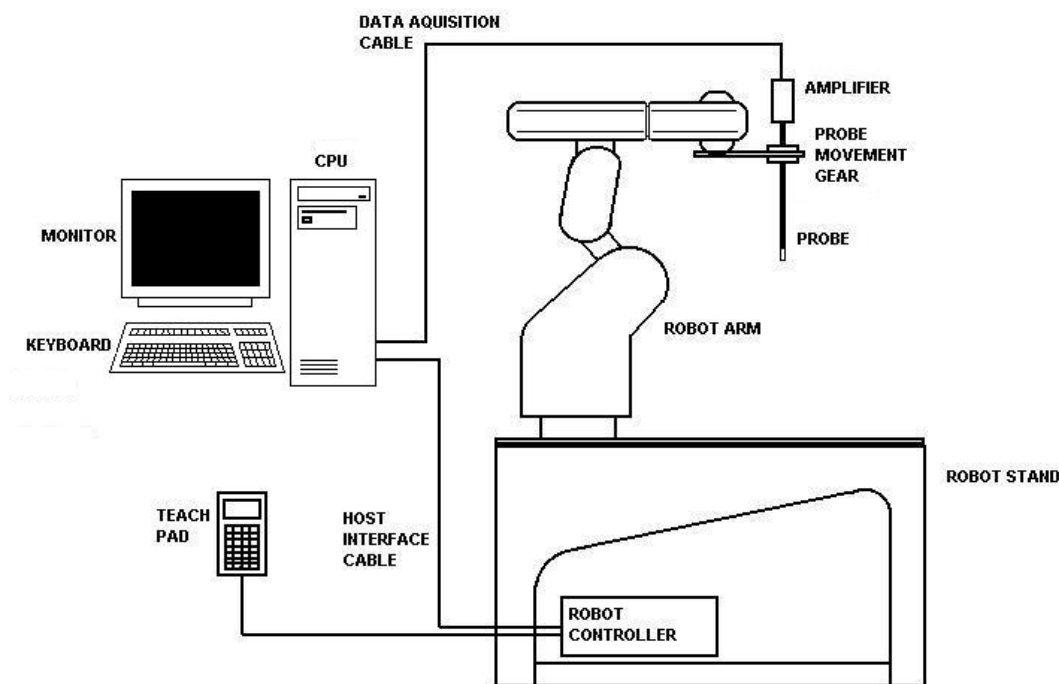


Figure 1: Schematic diagram of the SAR measurement system

The position and digitised shape of the phantom heads are made available to the software for accurate positioning of the probe and reduction of set-up time.

The SAM phantom heads are individually digitised using a Mitutoyo CMM machine to a precision of 0.02mm. The data is then converted into a shape format for the software, providing an accurate description of the phantom shell. In operation, the system first does an area (2D) scan at a fixed depth within the liquid from the inside wall of the phantom. When the maximum SAR point has been found, the system will then carry out a 3D scan centred at that point to determine volume averaged SAR level.

The first 2 measurements points in a direction perpendicular to the surface of the phantom during the zoom scan and closest to the phantom surface, were only 3.5mm and the probe is kept at greater than half a diameter from the surface.

2.4 SAR measurement system validation

Prior to the assessment, the system was verified to the $\pm 10\%$ of the specifications by using the system validation equipments. The validation was performed at 2450 MHz on the bottom side of box phantom.

Procedures

The SAR evaluation was performed with the following procedures:

- a. The SAR distribution was measured at the exposed side of the bottom of the box phantom and was measured at a distance of 8 mm from the inner surface of the shell. The feed power was 1/5 W.
- b. The dimension for this cube is 32 mm x 32 mm x 34 mm was assessed by measuring 5 x 5 x 7 points. On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure:
 - i) The data at the surface were extrapolated, since the center of the dipoles is 2.7 mm away from the tip of the probe and the distance between the surface and the lowest measurement point is 5 mm. The extrapolation was based on a least square algorithm. A polynomial of the fourth order was calculated through the points in Z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.
 - ii) The maximum interpolated value was searched with a straightforward algorithm. Around this maximum, the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3-D spline interpolation algorithm. The 3-D spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y and z directions). The volume was integrated with the trapezoidal algorithm. 1000 points (10 x 10 x 10) were interpolated to calculate the average.
 - iii) All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

The test scan procedure for system validation also apply to the general scan procedure except for the set-up position. For general scan, the EUT was placed at the side of phantom. For validation scan, the dipole antenna was placed at the bottom of phantom

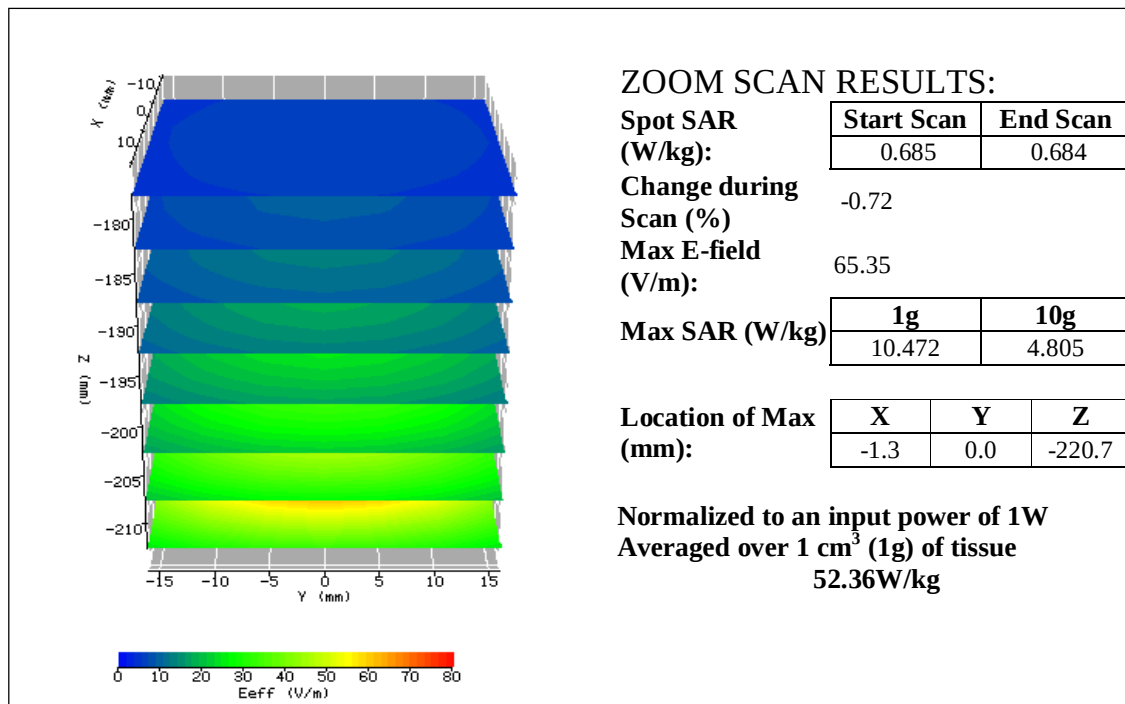
2.4.1 System Validation result

System Validation (2450 MHz Head)				
Frequency MHz	Operating Mode	Target SAR _{1g} (W/kg)	Measured SAR _{1g} (W/kg)	Deviation (±10%)
2450	CW	52.4	52.36	-0.07%

Please see the plot below:

Date:	2004/10/1	Position:	Bottom
Filename:	2450val10-15.txt	Phantom:	Box1.csv
Device Tested:	SARA2 system	Head Rotation:	0
Antenna:	2450dipole	Test Frequency:	2450MHz
Shape File:	none.csv	Power Level:	23dBm /CW

Probe:	0149	Liquid:	15.5cm
Cal File:	SN0149_2450_CW_HEAD	Type:	2450MHz Head
Cal Factors:		Conductivity:	1.804
		Relative Permittivity:	38.122
	Air	Liquid Temp (deg C):	23.3
	DCP	Ambient Temp (deg C):	23
	Lin	Ambient RH (%):	50
Amp Gain:	2	Density (kg/m3):	1000
Averaging:	1	Software Version:	2.3VPM
Batteries	-	Crest Factor = 1	
Replaced:			



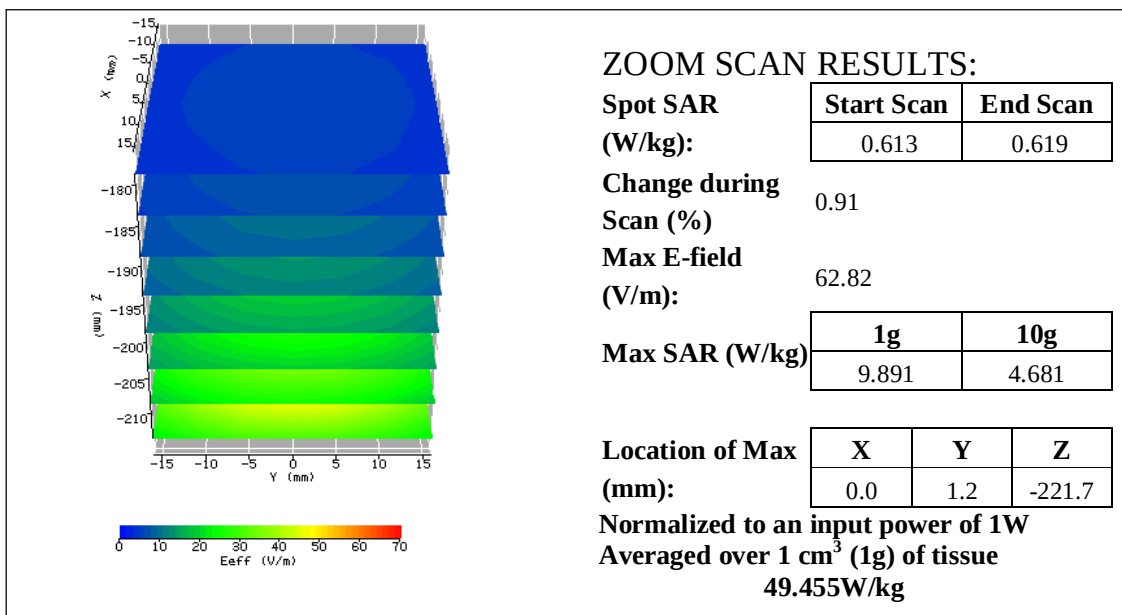
2.4.2 System Performance Check result

System performance check (2450 MHz Head)				
Frequency MHz	Operating Mode	Target SAR _{1g} (W/kg)	Measured SAR _{1g} (W/kg)	Deviation (±10%)
2450	CW	52.4	49.455	-5.62%

Please see the plot below:

Date:	2005/4/17	Position:	Bottom of phantom box
Filename:	2450performance check .txt	Phantom:	HeadBox1-val..csv
Device Tested:	2450 MHz performance check	Head Rotation:	0
Antenna:	Dipole antenna	Test Frequency:	2450 MHz
Shape File:	none.csv	Power Level:	23 dBm

Probe:	0149	Liquid:	15.5cm
Cal File:	SN0149_2450_CW_HEAD	Type:	2450 MHz head
Cal Factors:		Conductivity:	1.828
		Relative Permittivity:	39.931
		Liquid Temp (deg C):	23.2
		Ambient Temp (deg C):	23.5
Amp Gain:	2	Ambient RH (%):	50.2
Averaging:	1	Density (kg/m3):	1000
Batteries		Software Version:	2.33VPM
Replaced:	-	Crest Factor = 1	



2.5 Test Result

The results on the following page(s) were obtained when the device was tested in the condition described in this report. Detailed measurement data and plots, which reveal information about the location of the maximum SAR with respect to the device, are reported in Appendix A.

Measurement Results

Trade Name:	Z-Com	Model No.:	XG-705A
Serial No.:	Not Labeled	Test Engineer:	Kevin Chen
TEST CONDITIONS			
Ambient Temperature	22 °C	Relative Humidity	55 %
Test Signal Source	Test Mode	Signal Modulation	DSSS, OFDM
Output Power Before SAR Test	See page 6	Output Power After SAR Test	See page 6
Test Duration	23 min. each scan	Number of Battery Change	1

EUT Position						
Channel (MHz)	Operating Mode	Crest Factor	Description	Distance (mm)	Measured SAR_{1g} (W/kg)	Plot Number
2437	DSSS	1	Perpendicular to phantom	0	0.220	1
2437	OFDM	1	Perpendicular to phantom	0	0.142	2
2437	DSSS	1	Perpendicular to phantom	15	0.076	3
2437	OFDM	1	Perpendicular to phantom	15	0.056	4
2437	DSSS	1	NB Bottom to phantom	0	0.208	5
2437	OFDM	1	NB Bottom to phantom	0	0.127	6

Note: 1. The distance from bottom of EUT to flat phantom is 4 mm.
2. Configuration at middle channel with more than -3dB of applicable limit.

3.0 Test Equipment

3.1 Equipment List

The Specific Absorption Rate (SAR) tests were performed with the INDEXSAR SARA2 SYSTEM.

The following major equipment/components were used for the SAR evaluations:

SAR Measurement System			
EQUIPMENT	SPECIFICATIONS	Intertek ID No.	LAST CAL. DATE
Balanced Validation dipole	2450MHz	EC381-4	03/26/2005
Controller	Mitsubishi CR-E116	EP320-1	N/A
Robot	Mitsubishi RV-E2	EP320-2	N/A
	Repeatability: $\pm 0.04\text{mm}$; Number of Axes: 6		
E-Field Probe	IXP-050	EC356	05/2004
	Frequency Range: Probe outer diameter: 5.2 mm; Length: 350 mm; Distance between the probe tip and the dipole center: 2.7 mm		
Data Acquisition	SARA2	N/A	N/A
	Processor: Pentium 4; Clock speed: 1.5GHz; OS: Windows XP; I/O: two RS232; Software: SARA2 ver. 2.3VPM (Virtual Probe Minaturisation)		
Phantom	2mm wall thickness box phantom	N/A	N/A
	Shell Material: clear Perspex; Thickness: $2 \pm 0.1\text{ mm}$; Capacity: $152.5 \times 225.5 \times 200\text{ (W x L x D) mm}^3$; Dielectric constant: less than 2.85 above 500MHz;		
Device holder	Material: clear Perspex; Dielectric constant: less than 2.85 above 500MHz	N/A	N/A
Simulated Tissue	Mixture	N/A	04/17/2005
	Please see section 3.2 for details		
RF Power Meter	Boonton 4231A with 51011-EMC power sensor	EC359	03/12/2005
	Frequency Range: 0.03 to 8 GHz, <24dBm		
Vector Network Analyzer	HP 8753B HP 85046A	EC375	08/19/2004
	Frequency Range: 300k to 3GHz		
Signal Generator	R&S SMR27	EC354	08/19/2004
	Frequency Range: 10M to 27GHz, <120dBuV		
Wideband Peak Power Meter/ Sensor	Anritsu ML2497A with MA2491A Power sensor	EC396	10/18/2004
	Frequency Range: 100MHz~18GHz		

3.2 Tissue Simulating Liquid

The head and body tissue parameters should be used to test operating frequency band of transmitters. When a transmission band overlaps with one of the target frequencies, the tissue dielectric parameters of the tissue medium at the middle of a device transmission band should be within $\pm 5\%$ of the parameters specified at that target frequency.

3.2.1 Body Tissue Simulating Liquid for evaluation test

Body Ingredients Frequency (2.45 GHz)	
DGBE (Dilethylene Glycol Butyl Ether)	26.7%
Salt	0.04%
Water	73.2%

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e _r / Relative Permittivity			s / Conductivity (mho/m)			r *(kg/m ³)
		measured	target	△(±5%)	measured	target	△(±5%)	
2450	22.3	51.86	52.7	-1.59%	1.985	1.95	1.79%	1000

* Worst-case assumption

3.2.2 Head Tissue Simulating Liquid for System performance Check test

Head Ingredients Frequency (2.45 GHz)	
DGBE (Dilethylene Glycol Butyl Ether)	53.3%
Water	46.7%

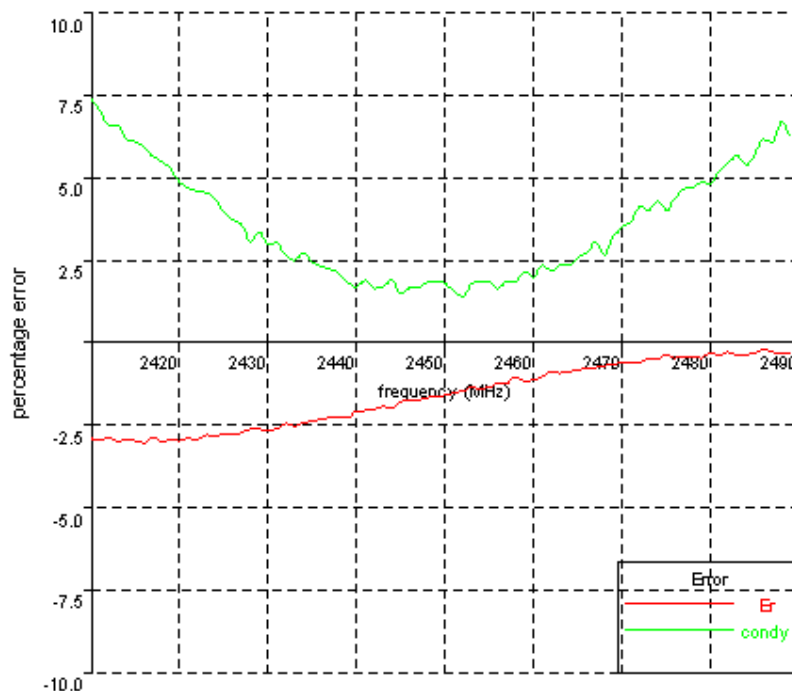
The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e _r / Relative Permittivity			s / Conductivity (mho/m)			r *(kg/m ³)
		measured	target	△(±5%)	measured	target	△(±5%)	
2450	23.6	39.93	39.2	-1.86%	1.828	1.80	1.55	1000

* Worst-case assumption

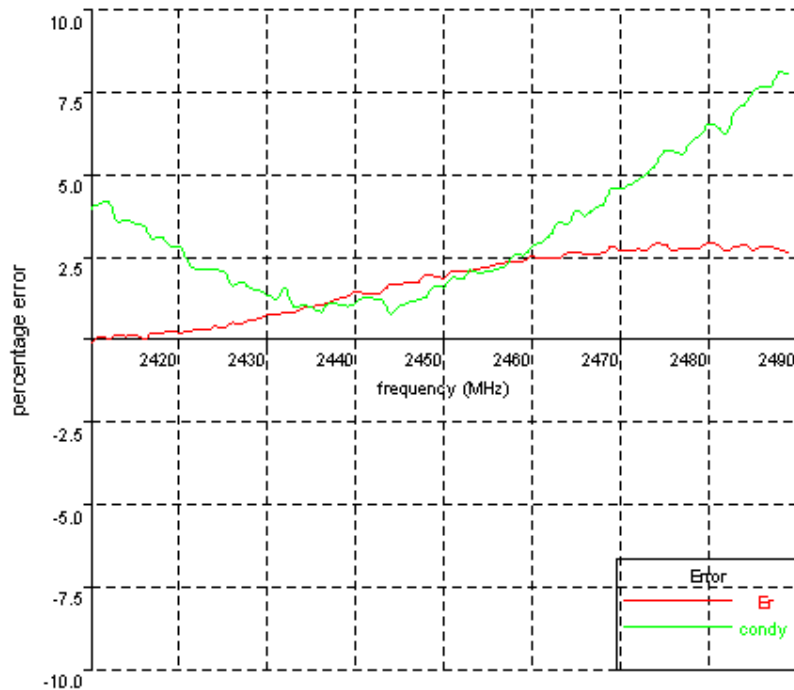
3.2.3 Body Liquid results

Date: 17 Apr. 2005	Temperature: 22.3 °C	Type: 2450 MHz/ body	Tested by: Kevin
2410, 51.2164588719, -2.053438391 2411, 51.2064395949, -2.0472486778 2412, 51.2322818306, -2.0400292938 2413, 51.174385997, -2.0410709634 2414, 51.2090545483, -2.0337021628 2415, 51.1756573592, -2.0331436402 2416, 51.1455464229, -2.0305674625 2417, 51.2221223623, -2.0268396647 2418, 51.1669123314, -2.024820304 2419, 51.1975862605, -2.0213832947 2420, 51.1700736998, -2.0144999437 2421, 51.2032369435, -2.012611683 2422, 51.1925111282, -2.0116125133 2423, 51.2603130575, -2.011361625 2424, 51.2488279708, -2.0088762017 2425, 51.2673786023, -2.002402375 2426, 51.2689109207, -1.9986115587 2427, 51.2928529535, -1.9974720186 2428, 51.345663005, -1.9876632049 2429, 51.348944031, -1.9945790913 2430, 51.3189182858, -1.988487864 2431, 51.3495574119, -1.9904479531 2432, 51.429641011, -1.9834437937 2433, 51.3895210957, -1.9819282792 2434, 51.4520820586, -1.9875077372 2435, 51.4570205066, -1.9829986752 2436, 51.5109008044, -1.9810778524 2437, 51.5127783767, -1.9807225429 2438, 51.52982136, -1.9791223141 2439, 51.528506556, -1.9744126472 2440, 51.6140124311, -1.9731866571 2441, 51.6299597481, -1.9780930687 2442, 51.6503050795, -1.9743276773 2443, 51.6876212424, -1.976029726 2444, 51.6697009982, -1.9814156344 2445, 51.7659436639, -1.9740119892 2446, 51.7939938752, -1.9784898255 2447, 51.793823965, -1.9798748816 2448, 51.8216626257, -1.9838694717 2449, 51.8401938557, -1.9854113004 2450, 51.8592987939, -1.9852921322 2451, 51.8860378865, -1.9817323699 2452, 51.9233970374, -1.9801772084 2453, 51.976856284, -1.988902377 2454, 51.9668882535, -1.9920846033 2455, 51.9871662764, -1.9932571261 2456, 52.0368347411, -1.9904012357 2457, 52.0444850769, -1.9966410701 2458, 52.1345213365, -1.9977692105 2459, 52.0698961352, -2.0050577944 2460, 52.0859843077, -2.003070342 2461, 52.1501914962, -2.0118577846 2462, 52.2155816783, -2.009980148 2463, 52.1983024785, -2.0146888288 2464, 52.2125271785, -2.0160560616 2465, 52.2494878351, -2.0226414865 2466, 52.2648695039, -2.0263217067 2467, 52.2791123442, -2.0345131832 2468, 52.3096904343, -2.0283388984 2469, 52.333555784, -2.0398724991 2470, 52.3551230844, -2.0476723612 2471, 52.3481895032, -2.0523245058 2472, 52.3449457059, -2.0631317723 2473, 52.4105800868, -2.0619396354 2474, 52.4119173219, -2.0694572315 2475, 52.4670269676, -2.0652029898 2476, 52.4213015767, -2.0735259146 2477, 52.4388171695, -2.0812501054 2478, 52.4446149977, -2.0835642238 2479, 52.4202534665, -2.0878638891 2480, 52.489107511, -2.0885056175 2481, 52.4659369693, -2.0984183335 2482, 52.508533775, -2.1039006832 2483, 52.4671706147, -2.1104334865 2484, 52.4685092937, -2.1058050105 2485, 52.4872718336, -2.11363283 2486, 52.5471200187, -2.1244999374 2487, 52.5047313089, -2.1235254821 2488, 52.469915349, -2.1380229259 2489, 52.4879130078, -2.1313226521 2490, 52.528612918, -2.1409375485			



3.2.4 Head Liquid results

Date: 17 Apr. 2005	Temperature: 23.6 °C	Type: 2450 MHz/ head	Tested by: Kevin
2410, 39.2345433256, -1.8346923863 2411, 39.3086266014, -1.838452495 2412, 39.2776615581, -1.839933076 2413, 39.3195342162, -1.8300057131 2414, 39.3050424214, -1.8317748307 2415, 39.3166133893, -1.8312925057 2416, 39.2742357732, -1.8306498379 2417, 39.3330377942, -1.8246464418 2418, 39.3349016059, -1.8270587714 2419, 39.3609683365, -1.822446932 2420, 39.3344604754, -1.823630692 2421, 39.357514106, -1.8165546449 2422, 39.3619947439, -1.8126812077 2423, 39.3586468319, -1.813544192 2424, 39.403047253, -1.8145593957 2425, 39.3904387163, -1.8146389178 2426, 39.4446221967, -1.8079301334 2427, 39.4286471247, -1.8108310181 2428, 39.4789493875, -1.8083328936 2429, 39.4851852624, -1.8080989222 2430, 39.5277113858, -1.8060963008 2431, 39.5281436213, -1.8052385525 2432, 39.5552600634, -1.8121064751 2433, 39.5430352187, -1.802257416 2434, 39.6048499084, -1.8044620155 2435, 39.6208898726, -1.8040260663 2436, 39.6379476536, -1.8027756625 2437, 39.6651394217, -1.8082333891 2438, 39.7078593583, -1.808308656 2439, 39.7360984559, -1.8085051165 2440, 39.796944894, -1.8109751627 2441, 39.7641457789, -1.8148780743 2442, 39.7613432896, -1.8151927635 2443, 39.781699536, -1.8152469457 2444, 39.8748250843, -1.8086556733 2445, 39.8743890531, -1.8139942736 2446, 39.8943669344, -1.8166244726 2447, 39.8752539286, -1.8188625643 2448, 39.9799975554, -1.8217058922 2449, 39.9485036452, -1.8286978984 2450, 39.9317422561, -1.8286370292 2451, 40.0203753947, -1.8350947215 2452, 40.0085901503, -1.8353697097 2453, 40.0115551725, -1.8413283098 2454, 40.0420932479, -1.8411494543 2455, 40.059770421, -1.8428695698 2456, 40.0881282787, -1.8450498001 2457, 40.1068490056, -1.8478832868 2458, 40.1136226977, -1.855491435 2459, 40.1260167091, -1.8561312898 2460, 40.1698186623, -1.8621279813 2461, 40.1513251701, -1.865640765 2462, 40.1616813276, -1.8704733576 2463, 40.1449768565, -1.8784277836 2464, 40.2095410739, -1.8793502588 2465, 40.2204986843, -1.8876686933 2466, 40.1997641505, -1.8855161669 2467, 40.1982988691, -1.8907584185 2468, 40.2046483684, -1.8941060113 2469, 40.281591159, -1.9038705297 2470, 40.2356303512, -1.9050912356 2471, 40.2311816453, -1.9082731211 2472, 40.2436119792, -1.9122341493 2473, 40.2406291082, -1.9167409299 2474, 40.3157303762, -1.9231916333 2475, 40.2964154993, -1.9320084359 2476, 40.2262891523, -1.9328531548 2477, 40.249949577, -1.9321169245 2478, 40.2548399459, -1.9411859482 2479, 40.2489219893, -1.94468312 2480, 40.3206095916, -1.952777624 2481, 40.2771498129, -1.9518340266 2482, 40.2232154967, -1.9494104676 2483, 40.2547133083, -1.963803314 2484, 40.2808023242, -1.9679714153 2485, 40.2179487454, -1.9759212048 2486, 40.2569598319, -1.9803766234 2487, 40.2545627986, -1.9820478532 2488, 40.2208000725, -1.9907408191 2489, 40.1846735022, -1.991204627 2490, 40.2162730621, -1.9980245525			



3.3 E-Field Probe and 2450 Balanced Dipole Antenna Calibration

Probe calibration factors and dipole antenna calibration are included in Appendix C.

4.0 Measurement Uncertainty

The uncertainty budget has been determined for the INDEXSAR SARA2 measurement system according to IEEE P1528 documents [3] and is given in the following table. The extended uncertainty (95% confidence level) was assessed to be 20.6 % for SAR measurement, and the extended uncertainty (95% confidence level) was assessed to be 20.2 % for system performance check.

Table 1 Exposure Assessment Uncertainty
Example of measurement uncertainty assessment SAR measurement

(blue entries are site-specific)

a	b			c	d	e		f	g	h	i
Uncertainty Component	Sec.	Tol. (+/-)		Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g	
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	√3	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	√3	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	√3	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	√3	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	√3	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	√3	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	√3	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	√3	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	√3	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	√3	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	√3	1.73	1	1	4.62	4.62
Test Sample Related											
Test Sample Positioning	E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Device Holder Uncertainty	E4.1		2	2.00	N	1	1.00	1	1	2.00	2.00
Output Power Variation	6.6.2		5	5.00	R	√3	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (shape and thickness)	E3.1		4	4.00	R	√3	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.5	10.3
Expanded uncertainty	(95% Confidence Level)				k=2					20.6	20.3

Table 2 System Check (Verification)

Example of measurement uncertainty assessment for system performance check

(blue entries are site-specific)

a	b			c	d	e		f	g	h	i
Uncertainty Component	Sec.	Tol. (+/-)			Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	$\sqrt{3}$	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	$\sqrt{3}$	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	$\sqrt{3}$	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	$\sqrt{3}$	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	$\sqrt{3}$	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	$\sqrt{3}$	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	$\sqrt{3}$	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	$\sqrt{3}$	1.73	1	1	4.62	4.62
Dipole											
Dipole axis to liquid distance	8, E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Input power and SAR drift measurement	8, 6.6.2		5	5.00	R	$\sqrt{3}$	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (thickness)	E3.1		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.3	10.1
Expanded uncertainty	(95% Confidence Level)				k=2					20.2	19.9

5.0 Measurement Traceability

All measurements described in this report are traceable to Chinese National Laboratory Accreditation (CNLA) standards or appropriate national standards.

6.0 WARNING LABEL INFORMATION - USA

See user manual.

7.0 REFERENCES

- [1] ANSI, *ANSI/IEEE C95.1-1999: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3kHz to 300 GHz*, The Institute of electrical and Electronics Engineers, Inc., New York, NY 10017, 1999

- [2] Federal Communications Commission, "Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields", Supplement C to OET Bulletin 65, Washington, D.C. 20554, 1997

- [3] IEEE Standards Coordinating Committee 34, "IEEE Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques", IEEE Std 1528TM-2003

8.0 DOCUMENT HISTORY

Revision/ Job Number	Writer Initials	Date	Change
N/A	I.C	May 12, 2005	Original document

APPENDIX A - SAR Evaluation Data

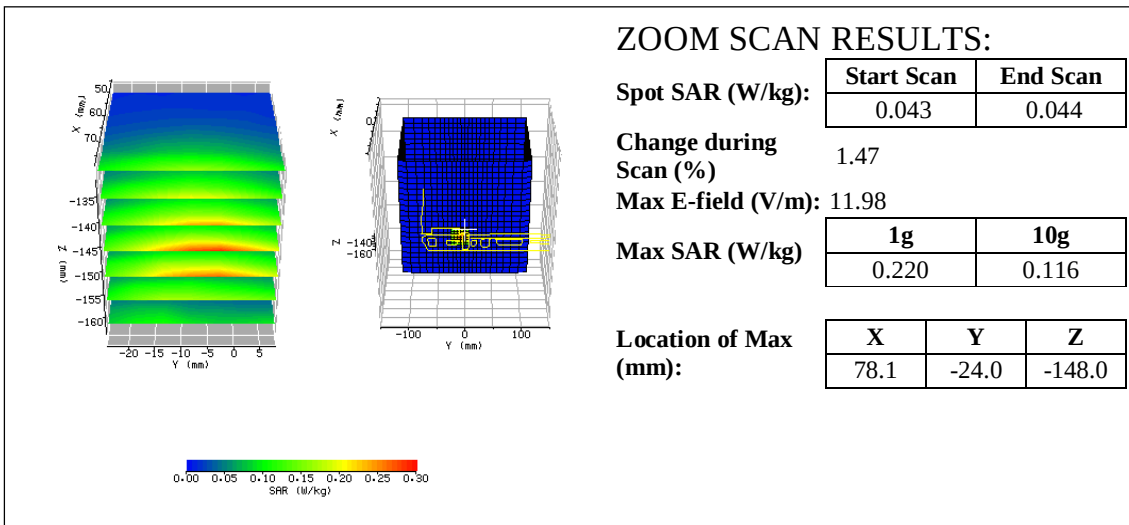
Power drift is the measurement of power drift of the device over one complete SAR scan. To assess the drift of the power of the device under test, a SAR measurement was made in the middle of the zoom scan volume at the start of the scan and a measurement at this point was then also made after the measurement scan. The difference between the two measurements should be less than 5%.

Plot #1(1/2)

Date:	2005/4/18	Position:	perpendicular to the phantom 0mm
Filename:	per0_11b-ch6.txt	Phantom:	HeadBox2-test.csv
Device Tested:	XG-705A	Head Rotation:	0
Antenna:	PCB printed	Test Frequency:	11b_2437MHz
Shape File:	XG-705A-per..csv	Power Level:	18.32 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.9853
Relative Permittivity:	51.8593
Liquid Temp (deg C):	22
Ambient Temp (deg C):	22
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.33VPM
Crest Factor =	1

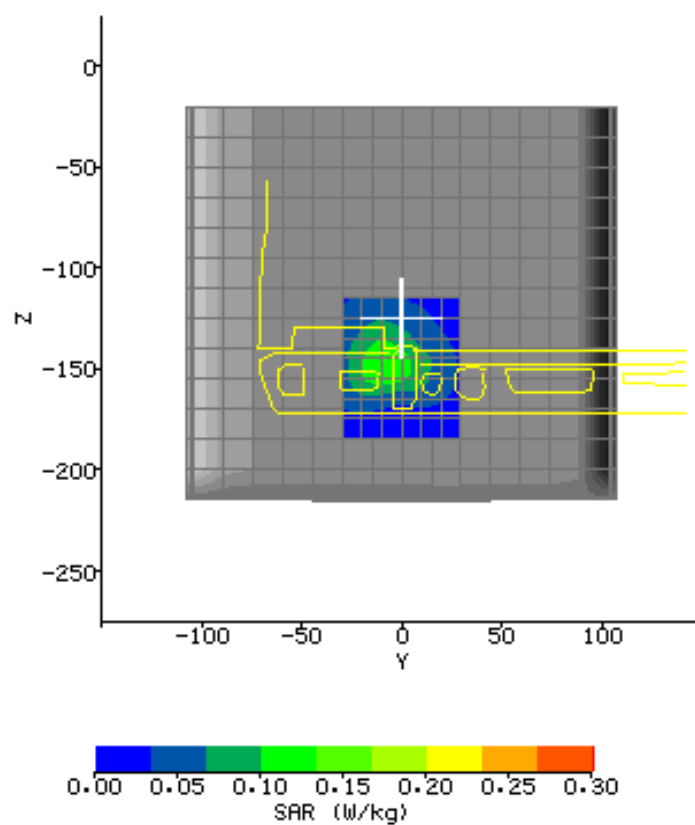


Plot #1(22)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-30.0	30.0	6.0
Z	-185.0	-115.0	7.0

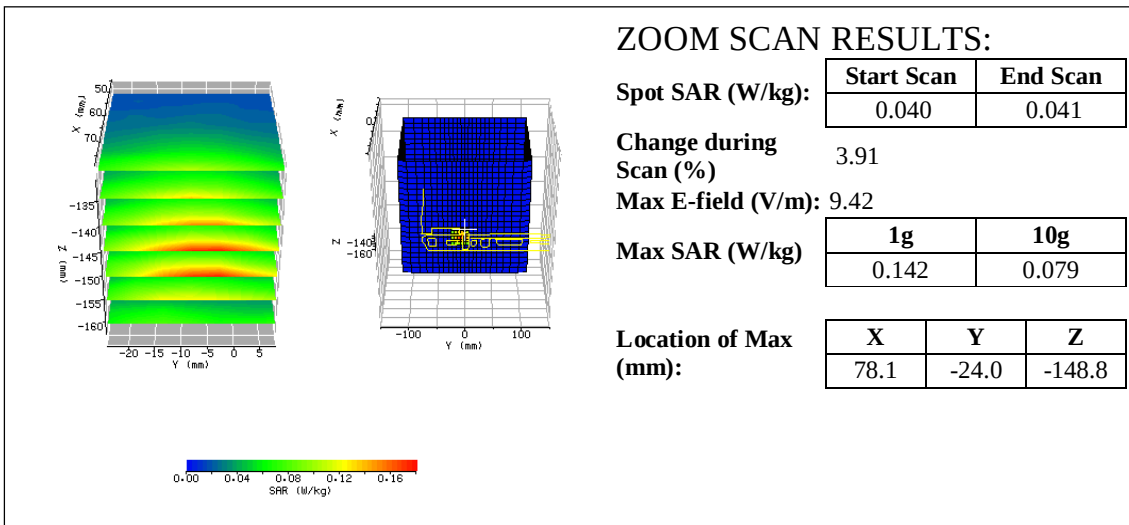


Plot #2 (1/2)

Date:	2005/4/18	Position:	perpendicular to the phantom 0mm
Filename:	per0_11g-ch6.txt	Phantom:	HeadBox2-test.csv
Device Tested:	XG-705A	Head Rotation:	0
Antenna:	PCB printed	Test Frequency:	11g_2437MHz
Shape File:	XG-705A-per..csv	Power Level:	17.65 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.9853
Relative Permittivity:	51.8593
Liquid Temp (deg C):	22
Ambient Temp (deg C):	22
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.33VPM
Crest Factor = 1	

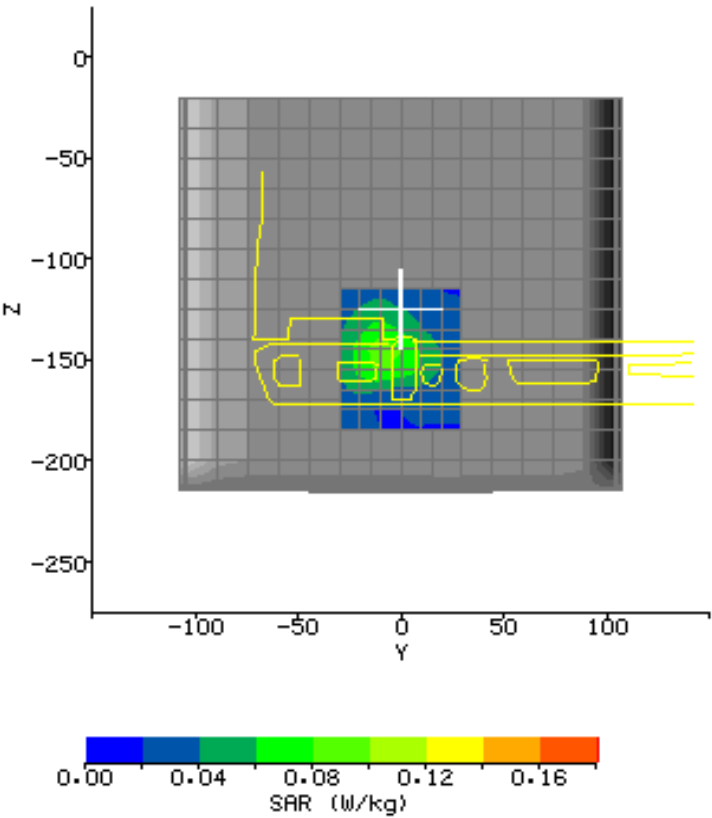


Plot #2 (2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-30.0	30.0	6.0
Z	-185.0	-115.0	7.0

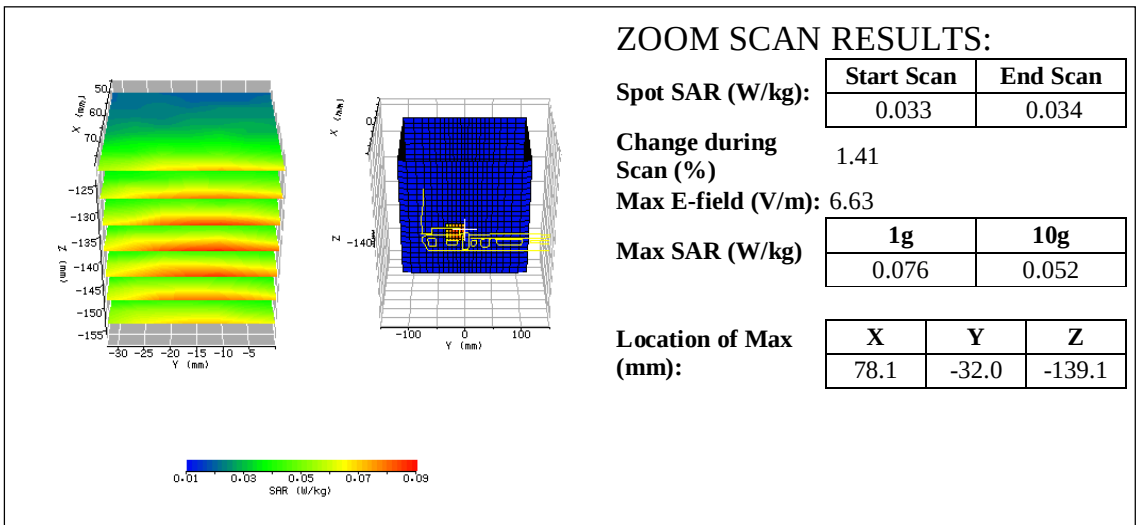


Plot #3 (1/2)

Date:	2005/4/18	Position:	perpendicular to the phantom 15mm
Filename:	per15_11b-ch6.txt	Phantom:	HeadBox2-test.csv
Device Tested:	XG-705A	Head Rotation:	0
Antenna:	PCB printed	Test Frequency:	11b_2437MHz
Shape File:	XG-705A-per..csv	Power Level:	18.32 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.9853
Relative Permittivity:	51.8593
Liquid Temp (deg C):	22
Ambient Temp (deg C):	22
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.33VPM
Crest Factor = 1	

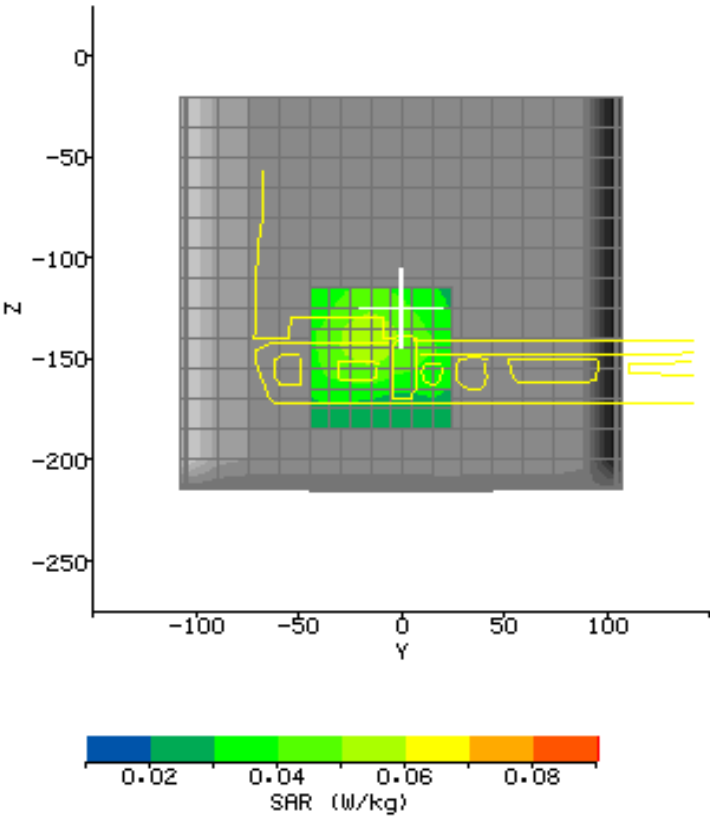


Plot #3 (2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-45.0	25.0	7.0
Z	-185.0	-115.0	7.0

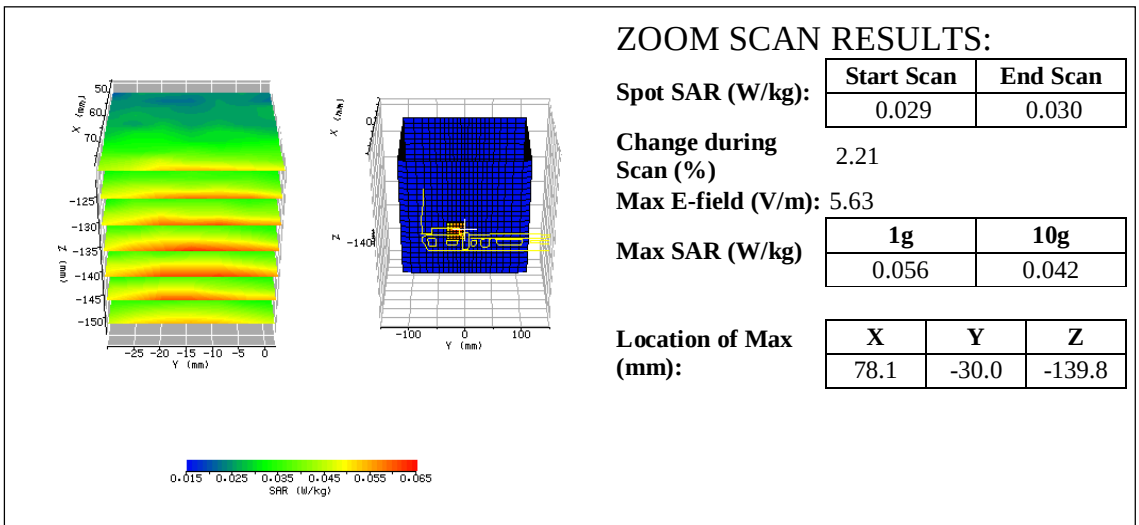


Plot #4 (1/2)

Date:	2005/4/18	Position:	perpendicular to the phantom 15mm
Filename:	per15_11g-ch6.txt	Phantom:	HeadBox2-test.csv
Device Tested:	XG-705A	Head Rotation:	0
Antenna:	PCB printed	Test Frequency:	11g_2437MHz
Shape File:	XG-705A-per..csv	Power Level:	17.65 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.9853
Relative Permittivity:	51.8593
Liquid Temp (deg C):	22
Ambient Temp (deg C):	22
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.33VPM
Crest Factor = 1	

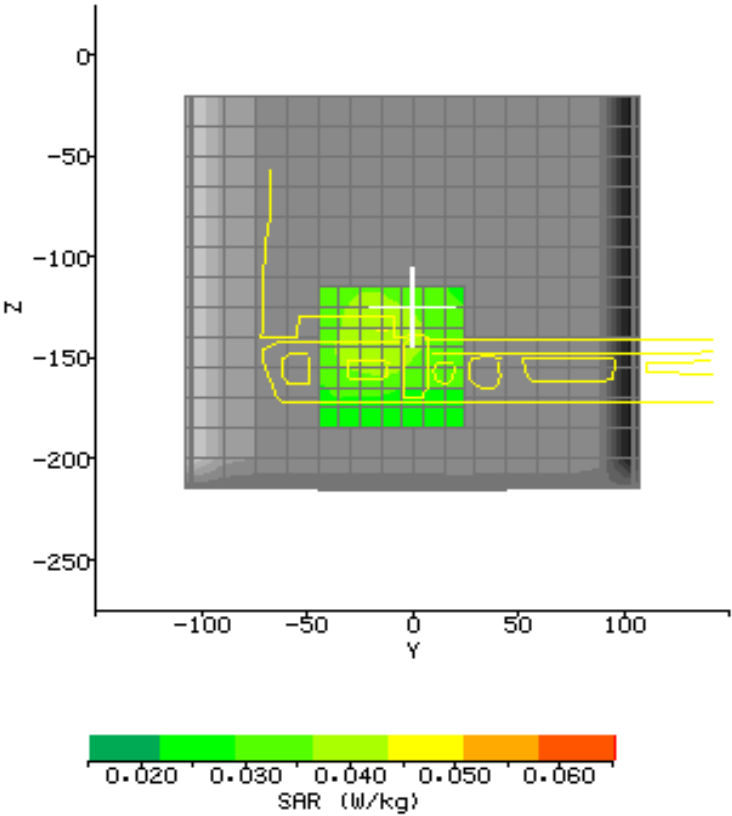


Plot #4 (2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-45.0	25.0	7.0
Z	-185.0	-115.0	7.0

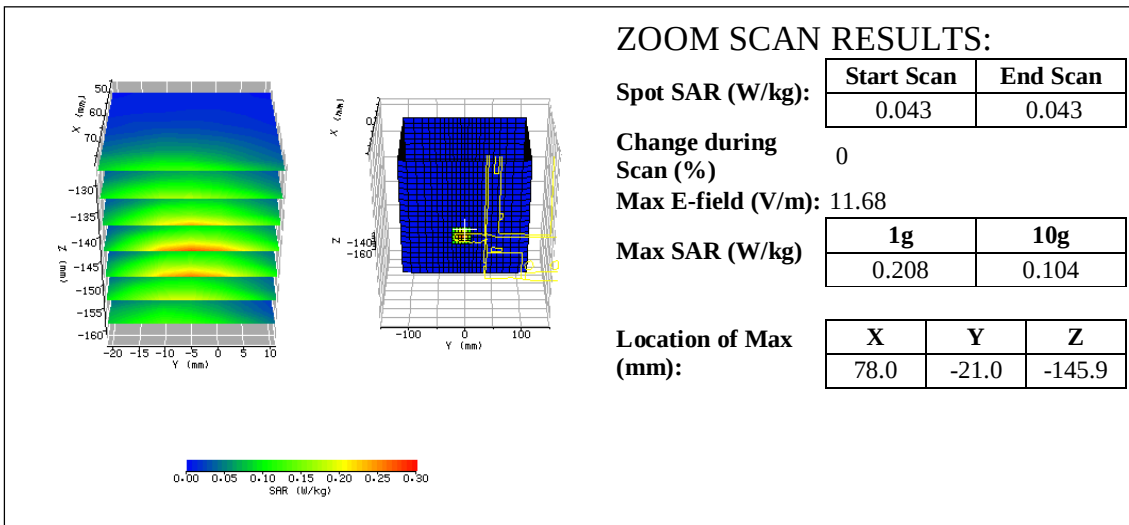


Plot #5 (1/2)

Date:	2005/4/18	Position:	bottom to the phantom 0mm
Filename:	bot0_11b-ch6.txt	Phantom:	HeadBox2-test.csv
Device Tested:	XG-705A	Head Rotation:	0
Antenna:	PCB printed	Test Frequency:	11b_2437MHz
Shape File:	XG-705A-bot..csv	Power Level:	18.32 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.9853
Relative Permittivity:	51.8593
Liquid Temp (deg C):	22
Ambient Temp (deg C):	22
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.33VPM
Crest Factor = 1	

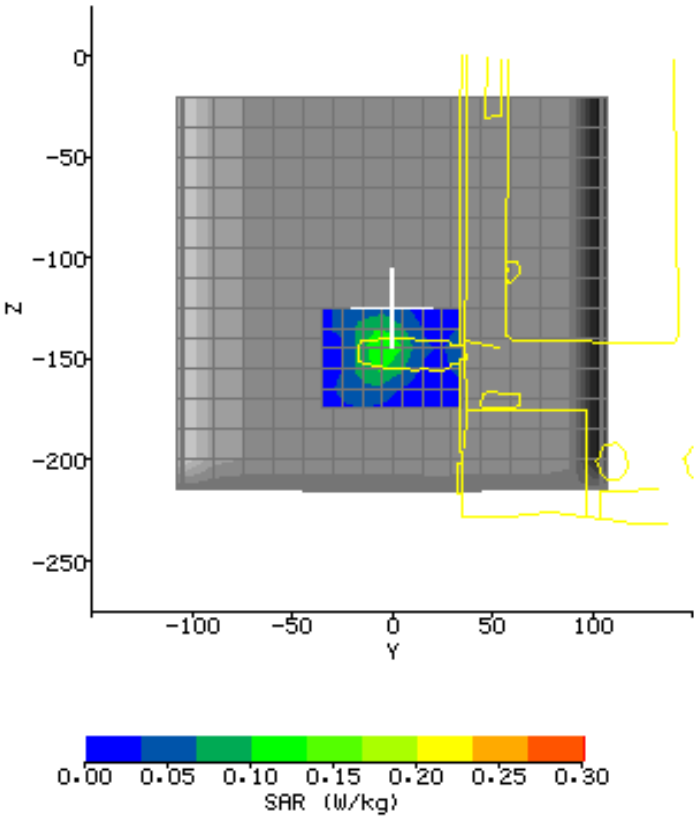


Plot #5 (2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-35.0	35.0	7.0
Z	-175.0	-125.0	5.0

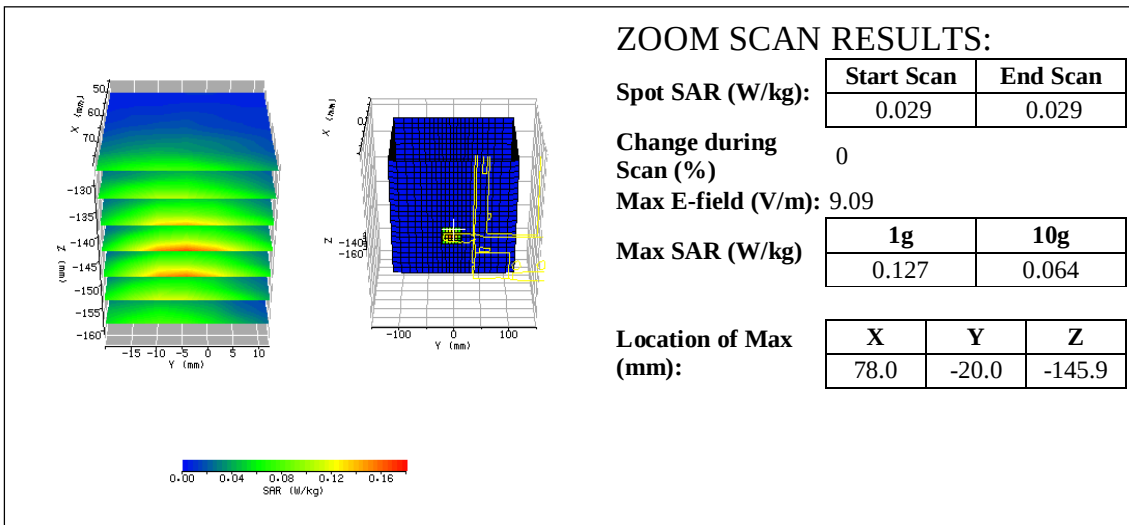


Plot #6 (1/2)

Date:	2005/4/18	Position:	bottom to the phantom 0mm
Filename:	bot0_11g-ch6.txt	Phantom:	HeadBox2-test.csv
Device Tested:	XG-705A	Head Rotation:	0
Antenna:	PCB printed	Test Frequency:	11g_2437MHz
Shape File:	XG-705A-bot..csv	Power Level:	17.65 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

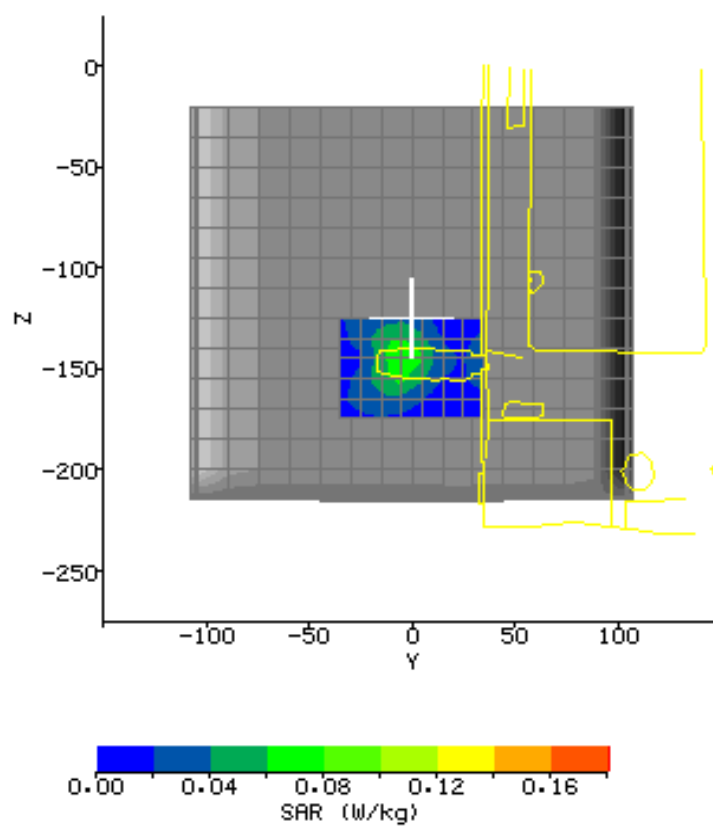
Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.9853
Relative Permittivity:	51.8593
Liquid Temp (deg C):	22
Ambient Temp (deg C):	22
Ambient RH (%):	55
Density (kg/m3):	1000
Software Version:	2.33VPM
Crest Factor = 1	



Plot #6 (2/2)

AREA SCAN:

Scan Extent:		Min	Max	Steps
	Y	-35.0	35.0	7.0
	Z	-175.0	-125.0	5.0



APPENDIX B – Photographs



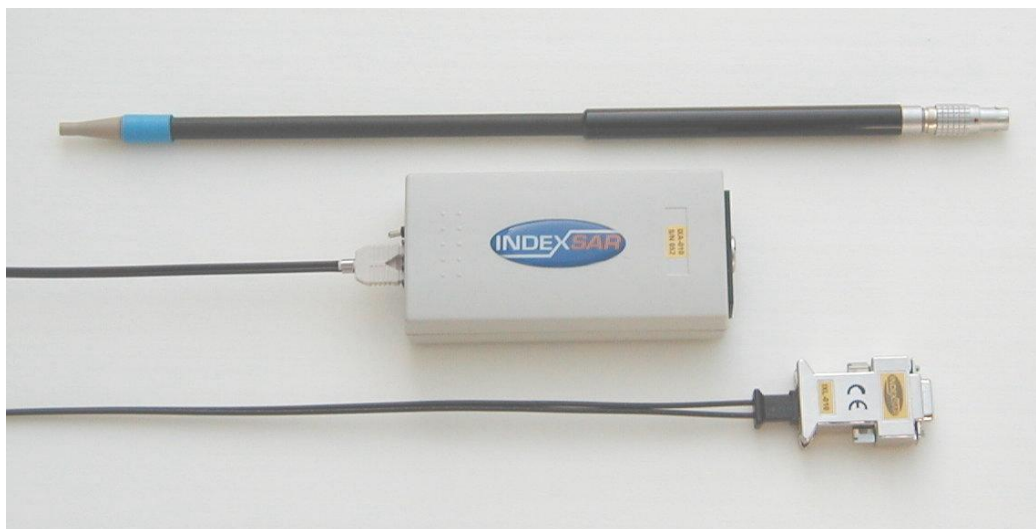
**APPENDIX C - E-Field Probe and 2450MHz Balanced Dipole Antenna
Calibration Data**



**IMMERSIBLE SAR PROBE
CALIBRATION REPORT
Part Number: IXP – 050**

S/N 0149

May 2004



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INTRODUCTION

This Report presents measured calibration data for a particular Indexsar SAR probe (S/N 0149) and describes the procedures used for characterisation and calibration.

Indexsar probes are characterised using procedures that, where applicable, follow the recommendations of CENELEC [1] and IEEE [2] standards. The procedures incorporate techniques for probe linearisation, isotropy assessment and determination of liquid factors (conversion factors). Calibrations are determined by comparing probe readings with analytical computations in canonical test geometries (waveguides) using normalised power inputs.

Each step of the calibration procedure and the equipment used is described in the sections below.

CALIBRATION PROCEDURE

1. Equipment Used

For the first part of the characterisation procedure, the probe is placed in an isotropy measurement jig as pictured in Figure 1. In this position the probe can be rotated about its axis by a non-metallic belt driven by a stepper motor.

The probe is attached via its amplifier and an optical cable to a PC. A schematic representation of the test geometry is illustrated in Figure 2.

A balanced dipole (900 MHz) is inserted horizontally into the bracket attached to a second belt (Figure 1). The dipole can also be rotated about its axis. A cable connects the dipole to a signal generator, via a directional coupler and power meter. The signal generator feeds an RF amplifier at constant power, the output of which is monitored using the power meter. The probe is positioned so that its sensors line up with the rotation center of the source dipole. By recording output voltage measurements of each channel as both the probe and the dipole are rotated, data are obtained from which the spherical isotropy of the probe can be optimised and its magnitude determined.

The calibration process requires E-field measurements to be taken in air, in 900 MHz simulated brain liquid and at other frequencies/liquids as appropriate.

2. Linearising probe output

The probe channel output signals are linearised in the manner set out in Refs [1] and [2]. The following equation is utilized for each channel:

$$U_{lin} = U_{o/p} + U_{o/p}^2 / DCP \quad (1)$$

where U_{lin} is the linearised signal, $U_{o/p}$ is the raw output signal in voltage units and DCP is the diode compression potential in similar voltage units.

DCP is determined from fitting equation (1) to measurements of U_{lin} versus source feed power over the full dynamic range of the probe. The DCP is a characteristic of the schottky diodes used as the sensors. For the IXP-050 probes with CW signals the DCP values are typically 0.10V (or 20 in the voltage units used by Indexsar software, which are $V*200$).

3. Selecting channel sensitivity factors to optimise isotropic response

The basic measurements obtained using the calibration jig (Fig 1) represent the output from each diode sensor as a function of the presentation angle of the source (probe and dipole rotation angles). The directionality of the orthogonally-arranged sensors can be checked by analysing the data using dedicated Indexsar software, which displays the data in 3D format as in Figure 3. The left-hand side of this diagram shows the individual channel outputs after linearisation (see above). The program uses these data to balance the channel outputs and then applies an optimisation process, which makes fine adjustments to the channel factors for optimum isotropic response.

The next stage of the process is to calibrate the Indexsar probe to a W&G EMR300 E-field meter in air. The principal reasons for this are to obtain conversion factors applicable should the probe be used in air and to provide an overall measure of the probe sensitivity.

A multiplier is applied to factors to bring the magnitudes of the average E-field measurements as close as possible to those of the W&G probe.

The following equation is used (where linearised output voltages are in units of $V*200$):

$$E_{air}^2 (V/m) = U_{linx} * Air Factor_x + U_{liny} * Air Factor_y + U_{linz} * Air Factor_z \quad (2)$$

It should be noted that the air factors are not separately used for normal SAR testing. The IXP-050 probes are optimised for use in tissue-simulating liquids and do not behave isotropically in air.

4. 900 MHz Liquid Calibration

Conversion factors for use when the probes are immersed in tissue-simulant liquids at 900 MHz are determined either using a waveguide or by comparison to a reference probe that has been calibrated by NPL. Waveguide procedures are described later. The summary sheet indicates the method used for the probe S/N 0149.

The conversion factor, referred to as the 'liquid factor' is also applied to the measurements of each channel. The following equation is used (where output voltages are in units of $V*200$):

$$E_{liq}^2 (V/m) = U_{linx} * Air Factor_x * Liq Factor_x + U_{liny} * Air Factor_y * Liq Factor_y + U_{linz} * Air Factor_z * Liq Factor_z \quad (3)$$

A 3D representation of the spherical isotropy for probe S/N 0149 using these factors is shown in Figure 3.

The rotational isotropy can also be determined from the calibration jig measurements and is reported as the 900MHz isotropy in the summary table. Note that waveguide measurements can also be used to determine rotational isotropy (Fig. 5).

The design of the cells used for determining probe conversion factors are waveguide cells is shown in Figure 4. The cells consist of a coax to waveguide transition and an open-ended section of waveguide containing a dielectric separator. Each waveguide cell stands in the upright position and is filled with liquid within 10 mm of the open end. The separator provides a liquid seal and is designed for a good electrical transition from air filled guide to liquid filled guide. The choice of cell depends on the portion of the frequency band to be examined and the choice of liquid used. The depth of liquid ensures there is negligible radiation from the waveguide open top and that the probe calibration is not influenced by reflections from nearby objects. The return loss at the coaxial connector of the filled waveguide cell is measured initially using a network analyser and this information is used subsequently in the calibration procedure. The probe is positioned in the centre of the waveguide and is adjusted vertically or rotated using stepper motor arrangements. The signal generator is connected to the waveguide cell and the power is monitored with a coupler and a power meter. A fuller description of the waveguide method is given below.

The liquid dielectric parameters used for the probe calibrations are listed in the Tables below. The final calibration factors for the probe are listed in the summary chart.

WAVEGUIDE MEASUREMENT PROCEDURE

The calibration method is based on setting up a calculable specific absorption rate (SAR) in a vertically-mounted WG8 (R22) waveguide section [1]. The waveguide has an air-filled, launcher section and a liquid-filled section separated by a matching window that is designed to minimise reflections at the liquid interface. A TE_{01} mode is launched into the waveguide by means of a N-type-to-waveguide adapter. The power delivered to the liquid section is calculated from the forward power and reflection coefficient measured at the input to the waveguide. At the centre of the cross-section of the waveguide, the local spot SAR in the liquid as a function of distance from the window is given by functions set out in IEEE1528 as below:

Because of the low cutoff frequency, the field inside the liquid nearly propagates as a TEM wave. The depth of the medium (greater than three penetration depths) ensures that reflections at the upper surface of the liquid are negligible. The power absorbed in the liquid is determined by measuring the waveguide forward and reflected power. Equation (4) shows the relationship between the SAR at the cross-sectional center of the lossy waveguide and the longitudinal distance (z) from the dielectric separator

$$SAR(z) = \frac{4(P_f - P_b)}{r abd} e^{-2z/d} \quad (4)$$

where the density ρ is conventionally assumed to be 1000 kg/m^3 , ab is the cross-sectional area of the waveguide, P_f and P_b are the forward and reflected power inside the lossless section of the waveguide, respectively. The penetration depth d , which is the reciprocal of the waveguide-mode attenuation coefficient, is determined from a scan along the z -axis and compared with the theoretical value determined from Equation (5) using the measured dielectric properties of the lossy liquid.

$$d = \left[\text{Re} \left\{ \sqrt{(p/a)^2 + j\omega m_o (s + j\omega e_o e_r)} \right\} \right]^{-1}. \quad (5)$$

Table A.1 of [1] can be used for designing calibration waveguides with a return loss greater than 30 dB at the most important frequencies used for personal wireless communications. Values for the penetration depth for these specific fixtures and tissue-simulating mixtures are also listed in Table A.1.

According to [1], this calibration technique provides excellent accuracy, with standard uncertainty of less than 3.6% depending on the frequency and medium. The calibration itself is reduced to power measurements traceable to a standard calibration procedure. The practical limitation to the frequency band of 800 to 2500 MHz because of the waveguide size is not severe in the context of compliance testing.

CALIBRATION FACTORS MEASURED FOR PROBE S/N 0149

The probe was calibrated at 900, 1800, 1900 and 2450MHz MHz in liquid samples representing both brain liquid and body fluid at these frequencies. The calibration was for CW signals only, and the axis of the probe was parallel to the direction of propagation of the incident field i.e. end-on to the incident radiation. The axial isotropy of the probe was measured by rotating the probe about its axis in 10 degree steps through 360 degrees in this orientation.

The reference point for the calibration is in the centre of the probe's cross-section at a distance of 2.7 m from the probe tip in the direction of the probe amplifier. A value of 2.7 mm should be used for the tip to sensor offset distance in the software.

It is important that the diode compression point and air factors used in the software are the same as those quoted in the results tables, as these are used to convert the diode output voltages to a SAR value.

DIELECTRIC PROPERTIES OF LIQUIDS

The dielectric properties of the brain and body tissue-simulant liquids employed for calibration are listed in the tables below. The measurements were performed prior to each waveguide test using an Indexsar DiLine measurement kit, which uses the TEM method as recommended in [2].

AMBIENT CONDITIONS

Measurements were made in the open laboratory at $22 \pm 2.0^\circ\text{C}$. The temperature of the liquids in the waveguide used was measured using a mercury thermometer.

RESPONSE TO MODULATED SIGNALS

To measure the response of the probe and amplifier to modulated signals, the probe is held vertically in a liquid-filled waveguide.

An RF amplifier is allowed to warm up and stabilise before use. A spectrum analyser is used to demonstrate that the peak power of the RF amplifier for the CW signals and the pulsed signals are within 0.1dB of each other when the signal generator is switched from CW to modulated output. Subsequently, the power levels recorded are read from a power meter when a CW signal is being transmitted.

The test sequence involves manually stepping the power up in regular (e.g. 2 dB) steps from the lowest power that gives a measurable reading on the SAR probe up to the maximum that the amplifiers can deliver.

At each power level, the individual channel outputs from the SAR probe are recorded at CW and then recorded again with the modulation setting. The results are entered into a spreadsheet. Using the spreadsheets, the modulated power is calculated by applying a factor to the measured CW power (e.g. for GSM, this factor is 9.03dB). This process is repeated 3 times with the response maximised for each channel sensor in turn.

The probe channel output signals are linearised in the manner set out in Section 1 above using equation (1) with the DCPs determined from the linearisation procedure. Calibration factors for the probe are used to determine the E-field values corresponding to the probe readings using equation (3). SAR is determined from the equation

$$\text{SAR (W/kg)} = E_{\text{liq}}^2 \text{ (V/m)} * \sigma \text{ (S/m)} / 1000 \quad (6)$$

Where σ is the conductivity of the simulant liquid employed.

Using the spreadsheet data, the DCP value for linearising each of the individual channels (X, Y and Z) is assessed separately. The corresponding DCP values are listed in the summary page of the calibration factors for each probe.

Figure 7 shows the linearised probe response to GSM signals, Figure 8 the response to GPRS signals (GSM with 2 timeslots) and Figure 9 the response to CDMA IS-95A and W-CDMA signals.

Additional tests have shown that the modulation response is similar at 1800MHz and is not affected by the orientation between the source and the probe.

VPM (Virtual Probe Miniaturisation)

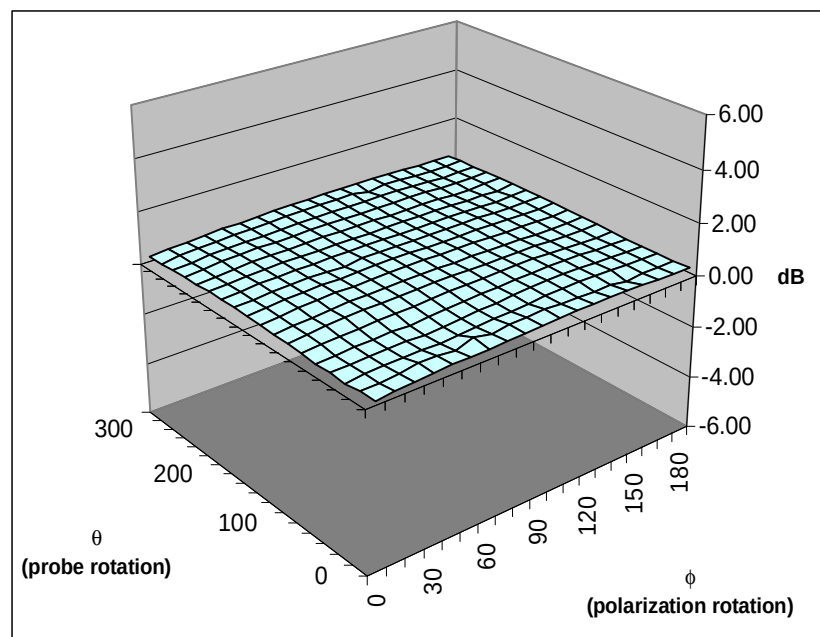
SAR probes with 3 diode-sensors in an orthogonal arrangement are designed to display an isotropic response when exposed to a uniform field. However, the probes are ordinarily used for measurements in non-uniform fields and isotropy is not assured when the field gradients are significant compared to the dimensions of the tip containing the three orthogonally-arranged dipole sensors.

It becomes increasingly important to assess the effects of field gradients on SAR probe readings when higher frequencies are being used. For Indexsar IXP-050 probes, which are of 5mm tip diameter, field gradient effects are minor at GSM frequencies, but are major above 5GHz. Smaller probes are less affected by field gradients and so probes, which are significantly less than 5mm diameter, would be better for applications above 5GHz.

The IndexSAR report IXS0223 describes theoretical and experimental studies to evaluate the issues associated with the use of probes at arbitrary angles to surfaces and field directions. Based upon these studies, the procedures and uncertainty analyses referred to in P1528 are addressed for the full range of probe presentation angles.

In addition, generalized procedures for correcting for the finite size of immersible SAR probes are developed. Use of these procedures enables application of schemes for virtual probe miniaturization (VPM) – allowing probes of a specific size to be used where physically-smaller probes would otherwise be required.

Given the typical dimensions of 3-channel SAR probes presently available, use of the VPM technique extends the satisfactory measurement range to higher frequencies.



Surface Isotropy diagram of IXP-050 Probe S/N 0149 at 900MHz after VPM

Probe tip radius

1.25

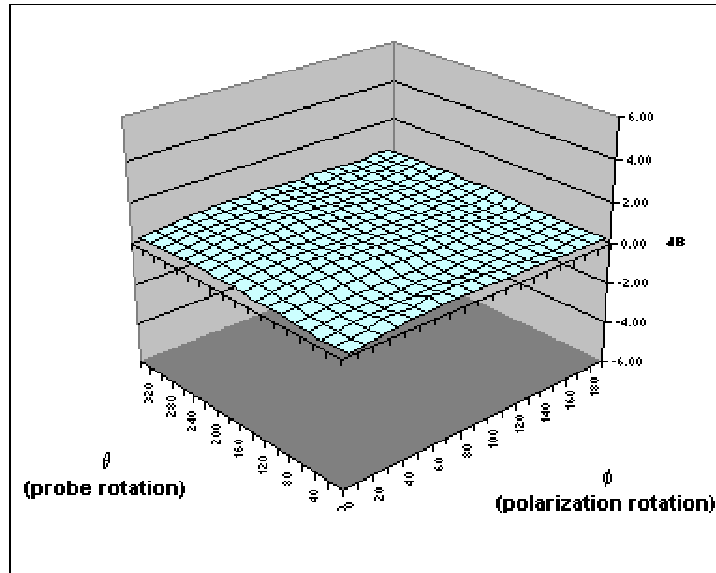
X Ch. Angle to red dot

7

	Head		Body	
Frequency	Bdy. Corr. – f(0)	Bdy. Corr. – d(mm)	Bdy. Corr. – f(0)	Bdy. Corr. – d(mm)
900	0.2	1.0	0.31	2.0
1800	0.2	2.0	0.27	1.6
1900	0.19	1.7	0.3	1.4
2450	0.24	2.0	0.72	2.0

SUMMARY OF CALIBRATION FACTORS FOR PROBE IXP-050 S/N 0149

Spherical isotropy measured at 900 MHz 0.28 (+/-) dB



	X	Y	Z	
Air factors	365	444	414	(V*200)
DCPs	20	20	20	(V*200)
GSM	13.4	9.6	7.9	(V*200)
CDMA	20	20	20	(V*200)

f (MHz)	Axial isotropy (+/- dB)		SAR conversion factors (liq/air)		Notes
	BRAIN	BODY	BRAIN	BODY	
450	0.08	0.07	0.344	0.360	1,2,3
835	0.08	0.07	0.344	0.360	1,2,3
900	0.08	0.07	0.344	0.360	1,2,3
1800	0.10	0.11	0.438	0.477	1,2,3
1900	0.11	0.12	0.441	0.504	1,2,3
2450	0.11	0.11	0.504	0.561	1,2,3

Notes

- 1) Calibrations done at 22C +/- 2C
- 2) Waveguide calibration
- 3) Checked using box-phantom validation test

(the graph shows a simple, spreadsheet representation of surface shown in 3D in Figure 3 below)

PROBE SPECIFICATIONS

Indexsar probe 0149, along with its calibration, is compared with CENELEC and IEEE standards recommendations (Refs [1] and [2]) in the Tables below. A listing of relevant specifications is contained in the tables below:

Dimensions	S/N 0149	CENELEC [1]	IEEE [2]
Overall length (mm)	350		
Tip length (mm)	10		
Body diameter (mm)	12		
Tip diameter (mm)	5.2	8	8
Distance from probe tip to dipole centers (mm)	2.7		

Dynamic range	S/N 0149	CENELEC [1]	IEEE [2]
Minimum (W/kg)	0.01	<0.02	0.01
Maximum (W/kg)	>35	>100	100
N.B. only measured to 35 W/kg			

Linearity of response	S/N 0149	CENELEC [1]	IEEE [2]
Over range 0.01 – 100 W/kg (+/- dB)	0.125	0.50	0.25

Isotropy (measured at 900MHz)	S/N 0149	CENELEC [1]	IEEE [2]
Axial rotation with probe normal to source (+/- dB) at 900, 1800, 1900 and 2450 MHz	0.12 Max (See table above)	0.5	0.25
Spherical isotropy covering all orientations to source (+/- dB)	0.28	1.0	0.50

Construction	Each probe contains three orthogonal dipole sensors arranged on a triangular prism core, protected against static charges by built-in shielding, and covered at the tip by PEEK cylindrical enclosure material. No adhesives are used in the immersed section. Outer case materials are PEEK and heat-shrink sleeving.
Chemical resistance	Tested to be resistant to glycol and alcohol containing simulant liquids but probes should be removed, cleaned and dried when not in use.

REFERENCES

- [1] CENELEC, EN 50361, July 2001. Basic Standard for the measurement of specific absorption rate related to human exposure to electromagnetic fields from mobile phones.
- [2] IEEE 1528, Recommended practice for determining the spatial-peak specific absorption rate (SAR) in the human body due to wireless communications devices: Experimental techniques.

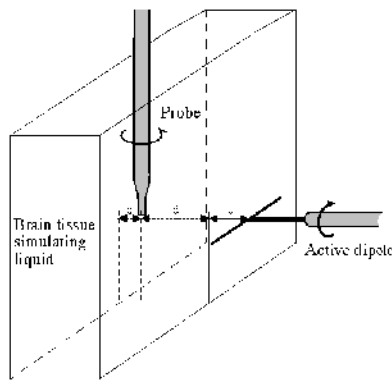
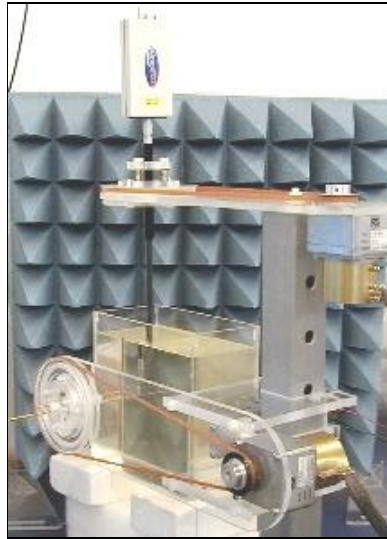


Figure 1. Spherical isotropy jig showing probe, dipole and box filled with simulated brain liquid (see Ref [2], Section A.5.2.1)

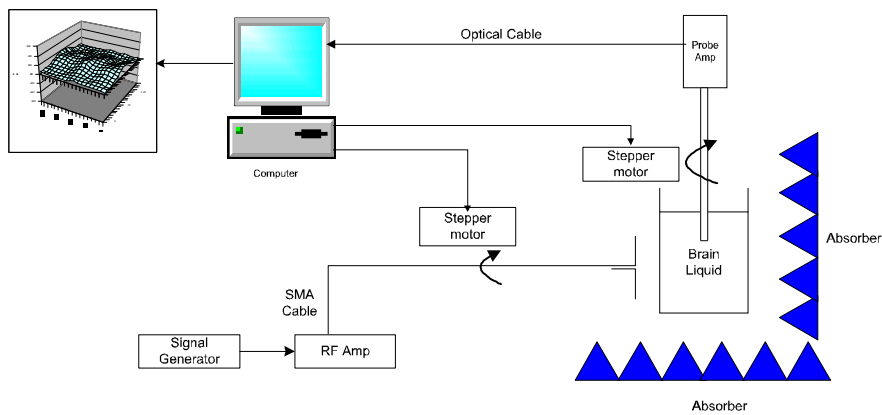


Figure 2. Schematic diagram of the test geometry used for isotropy determination

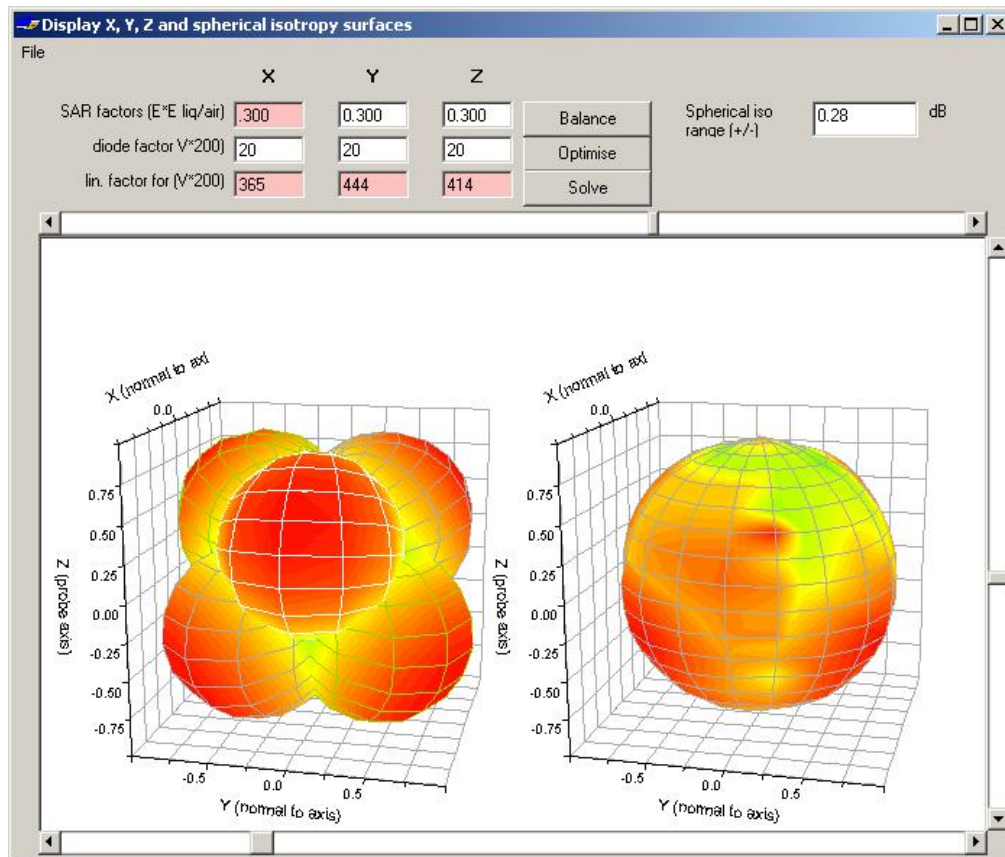


Figure 3. Graphical representation of the probe response to fields applied from each direction. The diagram on the left shows the individual response characteristics of each of the three channels and the diagram on the right shows the resulting probe sensitivity in each direction. The colour range in the figure images the lowest values as blue and the maximum values as red. For the probe S/N 0149, this range is (+/-) 0.28 dB. The probe is more sensitive to fields parallel to the axis and less sensitive to fields normal to the probe axis.

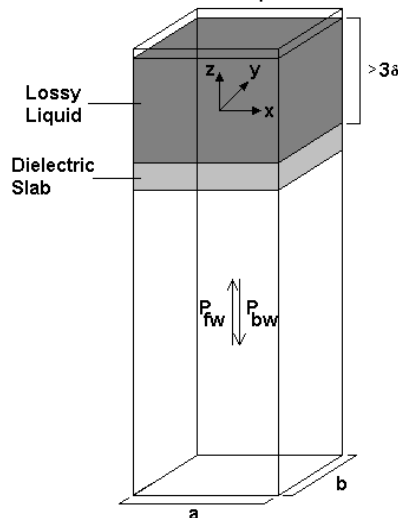


Figure 4. Geometry used for waveguide calibration (after Ref [2]. Section A.3.2.2)

IXP-050 S/N 0149

11-May-04

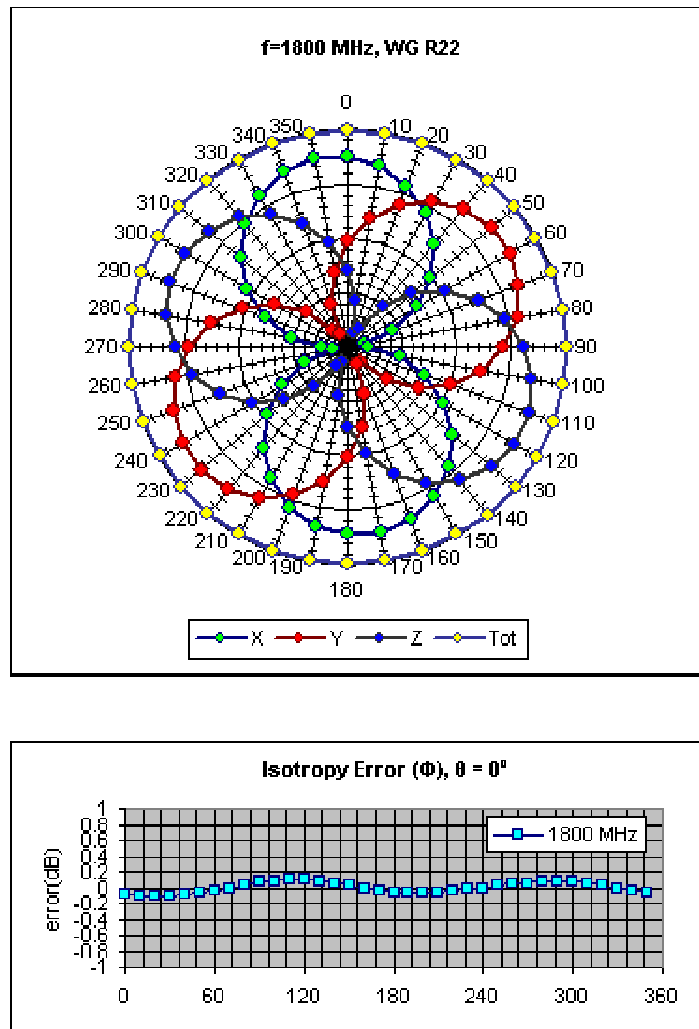


Figure 5. Example of the rotational isotropy of probe S/N 0149 obtained by rotating the probe in a liquid-filled waveguide at 1800 MHz. Similar distributions are obtained at the other test Frequencies (900 and 2450 MHz) both in brain liquids and body fluids (see summary table).

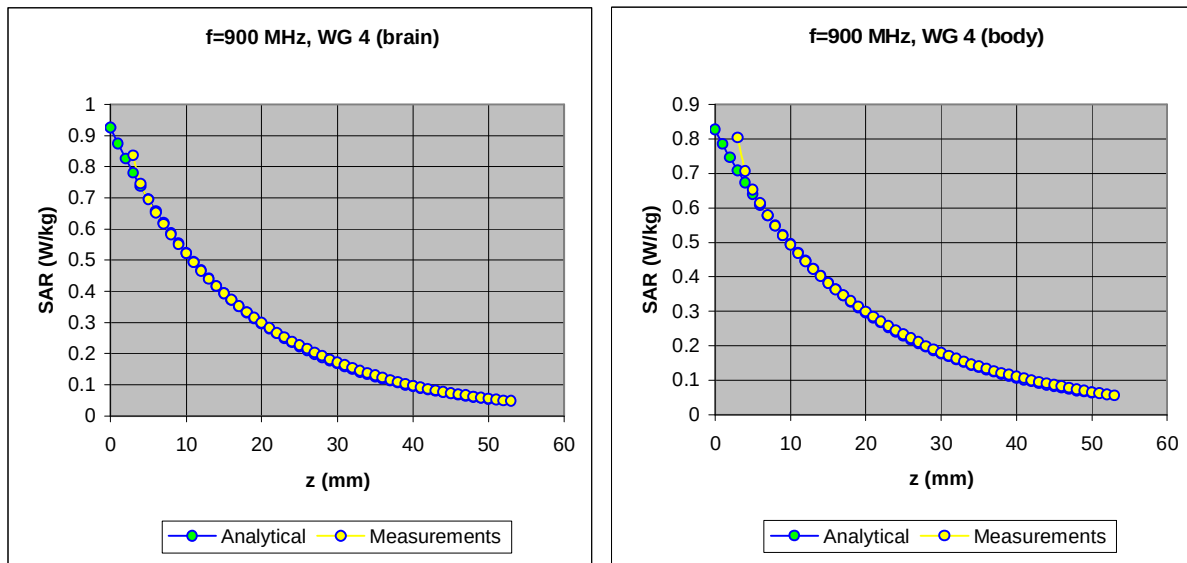
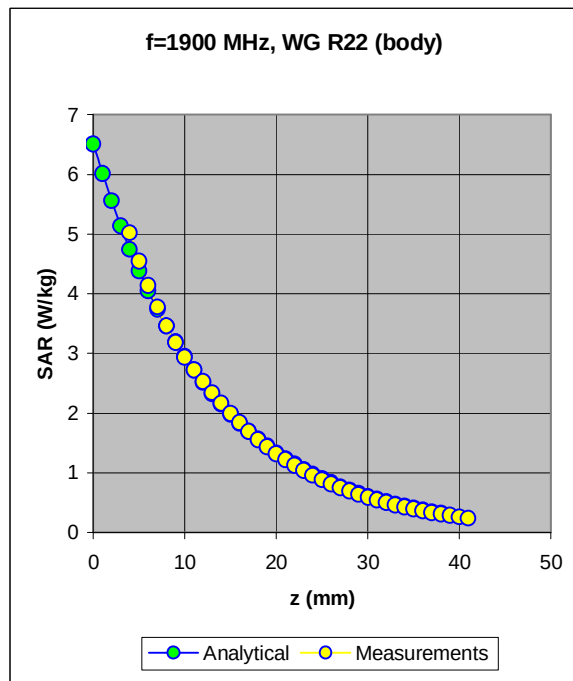
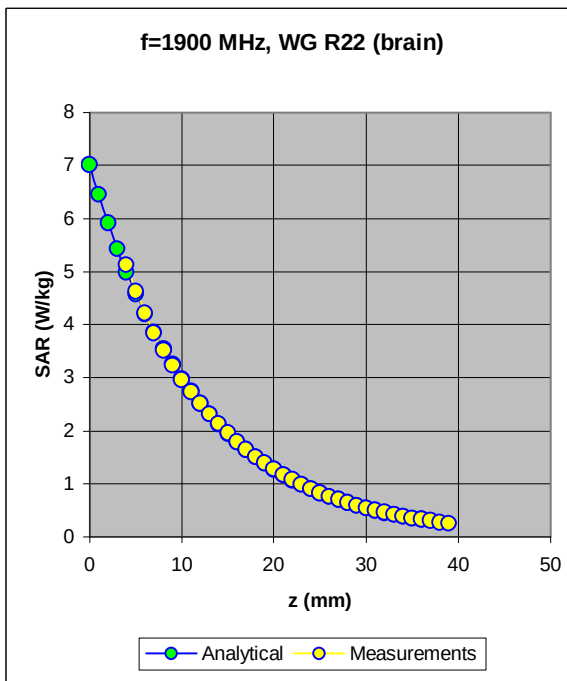
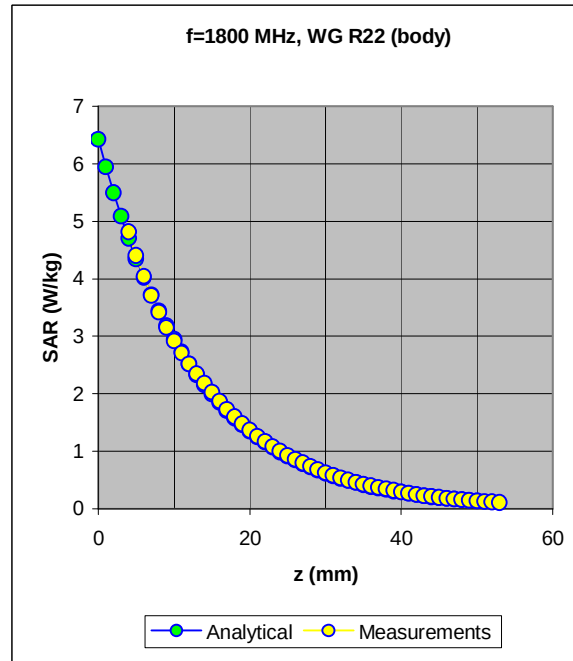
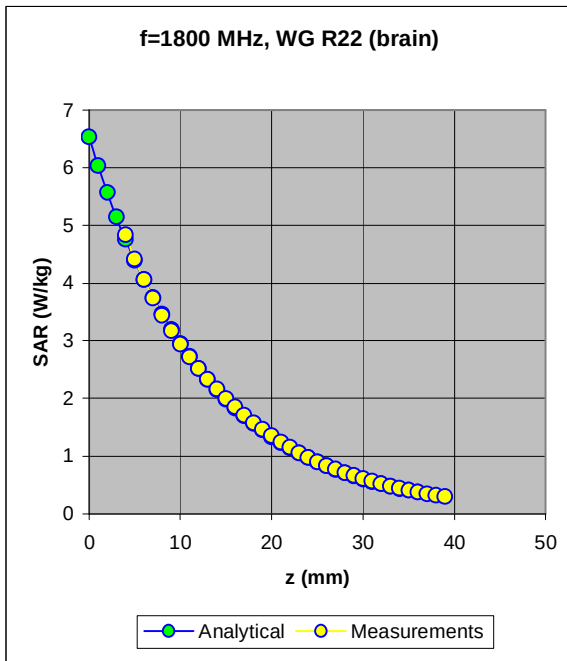


Figure 6. The measured SAR decay function along the centreline of the WG4 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.



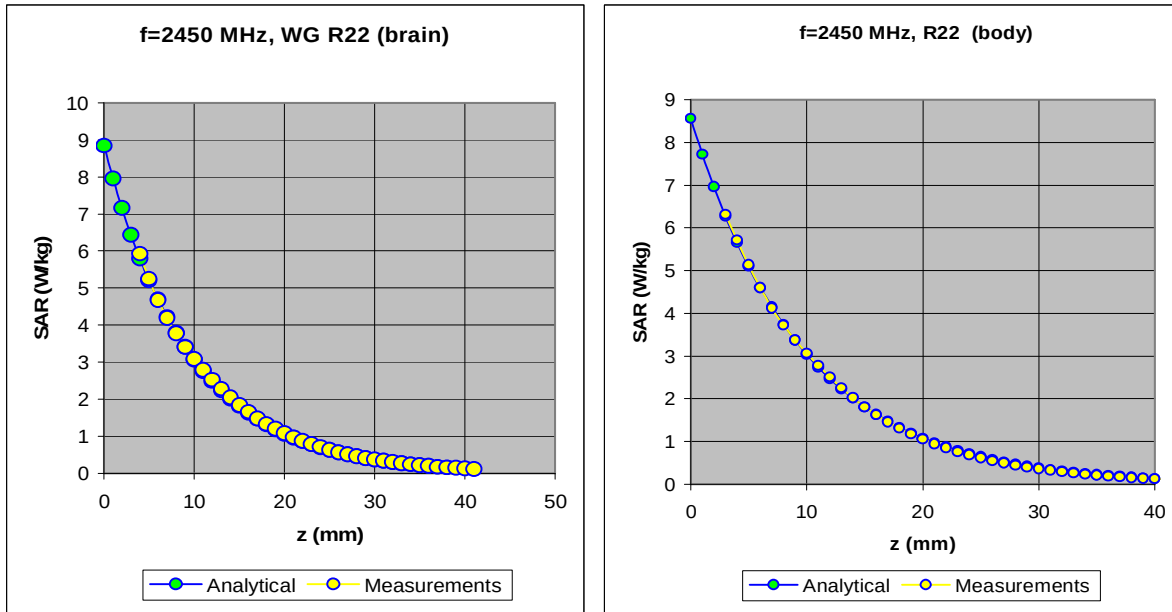


Figure 7. The measured SAR decay function along the centreline of the R22 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.

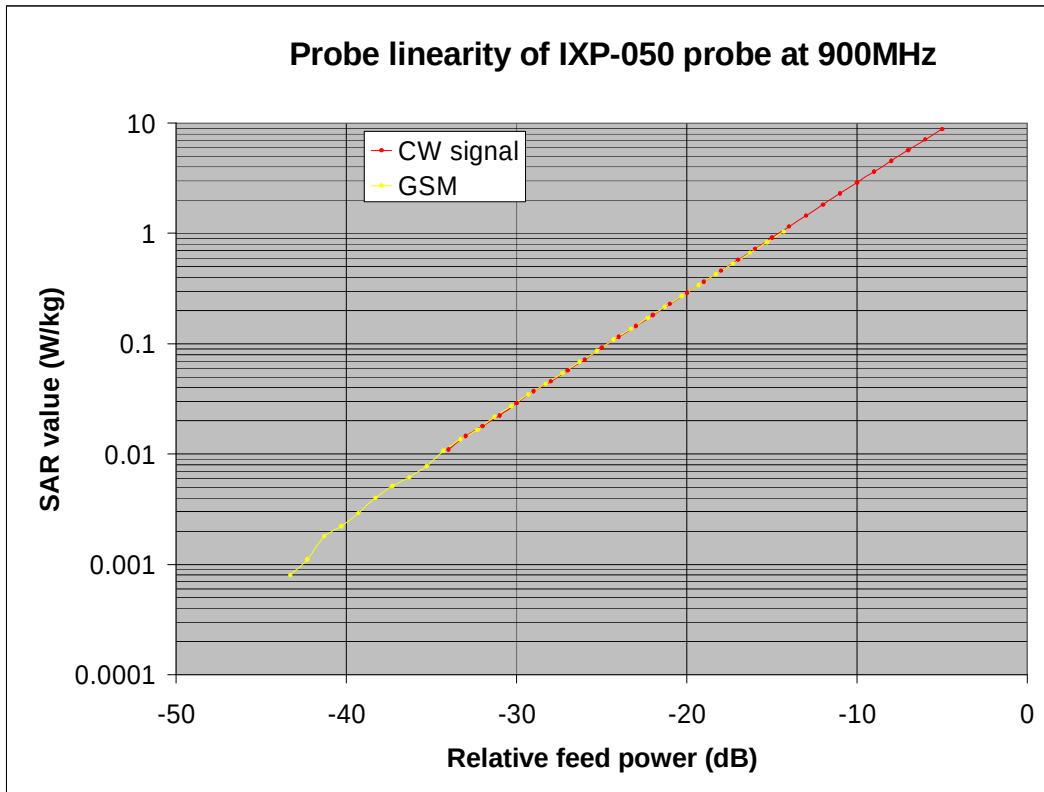


Figure 8. The GSM response of an IXP-050 probe at 900MHz

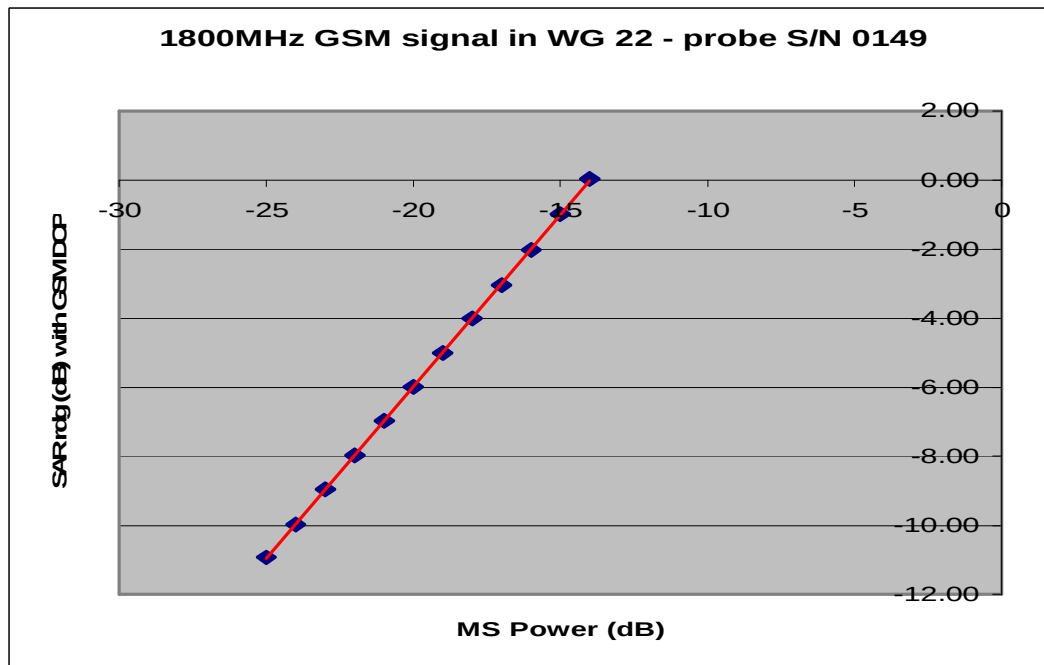


Figure 8a. The actual GSM response of IXP-050 probe S/N 0149 at 1800MHz

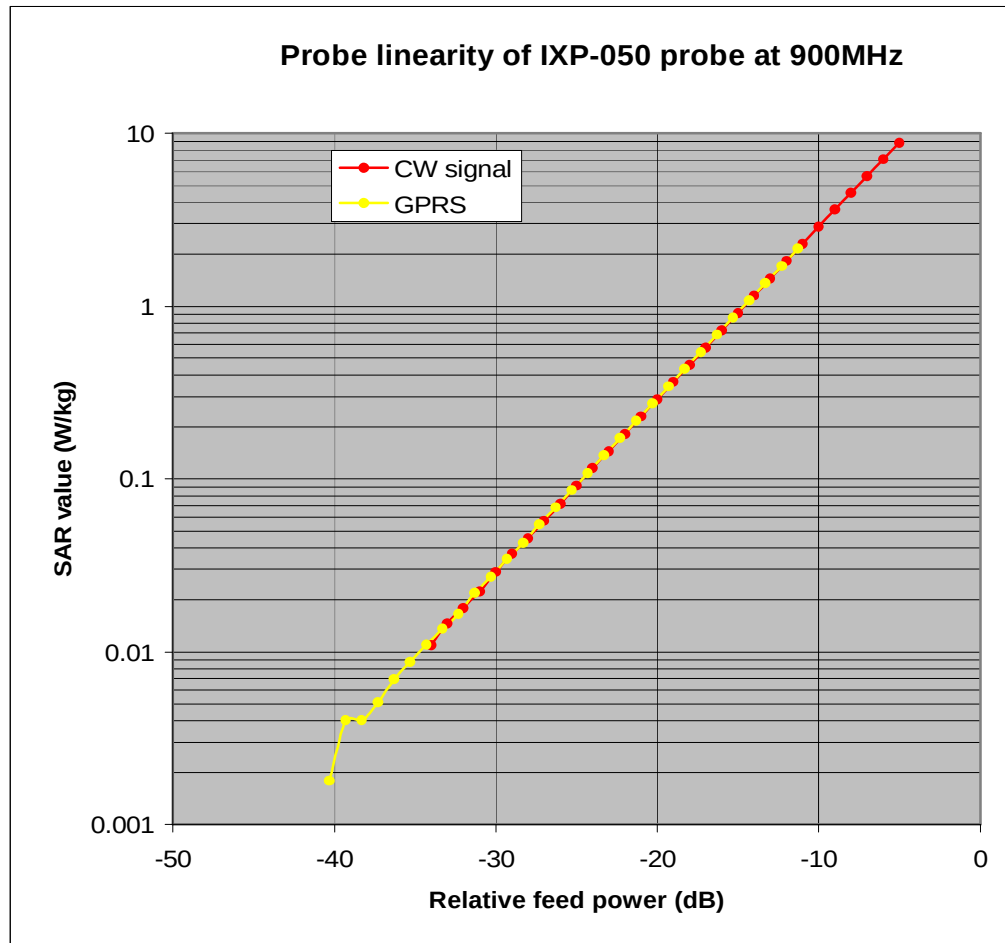


Figure 9. The GPRS response of an IXP-050 probe at 900MHz.

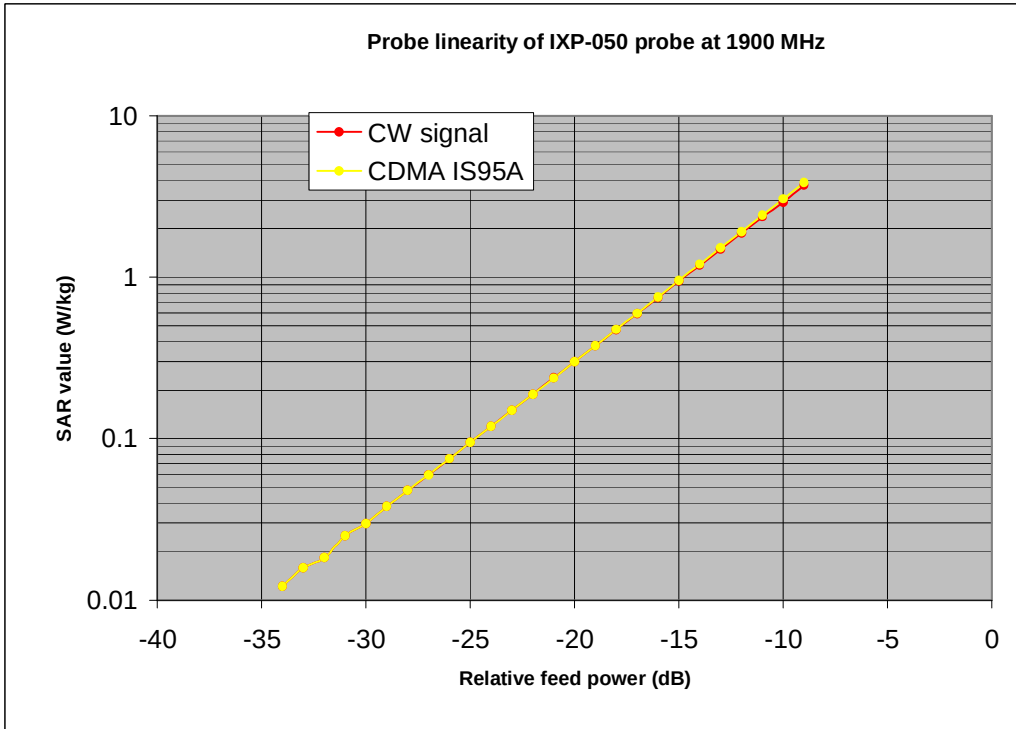
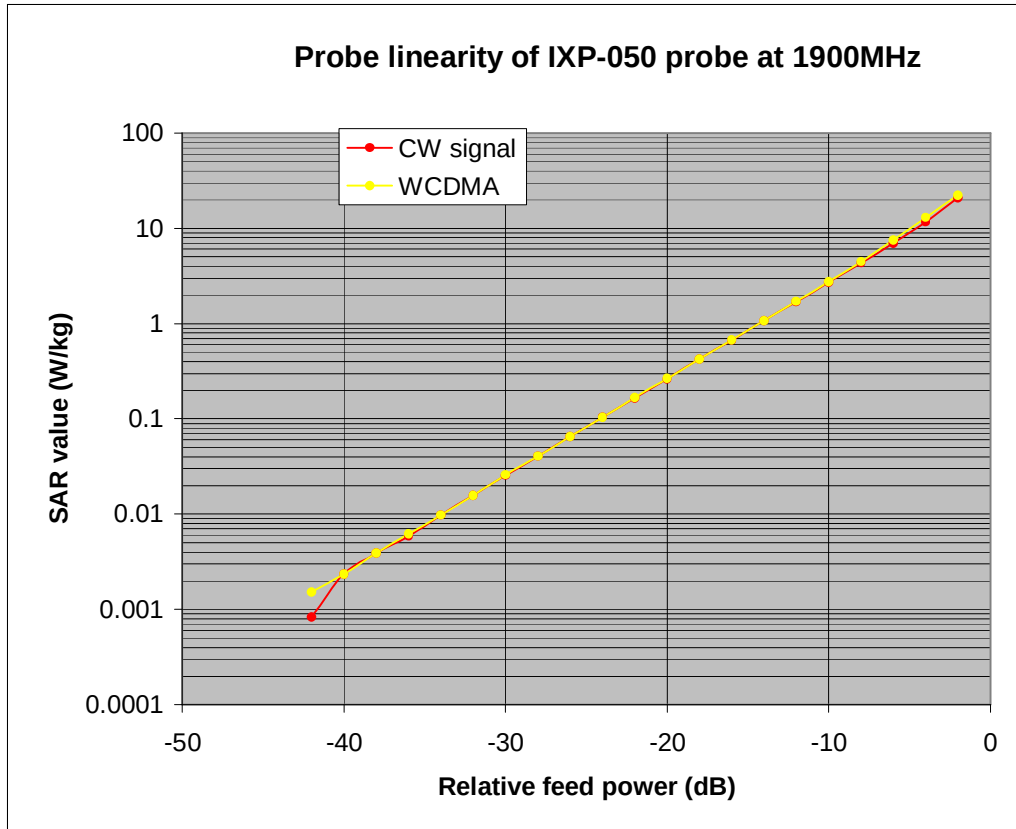


Figure 10. The CDMA response of an IXP-050 probe at 1900MHz.

Table indicating the dielectric parameters of the liquids used for calibrations at each frequency

<i>Liquid used</i>	<i>Relative permittivity (measured)</i>	<i>Conductivity (S/m) (measured)</i>
<i>900 MHz BRAIN</i>	<i>40.92</i>	<i>0.99</i>
<i>900 MHz BODY</i>	<i>57.27</i>	<i>1.045</i>
<i>1800 MHz BRAIN</i>	<i>40.63</i>	<i>1.37</i>
<i>1800 MHz BODY</i>	<i>52.89</i>	<i>1.53</i>
<i>1900 MHz BRAIN</i>	<i>40.33</i>	<i>1.47</i>
<i>1900 MHz BODY</i>	<i>52.84</i>	<i>1.55</i>
<i>2450 MHz BRAIN</i>	<i>40.73</i>	<i>1.82</i>
<i>2450 MHz BODY</i>	<i>54.56</i>	<i>2.04</i>



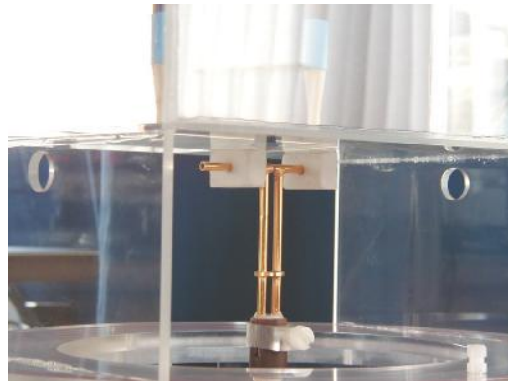
Report No. SN0048_2450

26th March 2003

INDEXSAR
2450MHz validation Dipole
Type IXD-245 S/N 0048

Performance measurements

- *MI Manning*



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e-mail: enquiries@indexsar.com**Calibration / Conformance statement****Balanced Validation dipole**

Type:	IXD-245 2450MHz
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Manufacturer:	IndexSAR, UK
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Serial Number:	0048
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Place of Calibration:	IndexSAR, UK
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IndexSAR Limited hereby declares that the IXD series dipole named above has been checked for conformity to the specifications given in the draft IEEE 1528 and CENELEC En 50361 standards on the date shown below.

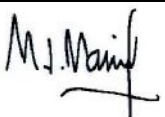
Date of Calibration/Check:	March 2005
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The dipole named above should be periodically re-checked using the procedures set out in the dipole calibration document. It is important that the cautions regarding handling of the dipoles (given in the calibration document) are adhered to.

Next Calibration Date:	March 2007
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The calibration measurements were carried out using the methods described in the calibration document. Where applicable, the standards used in the calibration process are traceable to the UK's National Physical Laboratory.

Calibrated By:	
----------------	---

Approved By:	
--------------	---

1. Tests on Validation Dipole

Tests have been performed on a balanced dipole made for 2450MHz application according to the construction guidelines, dimensions and tolerances given in the draft IEEE1528 standard [1]. Measurements have been made of the impedance and return loss when positioned against the liquid-filled phantom and a validation test has been performed according to the procedures set out in IEEE 1528 [1].

2. Measurement Conditions

Measurements were performed using a box-shaped phantom made of PMMA with dimensions designed to meet the accuracy criteria for reasonably-sized phantoms that do not have liquid capacities substantially in excess of the volume of liquid required to fill the Indexsar upright SAM phantoms used for SAR testing of handsets against the ear.

An HP 8753B vector network analyser was used for the return loss measurements.

The dipole was placed in a special holder made of low-permittivity, low-loss materials. This holder enables the dipole to be positioned accurately in the centre of the base of the Indexsar box-phantom used for flat-surface testing and validation checks.

The validation dipoles are supplied with special spacers made from a low-permittivity, low-loss foam material. These spacers are fitted to the dipole arms to ensure that, when the dipole is offered up to the phantom surface, the spacing between the dipole and the liquid surface is accurately aligned according to the guidance in the relevant standards documentation. The spacers are rectangular with a central hole equal to the dipole arm diameter and dimensioned so that the longer side can be used to ensure a spacing of 15mm from the liquid in the phantom (for tests at 900MHz and below) and the shorter side can be used for tests at 1800MHz and above to ensure a spacing of 10mm from the liquid in the phantom. The spacers are made on a CNC milling machine with an accuracy of 1/40th mm but they may suffer wear and tear and need to be replaced periodically. The material used is Rohacell, which has a relative permittivity of approx. 1.05 and a negligible loss tangent.

The apparatus supplied by Indexsar for dipole validation tests thus includes:

Balanced dipoles for each frequency required are dimensioned according to the guidelines given in IEEE 1528 [1]. The dipoles are made from semi-rigid 50 Ohm co-ax, which is joined by soldering and is gold-plated subsequently. The constructed dipoles are easily deformed, if mis-handled, and periodic checks need to be made of their symmetry.

Rohacell foam spacers designed for presenting the dipoles to 2mm thick PMMA box phantoms. These components also suffer wear and tear and should be replaced when the central hole is a loose-fit on the dipole arms or if the edges are too worn to ensure accurate alignment. The standard spacers are dimensioned for use with 2mm wall thickness (additional spacers are available for 4mm wall thickness).

3. SAR Validation Measurement

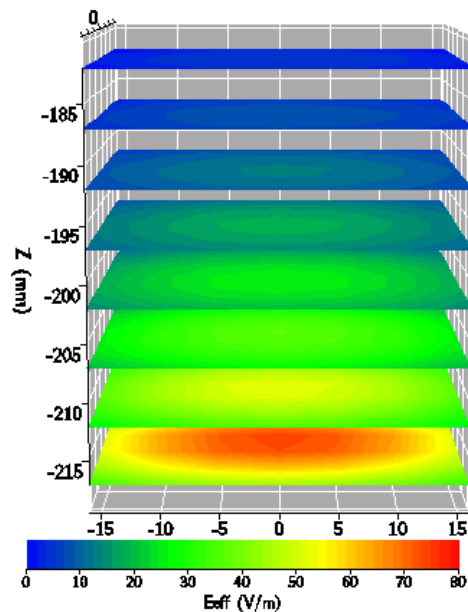
A SAR validation check was performed with the box-phantom located on the SARA2 phantom support base on the SARA2 robot system. Tests were then conducted at a feed power level of approx. 0.25W. The actual power level was recorded and used to normalise the results obtained to the standard input power conditions of 1W (forward power). The ambient temperature was 24°C.

The phantom was filled with a 2450MHz brain liquid using a recipe from [1], which was measured using an Indexsar DiLine kit at 2450MHz. Measurements were taken at 23°C and 30°C and interpolation was used to find the properties at 24°C which were as below:

Relative Permittivity **39.221**
Conductivity **1.8714 S/m**

The SARA2 software version 0.420N was used with an Indexsar probe previously calibrated using waveguide techniques.

The 3D measurement made using the dipole at the bottom of the phantom box is shown below:



The volume-averaged SAR results, normalised to an input power of 1W (forward power) are:

Averaged over 1 cm³ (1g) of tissue **51.376 W/kg**
Averaged over 10cm³ (10g) of tissue **23.888 W/kg**

These results can be compared with Table 8.1 in [1]. The agreement is within 10%.

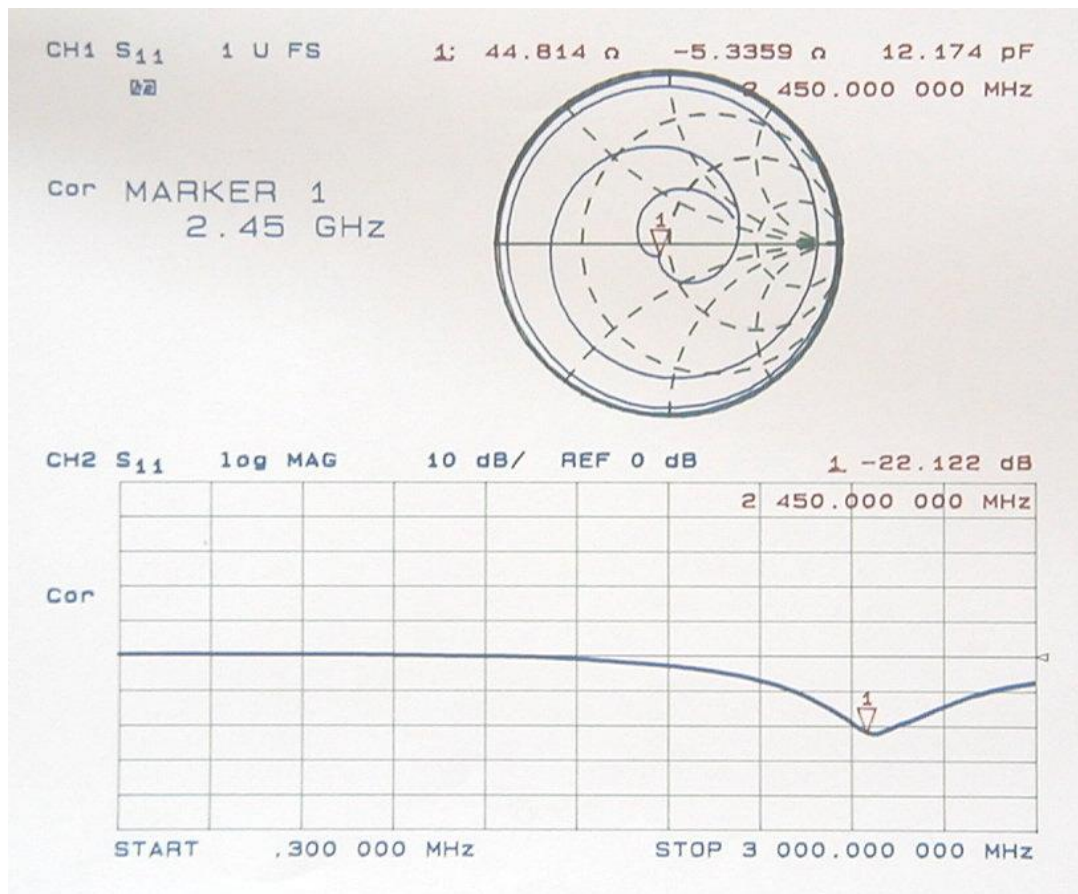
4. Dipole impedance and return loss

The dipoles are designed to have low return loss ONLY when presented against a lossy-phantom at the specified distance. A Vector Network Analyser (VNA) was used to perform a return loss measurement on the specific dipole when in the measurement-location against the box phantom. The distance was as specified in the standard i.e. 10mm from the liquid (for 2450MHz). The Indexsar foam spacers (described above) were used to ensure this condition during measurement.

The impedance was measured at the SMA-connector with the network analyser.
The following parameters were measured:

Dipole impedance at 2450 MHz $\text{Re}\{Z\} = 44.814 \Omega$
 $\text{Im}\{Z\} = -5.3359 \Omega$

Return loss at 2450MHz **-22.122 dB**



5. Dipole handling

The dipoles are made from standard, copper-sheathed coaxial cable. In assembly, the sections are joined using ordinary soft-soldering. This is necessary to avoid excessive heat input in manufacture, which would destroy the polythene dielectric used for the cable. The consequence of the construction material and the assembly technique is that the dipoles are fragile and can be deformed by rough handling. Conversely, they can be straightened quite easily as described in this report.

If a dipole is suspected of being deformed, a normal workshop lathe can be used as an alignment jig to restore the symmetry. To do this, the dipole is first placed in the headstock of the lathe (centred on the plastic or brass spacers) and the headstock is rotated by hand (do NOT use the motor). A marker (lathe tool or similar) is brought up close to the end of one dipole arm and then the headstock is rotated by 0.5 rev. to check the opposing arm. If they are not balanced, judicious deformation of the arms can be used to restore the symmetry.

If a dipole has a failed solder joint, the dipole can be fixed down in such a way that the arms are co-linear and the joint re-soldered with a reasonably-powerful electrical soldering iron. Do not use gas soldering irons. After such a repair, electrical tests must be performed as described below.

Please note that, because of their construction, the dipoles are short-circuited for DC signals.

6. Tuning the dipole

The dipole dimensions are based on calculations that assumed specific liquid dielectric properties. If the liquid dielectric properties are somewhat different, the dipole tuning will also vary. A pragmatic way of accounting for variations in liquid properties is to 'tune' the dipole (by applying minor variations to its effective length). For this purpose, Indexsar can supply short brass tube lengths to extend the length of the dipole and thus 'tune' the dipole. It cannot be made shorter without removing a bit from the arm. An alternative way to tune the dipole is to use copper shielding tape to extend the effective length of the dipole. Do both arms equally.

It should be possible to tune a dipole as described, whilst in place in the measurement position as long as the user has access to a VNA for determining the return loss.

7. Reference

[1] Draft recommended practice for determining the peak spatial-average specific absorption rate (SAR) in the human body due to wireless communications devices: Measurement Techniques. Draft CD1.1 – December 29, 2002.