

Specific Absorption Rate (SAR) Test Report
for
MITAC Technology Corporation
on the
Tablet Personal Computer
(with Intel PRO/Wireless 2200BG Network Connection inside)
Model Number: CA27

Test Report: EME-050081

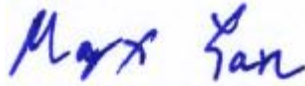
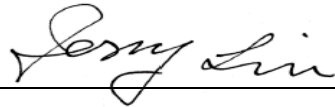
Date of Report: Feb. 3, 2005

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Accredited for testing to FCC Part 15

Tested by: Marx Yan	
Reviewed by: Jerry Liu	

Review Date: Feb. 3, 2005

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STATEMENT OF COMPLIANCE

The MITAC sample device, model # CA27 was evaluated in accordance with the requirements for compliance testing defined in FCC OET Bulletin 65, Supplement C (Edition 01-01). Testing was performed at the Intertek Testing Services facility in Hsinchu, Taiwan.

For the evaluation, the dosimetric assessment system INDEXSAR SARA2 was used. The phantom employed was the box phantom of 2mm thick in one wall. The total uncertainty for the evaluation of the spatial peak SAR values averaged over a cube of 1g tissue mass had been assessed for this system to be $\pm 20.6\%$.

The device was tested at their maximum output power declared by the MITAC.

In summary, the maximum spatial peak SAR value for the sample device averaged over 1g was found to be:

Phantom	Position	SAR _{1g} , W/kg
2mm thick box phantom wall	EUT top side to the phantom, 0 mm separation.	0.809W/kg

In conclusion, the tested Sample device was found to be in compliance with the requirements defined in OET Bulletin 65, Supplement C (Edition 01-01) for body configurations.

1.0 Job Description

1.1 Client Information

The CA27 has been tested at the request of:

Company: MITAC Technology Corporation
4F, No. 1, R&D Road 2, Hsinchu Science-Based
Industrial Park, Hsinchu 300, Taiwan

1.2 Equipment under test (EUT)

Product Descriptions:

Equipment	Tablet Personal Computer (with Intel PRO/Wireless 2200BG Network Connection insied)		
Trade Name	-	Model No:	CA27
FCC ID	MAU015	S/N No.	Not Labeled
Category	Portable	RF Exposure	Uncontrolled Environment
Frequency Band	2412 – 2462 MHz	System	DSSS, OFDM

EUT Antenna Description			
Type	PIFA	Configuration	Fixed
Dimensions	60 x 1.3 mm	Gain	3.26 dBi
Location	No Exposed		

Use of Product : Wireless Data Communication

Manufacturer: MITAC Technology Corporation

Production is planned: [X] Yes, [] No

EUT receive date: Jan. 25, 2005

EUT received condition: Good operating condition prototype

Test start date: Jan. 27, 2005

Test end date: Jan. 27, 2005

1.3 Test plan reference

FCC Rule: Part 2.1093, FCC's OET Bulletin 65, Supplement C (Edition 01-01) and IEEE 1528

1.4 System test configuration

1.4.1 Support equipment & System block diagram

Support Equipment				
Item #	Equipment	Brand	Model No.	S/N
1	N/A	N/A	N/A	N/A



Tx Antenna Position

1.4.2 Test Position

See the photographs as section 2.2

1.4.3 Test Condition

During tests the worst-case data (max RF coupling) was determined with following conditions:

Usage	N/A	Distance between antenna axis at the joint and the liquid surface:	Laptop is touching the Phantom in top side position, separating 0mm and 15mm, separating 15mm in bottom side position.	
Simulating human Head/ Body/Hand	Body	EUT Battery	Device is powered from host computer through battery.	
802.11b Conducted output Power	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
	Low Channel - 1	2412	16.131	16.130
	Mid Channel - 6	2437	15.381	15.382
	High Channel- 11	2462	14.912	14.915
802.11g Conducted output Power	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
	Low Channel - 1	2412	16.537	-
	Mid Channel - 6	2437	15.974	15.979
	High Channel- 11	2462	15.586	-

The spatial peak SAR values were assessed for lowest, middle and highest operating channels, defined by the manufacturer.

The conducted output power was measured before and after the test using a wideband peak power meter.

Run the test program “shortcut to crtu” under Windows OS. The EUT was transmitted continuously during the test.

The EUT contains 802.11b and 802.11g functions. Both 802.11b and 802.11g middle channels were verified, and the worst case was found in 802.11b function. Therefore, the test was performed on low and high channel of 802.11b function and recorded in this report individually.

After verifying the maximum output power, the maximum output power was occurred at 1Mbps data rate in 802.11b function and 6Mbps data rate in 802.11g function.

All the test data were performed under the above transmission rate.

1.5 Modifications required for compliance

Intertek Testing Services implemented no modifications.

1.6 Additions, deviations and exclusions from standards

The phantom employed was the box phantom of 2mm thick in vertical wall.

2.0 SAR Evaluation

2.1 SAR Limits

The following FCC limits for SAR apply to devices operate in General Population/Uncontrolled Exposure environment:

EXPOSURE (General Population/Uncontrolled Exposure environment)	SAR (W/kg)
Average over the whole body	0.08
Spatial Peak (1g)	1.60
Spatial Peak for hands, wrists, feet and ankles (10g)	4.00

2.2 Configuration Photographs

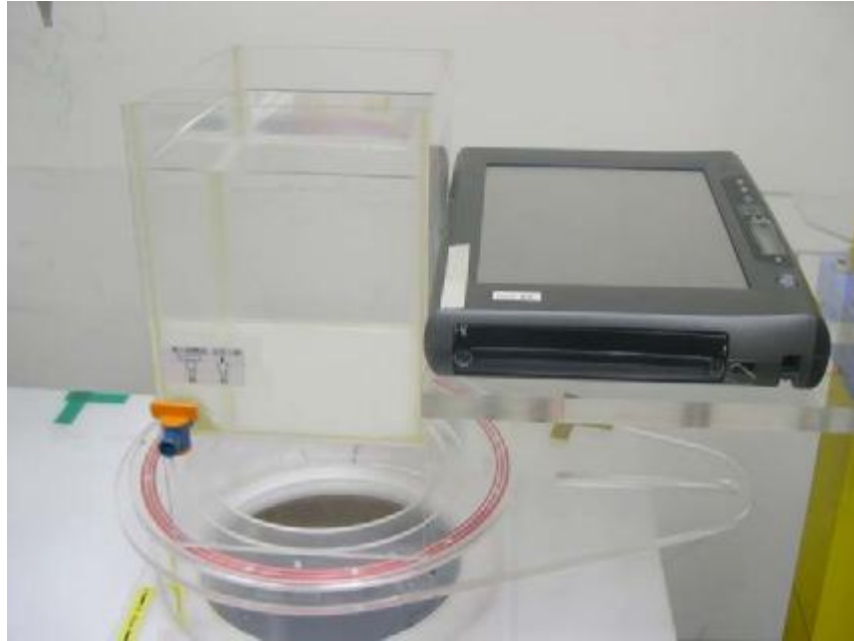
SAR Measurement Test Setup

Test System



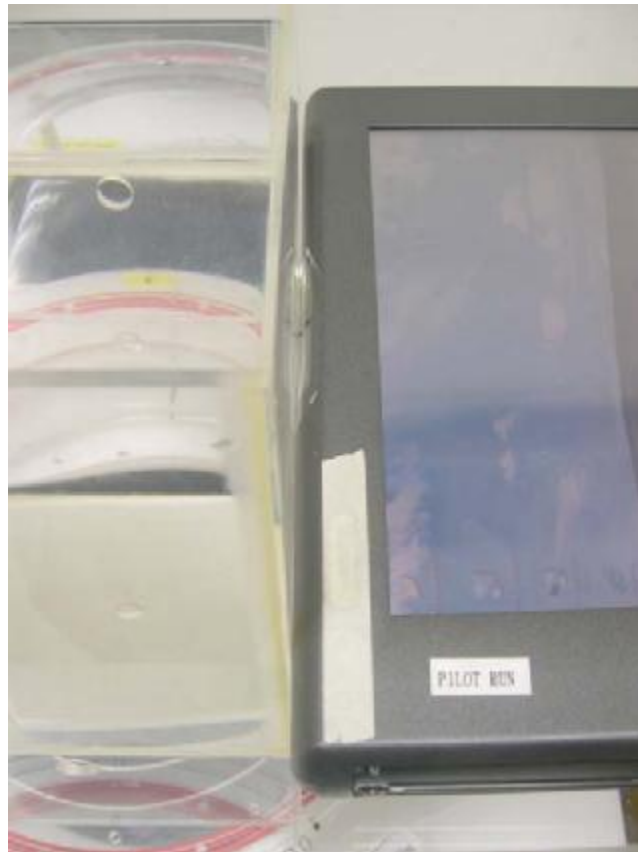
SAR Measurement Test Setup

EUT top side to phantom, 0 mm separation



SAR Measurement Test Setup

EUT top side to phantom, 0 mm separation-Zoon In



SAR Measurement Test Setup

EUT top side to phantom, 15 mm separation



SAR Measurement Test Setup

EUT top side to phantom, 15 mm separation-Zoon In



SAR Measurement Test Setup

EUT bottom to phantom, 0 mm separation



SAR Measurement Test Setup

EUT bottom to phantom, 0 mm separation-Zoon In



2.3 SAR measurement system

Robot system specification

The SAR measurement system being used is the IndexSAR SARA2 system, which consists of a Mitsubishi RV-E2 6-axis robot arm and controller, IndexSAR probe and amplifier and SAM phantom Head Shape. The robot is used to articulate the probe to programmed positions inside the phantom head to obtain the SAR readings from the DUT.

The system is controlled remotely from a PC, which contains the software to control the robot and data acquisition equipment. The software also displays the data obtained from test scans.

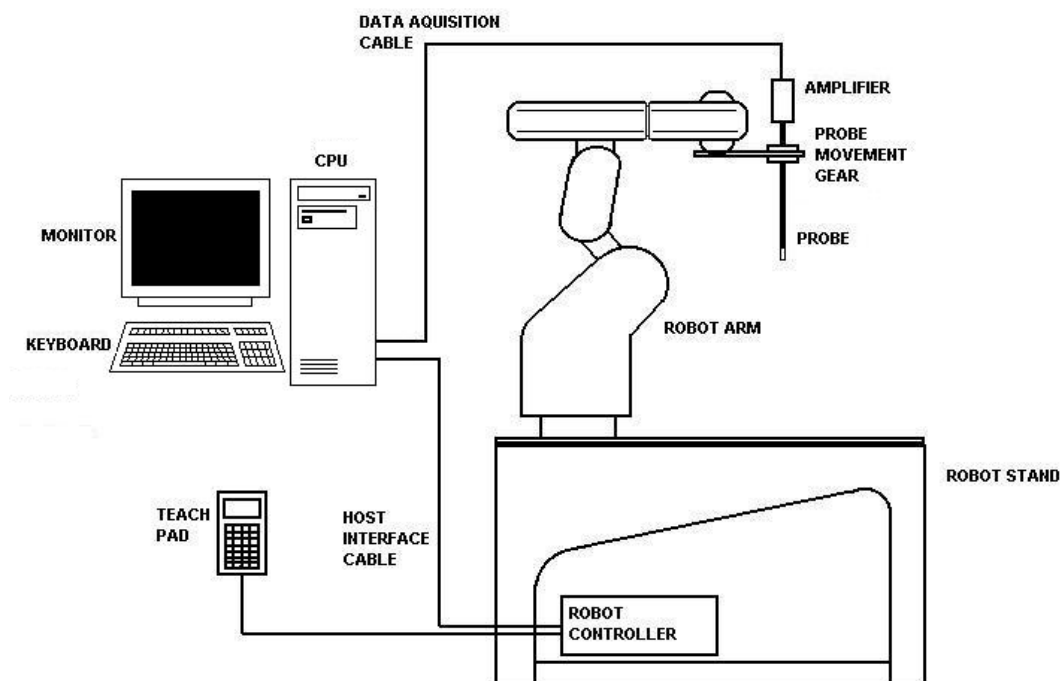


Figure 1: Schematic diagram of the SAR measurement system

The position and digitised shape of the phantom heads are made available to the software for accurate positioning of the probe and reduction of set-up time.

The SAM phantom heads are individually digitised using a Mitutoyo CMM machine to a precision of 0.02mm. The data is then converted into a shape format for the software, providing an accurate description of the phantom shell. In operation, the system first does an area (2D) scan at a fixed depth within the liquid from the inside wall of the phantom. When the maximum SAR point has been found, the system will then carry out a 3D scan centred at that point to determine volume averaged SAR level.

The first 2 measurements points in a direction perpendicular to the surface of the phantom during the zoom scan and closest to the phantom surface, were only 3.5mm and the probe is kept at greater than half a diameter from the surface.

2.4 SAR measurement system validation

Prior to the assessment, the system was verified to the $\pm 10\%$ of the specifications by using the system validation equipments. The validation was performed at 2450 MHz on the bottom side of box phantom.

Procedures

The SAR evaluation was performed with the following procedures:

- a. The SAR distribution was measured at the exposed side of the bottom of the box phantom and was measured at a distance of 8 mm from the inner surface of the shell. The feed power was 1/5 W.
- b. The dimension for this cube is 32 mm x 32 mm x 34 mm was assessed by measuring 5 x 5 x 7 points. On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure:
 - i) The data at the surface were extrapolated, since the center of the dipoles is 2.7 mm away from the tip of the probe and the distance between the surface and the lowest measurement point is 5 mm. The extrapolation was based on a least square algorithm. A polynomial of the fourth order was calculated through the points in Z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.
 - ii) The maximum interpolated value was searched with a straightforward algorithm. Around this maximum, the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3-D spline interpolation algorithm. The 3-D spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y and z directions). The volume was integrated with the trapezoidal algorithm. 1000 points (10 x 10 x 10) were interpolated to calculate the average.
 - iii) All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

The test scan procedure for system validation also apply to the general scan procedure except for the set-up position. For general scan, the EUT was placed at the side of phantom. For validation scan, the dipole antenna was placed at the bottom of phantom

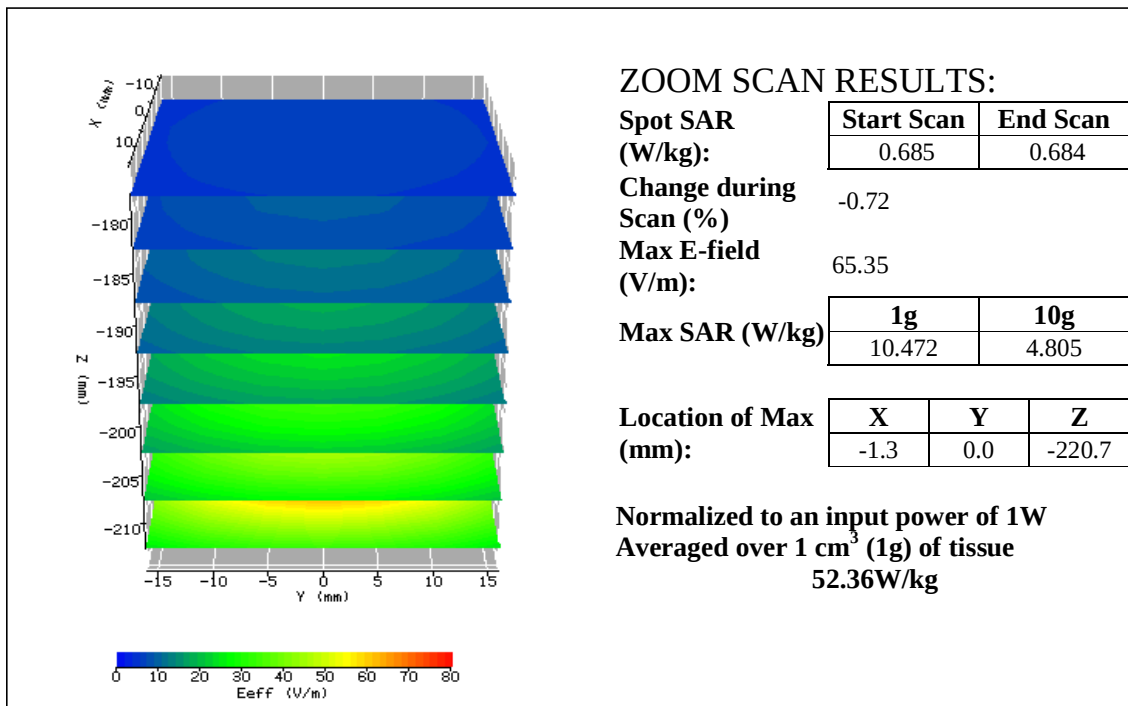
2.4.1 System Validation result

System Validation (2450 MHz Head)				
Frequency MHz	Operating Mode	Target SAR _{1g} (W/kg)	Measured SAR _{1g} (W/kg)	Deviation (±10%)
2450	CW	52.4	54.688	4.37%

Please see the plot below:

Date:	2004/10/1	Position:	Bottom
Filename:	2450val10-15.txt	Phantom:	Box1.csv
Device Tested:	SARA2 system	Head Rotation:	0
Antenna:	2450dipole	Test Frequency:	2450MHz
Shape File:	none.csv	Power Level:	23dBm /CW

Probe:	0149	Liquid:	15.5cm
Cal File:	SN0149_2450_CW_HEAD	Type:	2450MHz Head
Cal Factors:		Conductivity:	1.804
	Air	Relative Permittivity:	38.122
	DCP	Liquid Temp (deg C):	23.3
	Lin	Ambient Temp (deg C):	23
Amp Gain:	2	Ambient RH (%):	50
Averaging:	1	Density (kg/m3):	1000
Batteries	-	Software Version:	2.3VPM
Replaced:	-	Crest Factor = 1	



2.4.2 System Performance Check result

System performance check (2450 MHz Head)				
Frequency MHz	Operating Mode	Target SAR _{1g} (W/kg)	Measured SAR _{1g} (W/kg)	Deviation (±10%)
2450	CW	52.4	48.955	-6.57%

Please see the plot below:

Date:	2005/1/26	Position:	Bottom of phantom box
Filename:	2450performance check 050125-200mW.txt	Phantom:	HeadBox1-val.csv
Device Tested:	2450 MHz performance check	Head Rotation:	0
Antenna:	2450 Dipole antenna	Test Frequency:	2450 MHz
Shape File:	none.csv	Power Level:	23 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_HEAD			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.504	.504	.504
Amp Gain:	2			
Averaging:	1			
Batteries	-			
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz head
Conductivity:	1.828
Relative Permittivity:	39.931
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1

The figure displays a 3D visualization of the electric field (E-field) distribution within a rectangular phantom. The vertical axis represents the Z-position in millimeters (mm), ranging from -15 at the top to -210 at the bottom. The horizontal axes represent the X and Y positions in millimeters (mm), both ranging from -15 to 15. A color bar at the bottom indicates the E-field intensity in Volts per meter (V/m), with a scale from 0 (blue) to 70 (red). The plot shows a color gradient from blue at the top to red at the bottom, indicating increasing E-field intensity with depth. The highest intensity is concentrated in the lower right portion of the phantom.

ZOOM SCAN RESULTS:

Spot SAR

(W/kg):

Start Scan

0.613

End Scan

0.619

Change during

0.91

Scan (%)

Max E-field

62.81

(V/m):

Max SAR (W/kg)

1g

9.791

10g

4.581

Location of Max

(mm):

X

0.0

Y

1.3

Z

-221.7

Normalized to an input power of 1W

Averaged over 1 cm³ (10g) of tissue

48.955W/kg

2.5 Test Result

The results on the following page(s) were obtained when the device was tested in the condition described in this report. Detailed measurement data and plots, which reveal information about the location of the maximum SAR with respect to the device, are reported in Appendix A.

Measurement Results

Trade Name:	-	Model No.:	CA27
Serial No.:	Not Labeled	Test Engineer:	Marx Yan
TEST CONDITIONS			
Ambient Temperature	23.5 °C	Relative Humidity	50.2 %
Test Signal Source	Test Mode	Signal Modulation	DSSS, OFDM
Output Power Before SAR Test	See page 6	Output Power After SAR Test	See page 6
Test Duration	23 min. each scan	Number of Battery Change	1

EUT Position						
Channel (MHz)	Operating Mode	Crest Factor	Description	Distance (mm)	Measured SAR_{1g} (W/kg)	Plot Number
2437	OFDM	1	Top side to phantom	0	0.221	1
2437	DSSS	1	Top side to phantom	0	0.809	2
2412	DSSS	1	Top side to phantom	0	0.561	3
2462	DSSS	1	Top side to phantom	0	0.645	4
2437	OFDM	1	Top side to phantom	15	0.008	5
2437	DSSS	1	Top side to phantom	15	0.029	6
2437	OFDM	1	Bottom to phantom	0	0.134	7
2437	DSSS	1	Bottom to phantom	0	0.576	8

Note 1: Configuration at middle channel with more than -3dB of applicable limit.

3.0 Test Equipment

3.1 Equipment List

The Specific Absorption Rate (SAR) tests were performed with the INDEXSAR SARA2 SYSTEM.

The following major equipment/components were used for the SAR evaluations:

SAR Measurement System			
EQUIPMENT	SPECIFICATIONS	S/N #	LAST CAL. DATE
Balanced Validation dipole	2450MHz	EC381-4	03/26/2003
Controller	Mitsubishi CR-E116	EP320-1	N/A
Robot	Mitsubishi RV-E2	EP320-2	N/A
	Repeatability: $\pm 0.04\text{mm}$; Number of Axes: 6		
E-Field Probe	IXP-050	EC356	05/2004
	Frequency Range: Probe outer diameter: 5.2 mm; Length: 350 mm; Distance between the probe tip and the dipole center: 2.7 mm		
Data Acquisition	SARA2	N/A	N/A
	Processor: Pentium 4; Clock speed: 1.5GHz; OS: Windows XP; I/O: two RS232; Software: SARA2 ver. 2.3VPM (Virtual Probe Minaturisation)		
Phantom	2mm wall thickness box phantom	N/A	N/A
	Shell Material: clear Perspex; Thickness: $2 \pm 0.1\text{ mm}$; Capacity: $152.5 \times 225.5 \times 200\text{ (W x L x D) mm}^3$; Dielectric constant: less than 2.85 above 500MHz;		
Device holder	Material: clear Perspex; Dielectric constant: less than 2.85 above 500MHz	N/A	N/A
Simulated Tissue	Mixture	N/A	01/26/2005
	Please see section 3.2 for details		
RF Power Meter	Boonton 4231A with 51011-EMC power sensor	EC359	03/22/2004
	Frequency Range: 0.03 to 8 GHz, <24dBm		
Vector Network Analyzer	HP 8753B HP 85046A	EC375	08/19/2004
	Frequency Range: 300k to 3GHz		
Signal Generator	R&S SMR27	EC354	08/19/2004
	Frequency Range: 10M to 27GHz, <120dBuV		
Wideband Peak Power Meter/ Sensor	Anritsu ML2497A with MA2491A Power sensor	EC396	10/18/2004
	Frequency Range: 100MHz~18GHz		

3.2 Tissue Simulating Liquid

The head and body tissue parameters should be used to test operating frequency band of transmitters. When a transmission band overlaps with one of the target frequencies, the tissue dielectric parameters of the tissue medium at the middle of a device transmission band should be within $\pm 5\%$ of the parameters specified at that target frequency.

3.2.1 Body Tissue Simulating Liquid for evaluation test

Body Ingredients Frequency (2.45 GHz)	
DGBE (Dilethylene Glycol Butyl Ether)	26.7%
Salt	0.04%
Water	73.2%

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e _r / Relative Permittivity			s / Conductivity (mho/m)			r *(kg/m ³)
		measured	target	△(±5%)	measured	target	△(±5%)	
2450	23.4	50.72	52.7	-3.8%	1.89	1.95	3.08%	1000

* Worst-case assumption

3.2.2 Head Tissue Simulating Liquid for System performance Check test

Head Ingredients Frequency (2.45 GHz)	
DGBE (Dilethylene Glycol Butyl Ether)	53.3%
Water	46.7%

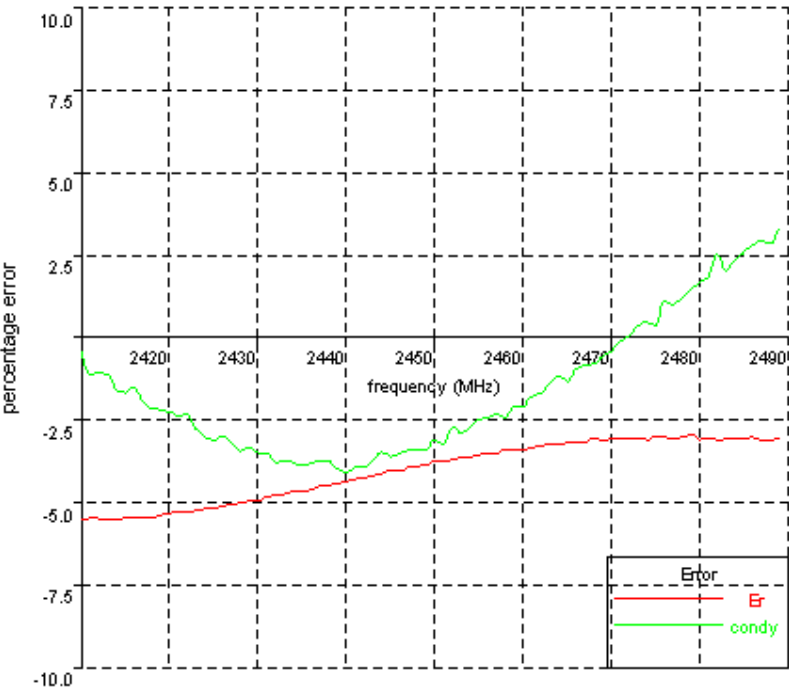
The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e _r / Relative Permittivity			s / Conductivity (mho/m)			r *(kg/m ³)
		measured	target	△(±5%)	measured	target	△(±5%)	
2450	23.6	39.93	39.2	1.86%	1.83	1.80	1.67%	1000

* Worst-case assumption

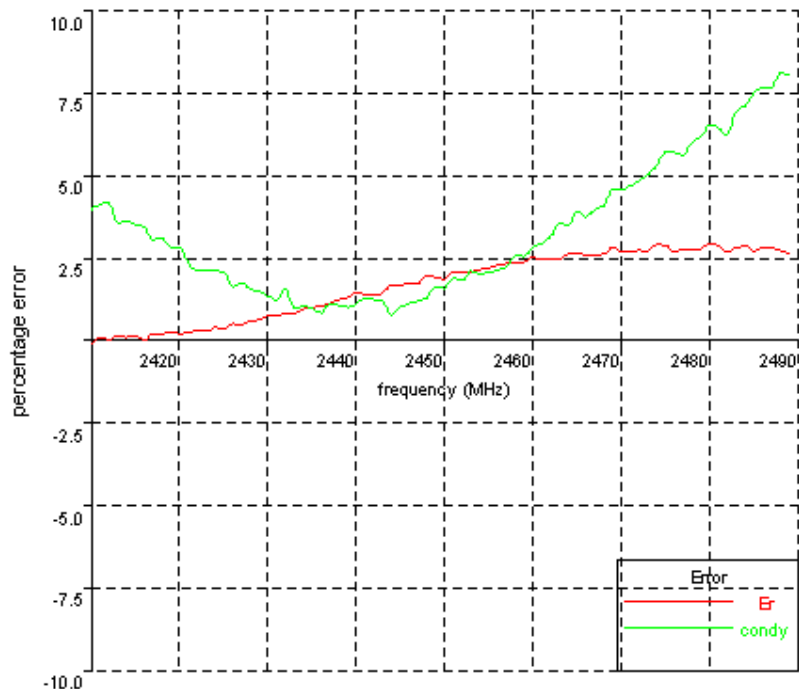
3.2.3 Body Liquid results

Date: 26 Jan. 2005	Temperature: 23.4 °C	Type: 2450 MHz/ Body (FCC)	Tested by: Marx
2410, 49.8336519755, -1.9034445282 2411, 49.8611640008, -1.8917515623 2412, 49.8582923837, -1.8929615409 2413, 49.8414117372, -1.8933344711 2414, 49.841956753, -1.885387091 2415, 49.8637966419, -1.8847090915 2416, 49.8601007194, -1.8883537926 2417, 49.874069992, -1.8811406123 2418, 49.8626180181, -1.8783622151 2419, 49.9078917208, -1.8784259146 2420, 49.9348805226, -1.8778828088 2421, 49.9480878418, -1.877056422 2422, 49.9512249498, -1.8783373158 2423, 49.9736591741, -1.8706507028 2424, 49.9926228918, -1.8673526361 2425, 50.0178889821, -1.86643075 2426, 50.0257895292, -1.8693022139 2427, 50.0735840974, -1.8669505496 2428, 50.0833188456, -1.8628054705 2429, 50.113403049, -1.865174091 2430, 50.1207706064, -1.8636018009 2431, 50.1718252715, -1.8638400749 2432, 50.206792327, -1.8596125204 2433, 50.2186437789, -1.8619283136 2434, 50.2642407419, -1.8617129779 2435, 50.2550193513, -1.8606693191 2436, 50.2926423883, -1.8628270023 2437, 50.3438721277, -1.8654900254 2438, 50.3557559376, -1.8661171841 2439, 50.3841071548, -1.8619704952 2440, 50.4050638915, -1.8612462047 2441, 50.448377895, -1.8650716174 2442, 50.472144874, -1.8664740753 2443, 50.4992731454, -1.8707914205 2444, 50.5397021171, -1.876687025 2445, 50.5821731036, -1.8749551898 2446, 50.5702267453, -1.8776532469 2447, 50.6273168676, -1.8804569976 2448, 50.6426086203, -1.8815761138 2449, 50.6737140918, -1.8827890642	2450, 50.7167043581, -1.8895002894 2451, 50.7143011673, -1.8885323579 2452, 50.7509831286, -1.9003245176 2453, 50.7801121404, -1.8974643939 2454, 50.7877443244, -1.9026752925 2455, 50.8227516147, -1.9088510718 2456, 50.8495122943, -1.9105644787 2457, 50.8356498372, -1.9142761457 2458, 50.8916990316, -1.9139773075 2459, 50.8954705971, -1.9220689685 2460, 50.8994650779, -1.9234741695 2461, 50.9281224133, -1.9307825534 2462, 50.9536384403, -1.933717913 2463, 50.9834412597, -1.9405357572 2464, 50.971400131, -1.9469954532 2465, 50.9958225502, -1.9450568549 2466, 51.0208145836, -1.9537394009 2467, 51.0057899177, -1.957870166 2468, 51.0596072153, -1.9597665537 2469, 51.0351450507, -1.9656174469 2470, 51.0560375989, -1.9703368297 2471, 51.0541766063, -1.9778200181 2472, 51.0565958288, -1.9818748387 2473, 51.0705093993, -1.9894737126 2474, 51.0391237851, -1.9931854155 2475, 51.0829826479, -1.9927717924 2476, 51.0799848175, -2.0088628459 2477, 51.0611585351, -2.0083635235 2478, 51.0774935677, -2.0142009957 2479, 51.1120964784, -2.0203289243 2480, 51.0355911854, -2.0258013858 2481, 51.0557022996, -2.0314068072 2482, 51.0275219639, -2.0464061217 2483, 51.0389903309, -2.0372216452 2484, 51.0496725188, -2.0458047661 2485, 51.0534557917, -2.0517462875 2486, 51.0624132872, -2.057324343 2487, 51.0190278012, -2.0612033543 2488, 51.0195856943, -2.0612496129 2489, 51.0488688731, -2.0715336006 2490, 51.0024587529, -2.0724414138		



3.2.4 Head Liquid results

Date: 26 Jan. 2005	Temperature: 23.6 °C	Type: 2450 MHz/ head (FCC)	Tested by: Marx
2410, 39.2345433256, -1.8346923863		2450, 39.9317422561, -1.8286370292	
2411, 39.3086266014, -1.838452495		2451, 40.0203753947, -1.8350947215	
2412, 39.2776615581, -1.839933076		2452, 40.0085901503, -1.8353697097	
2413, 39.3195342162, -1.8300057131		2453, 40.0115551725, -1.8413283098	
2414, 39.3050424214, -1.8317748307		2454, 40.0420932479, -1.8411494543	
2415, 39.3166133893, -1.8312925057		2455, 40.059770421, -1.8428695698	
2416, 39.2742357732, -1.8306498379		2456, 40.0881282787, -1.8450498001	
2417, 39.3330377942, -1.8246464418		2457, 40.1068490056, -1.8478832868	
2418, 39.3349016059, -1.8270587714		2458, 40.1136226977, -1.855491435	
2419, 39.3609683365, -1.822446932		2459, 40.1260167091, -1.8561312898	
2420, 39.3344604754, -1.823630692		2460, 40.1698186623, -1.8621279813	
2421, 39.357514106, -1.8165546449		2461, 40.1513251701, -1.865640765	
2422, 39.3619947439, -1.8126812077		2462, 40.1616813276, -1.8704733576	
2423, 39.3586468319, -1.813544192		2463, 40.1449768565, -1.8784277836	
2424, 39.403047253, -1.8145593957		2464, 40.2095410739, -1.8793502588	
2425, 39.3904387163, -1.8146389178		2465, 40.2204986843, -1.8876686933	
2426, 39.4446221967, -1.8079301334		2466, 40.1997641505, -1.8855161669	
2427, 39.4286471247, -1.8108310181		2467, 40.1982988691, -1.8907584185	
2428, 39.4789493875, -1.8083328936		2468, 40.2046483684, -1.8941060113	
2429, 39.4851852624, -1.8080989222		2469, 40.281591159, -1.9038705297	
2430, 39.5277113858, -1.8060963008		2470, 40.2356303512, -1.9050912356	
2431, 39.5281436213, -1.8052385525		2471, 40.2311816453, -1.9082731211	
2432, 39.5552600634, -1.8121064751		2472, 40.2436119792, -1.9122341493	
2433, 39.5430352187, -1.802257416		2473, 40.2406291082, -1.9167409299	
2434, 39.6048499084, -1.8044620155		2474, 40.3157303762, -1.9231916333	
2435, 39.6208898726, -1.8040260663		2475, 40.2964154993, -1.9320084359	
2436, 39.6379476536, -1.8027756625		2476, 40.2262891523, -1.9328531548	
2437, 39.6651394217, -1.8082333891		2477, 40.249949577, -1.9321169245	
2438, 39.7078593583, -1.808308656		2478, 40.2548399459, -1.9411859482	
2439, 39.7360984559, -1.8085051165		2479, 40.2489219893, -1.94468312	
2440, 39.796944894, -1.8109751627		2480, 40.3206095916, -1.952777624	
2441, 39.7641457789, -1.8148780743		2481, 40.2771498129, -1.9518340266	
2442, 39.7613432896, -1.8151927635		2482, 40.2232154967, -1.9494104676	
2443, 39.781699536, -1.8152469457		2483, 40.2547133083, -1.963803314	
2444, 39.8748250843, -1.8086556733		2484, 40.2808023242, -1.9679714153	
2445, 39.8743890531, -1.8139942736		2485, 40.2179487454, -1.9759212048	
2446, 39.8943669344, -1.8166244726		2486, 40.2569598319, -1.9803766234	
2447, 39.8752539286, -1.8188625643		2487, 40.2545627986, -1.9820478532	
2448, 39.9799975554, -1.8217058922		2488, 40.2208000725, -1.9907408191	
2449, 39.9485036452, -1.8286978984		2489, 40.1846735022, -1.991204627	
		2490, 40.2162730621, -1.9980245525	



3.3 E-Field Probe and 2450 Balanced Dipole Antenna Calibration

Probe calibration factors and dipole antenna calibration are included in Appendix C.

4.0 Measurement Uncertainty

The uncertainty budget has been determined for the INDEXSAR SARA2 measurement system according to IEEE P1528 documents [3] and is given in the following table. The extended uncertainty (95% confidence level) was assessed to be 20.6 % for SAR measurement, and the extended uncertainty (95% confidence level) was assessed to be 20.2 % for system performance check.

Table 1 Exposure Assessment Uncertainty
Example of measurement uncertainty assessment SAR measurement

(blue entries are site-specific)

a	b			c	d	e		f	g	h	i
Uncertainty Component	Sec.	Tol. (+/-)			Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	$\sqrt{3}$	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	$\sqrt{3}$	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	$\sqrt{3}$	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	$\sqrt{3}$	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	$\sqrt{3}$	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	$\sqrt{3}$	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	$\sqrt{3}$	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	$\sqrt{3}$	1.73	1	1	4.62	4.62
Test Sample Related											
Test Sample Positioning	E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Device Holder Uncertainty	E4.1		2	2.00	N	1	1.00	1	1	2.00	2.00
Output Power Variation	6.6.2		5	5.00	R	$\sqrt{3}$	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (shape and thickness)	E3.1		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.5	10.3
Expanded uncertainty	(95% Confidence Level)				k=2					20.6	20.3

Table 2 System Check (Verification)

Example of measurement uncertainty assessment for system performance check

(blue entries are site-specific)

a	b			c	d	e		f	g	h	i
Uncertainty Component	Sec.	Tol. (+/-)			Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	$\sqrt{3}$	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	$\sqrt{3}$	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	$\sqrt{3}$	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	$\sqrt{3}$	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	$\sqrt{3}$	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	$\sqrt{3}$	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	$\sqrt{3}$	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	$\sqrt{3}$	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	$\sqrt{3}$	1.73	1	1	4.62	4.62
Dipole											
Dipole axis to liquid distance	8, E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Input power and SAR drift measurement	8, 6.6.2		5	5.00	R	$\sqrt{3}$	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (thickness)	E3.1		4	4.00	R	$\sqrt{3}$	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	$\sqrt{3}$	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.3	10.1
Expanded uncertainty	(95% Confidence Level)				k=2					20.2	19.9

5.0 Measurement Traceability

All measurements described in this report are traceable to Chinese National Laboratory Accreditation (CNLA) standards or appropriate national standards.

6.0 WARNING LABEL INFORMATION - USA

See user manual.

7.0 REFERENCES

- [1] ANSI, *ANSI/IEEE C95.1-1999: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3kHz to 300 GHz*, The Institute of electrical and Electronics Engineers, Inc., New York, NY 10017, 1999
- [2] Federal Communications Commission, "Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields", Supplement C to OET Bulletin 65, Washington, D.C. 20554, 1997
- [3] IEEE Standards Coordinating Committee 34, "IEEE Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques", IEEE Std 1528TM-2003

8.0 DOCUMENT HISTORY

Revision/ Job Number	Writer Initials	Date	Change
N/A	S.L.	Feb. 3, 2005	Original document

APPENDIX A - SAR Evaluation Data

Power drift is the measurement of power drift of the device over one complete SAR scan.

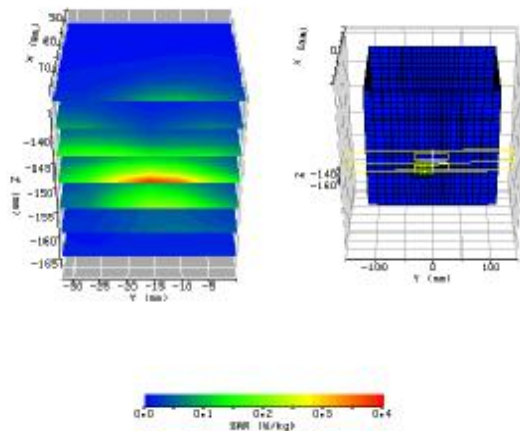
To assess the drift of the power of the device under test, a SAR measurement was made in the middle of the zoom scan volume at the start of the scan and a measurement at this point was then also made after the measurement scan. The difference between the two measurements should be less than 5%.

Plot #1(1/2)

Date:	2005/1/27	Position:	EUT top side at phantom box outside 0mm
Filename:	top 0mm mid 11g.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2437 MHz
Shape File:	CA27-top side.csv	Power Level:	15.974 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1



ZOOM SCAN RESULTS:

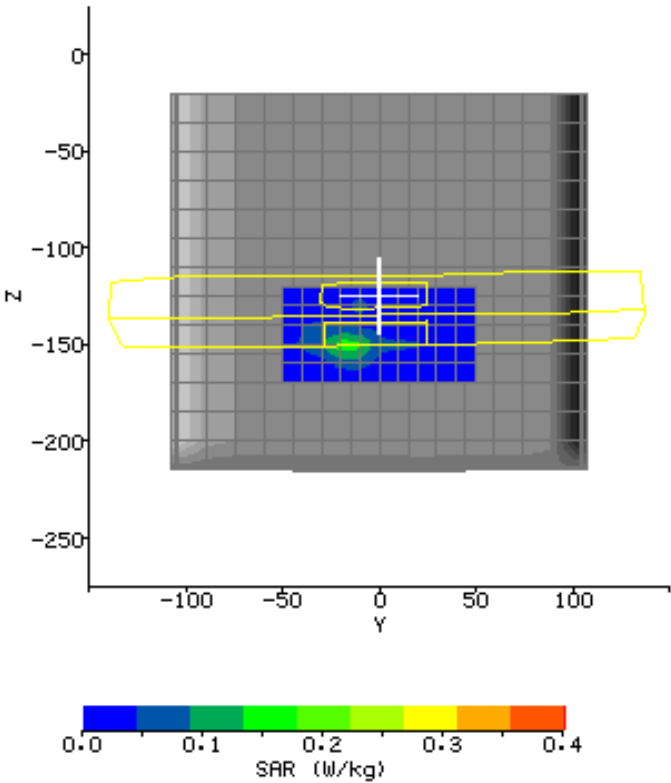
Spot SAR (W/kg):	Start Scan	End Scan	
	0.043	0.043	
Change during Scan (%)	-1.64		
Max E-field (V/m):	14.35		
Max SAR (W/kg)	1g	10g	
	0.221	0.084	
Location of Max (mm):	X	Y	Z
	78.1	-32.0	-151.9

Plot #1(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0

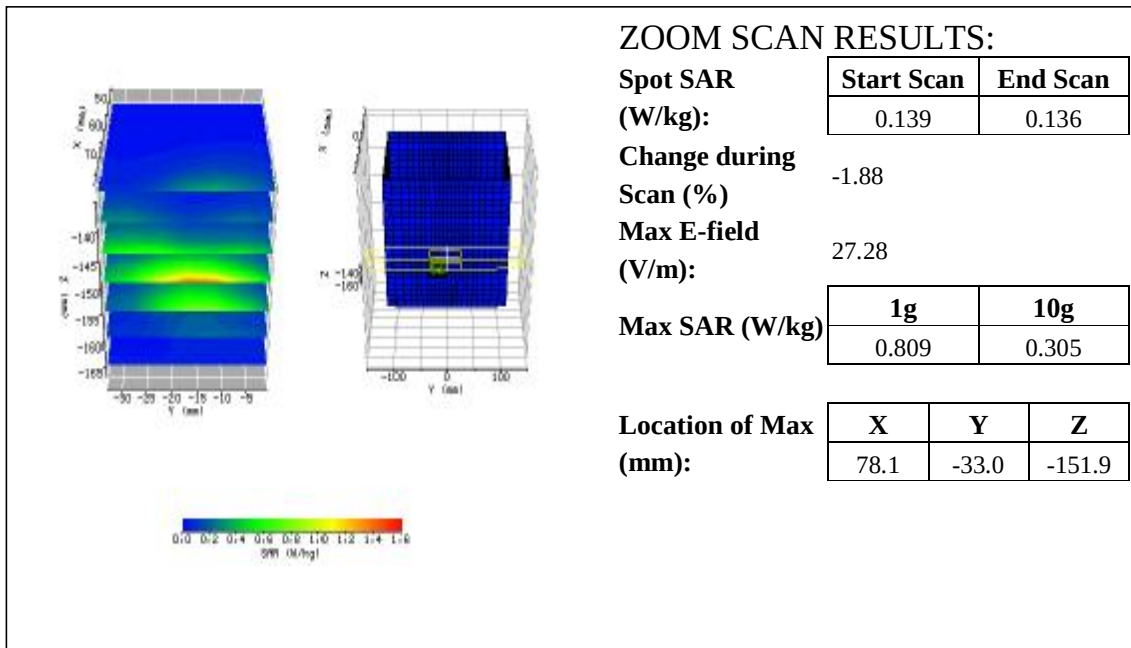


Plot #2(1/2)

Date:	2005/1/27	Position:	EUT top side at phantom box outside 0mm
Filename:	top 0mm mid 11b.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2437 MHz
Shape File:	CA27-top side.csv	Power Level:	15.381 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries	-			
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1

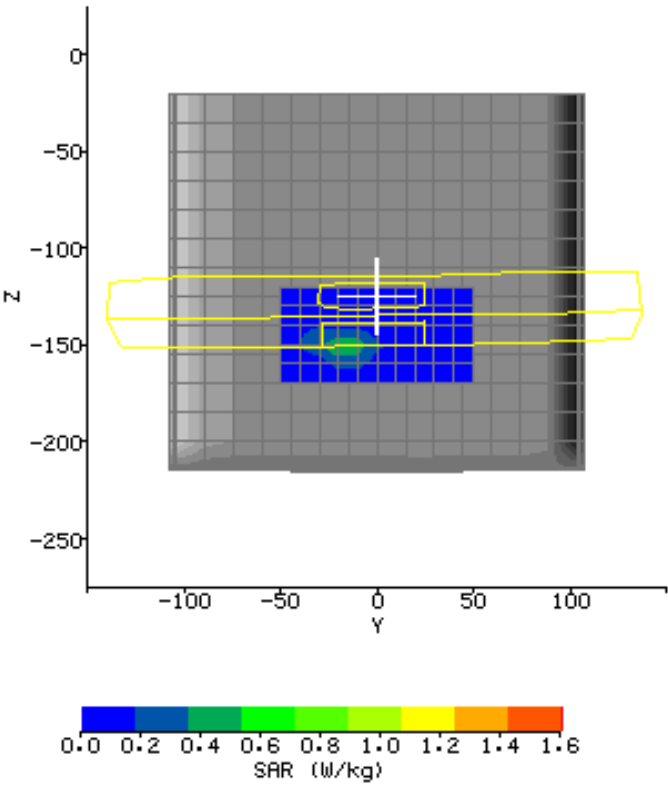


Plot #2(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0

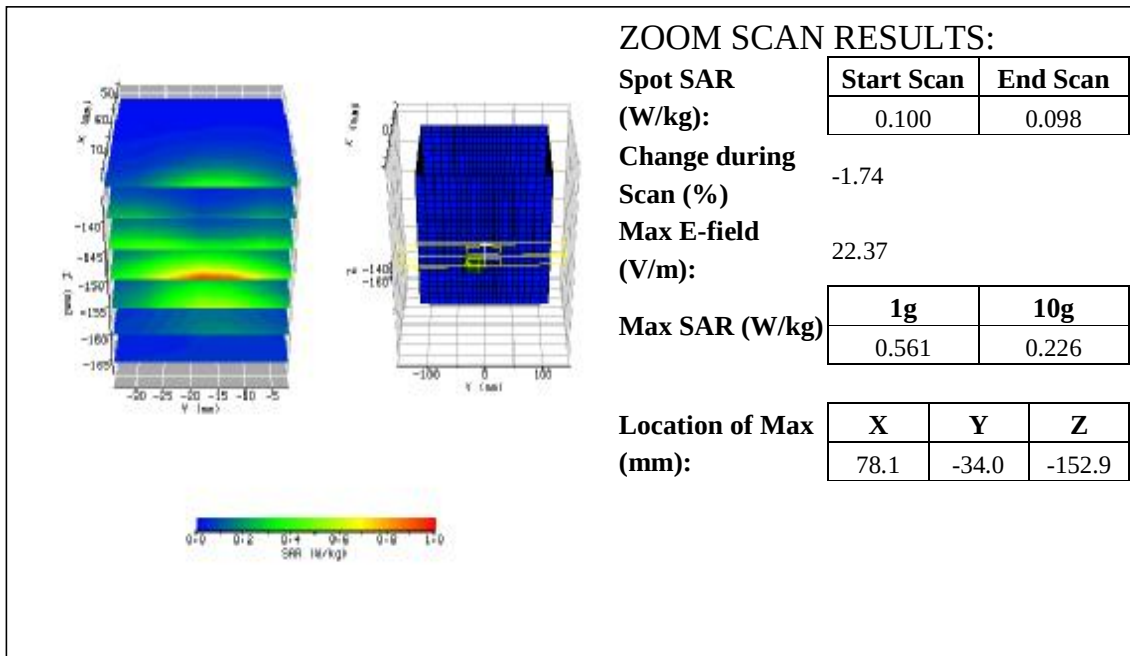


Plot #3(1/2)

Date:	2005/1/27	Position:	EUT top side at phantom box outside 0mm
Filename:	top 0mm low 11b.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2412 MHz
Shape File:	CA27-top side.csv	Power Level:	16.131 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries	-			
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1

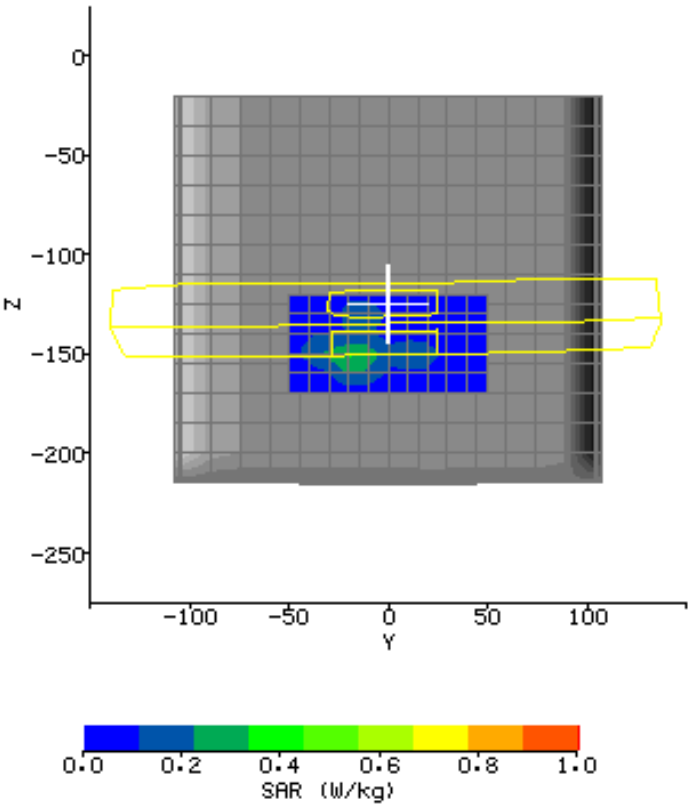


Plot #3(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0

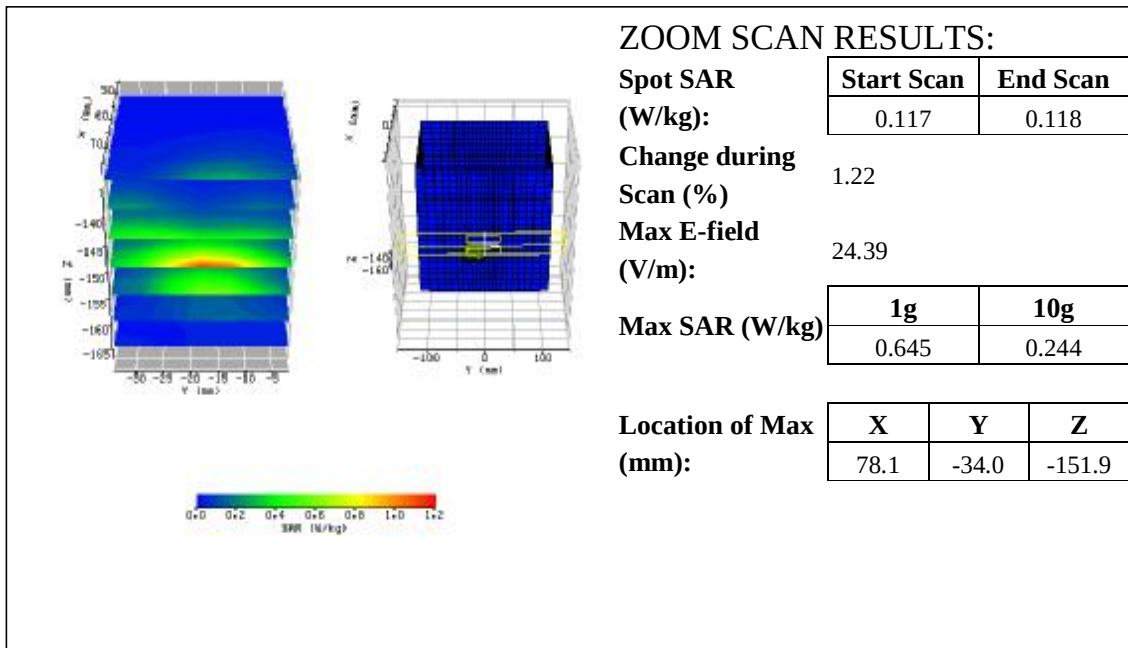


Plot #4(1/2)

Date:	2005/1/27	Position:	EUT top side at phantom box outside 0mm
Filename:	top 0mm high 11b.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2462 MHz
Shape File:	CA27-top side.csv	Power Level:	14.912 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries	-			
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1

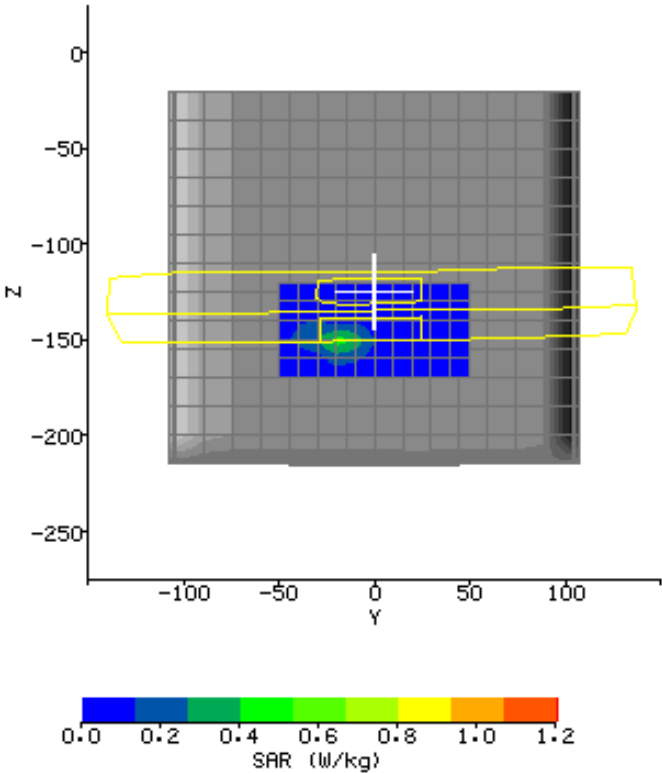


Plot #4(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0

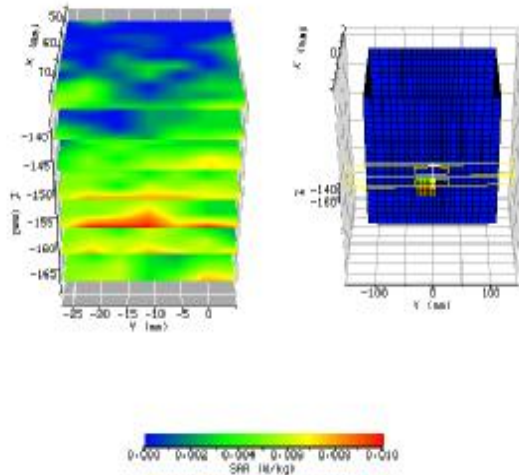


Plot #5(1/2)

Date:	2005/1/27	Position:	EUT top side at phantom box outside 15mm
Filename:	top 15mm mid 11g.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2437 MHz
Shape File:	CA27-top side.csv	Power Level:	15.974 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1



ZOOM SCAN RESULTS:

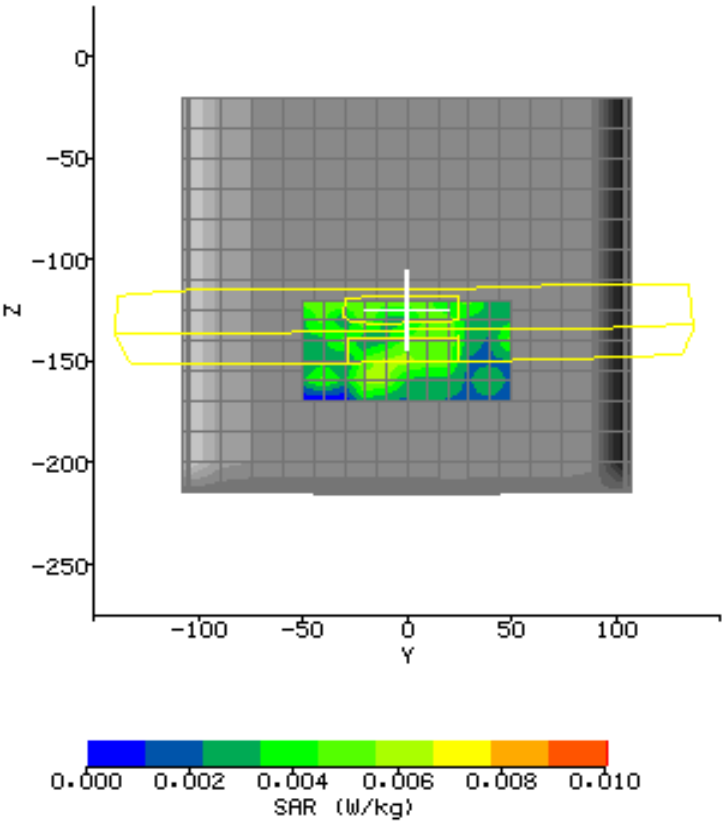
Spot SAR (W/kg):	Start Scan		End Scan	
	0.005		0.005	
Change during Scan (%)	0			
Max E-field (V/m):	2.26			
Max SAR (W/kg)	1g		10g	
	0.008		0.005	
Location of Max (mm):	X	Y	Z	
	78.1	-27.0	-159.3	

Plot #5(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0



Plot #6(1/2)

Date:	2005/1/27	Position:	EUT top side at phantom box outside 15mm
Filename:	top 15mm mid 11b.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2437 MHz
Shape File:	CA27-top side.csv	Power Level:	15.381 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries	-			
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1

Two 3D SAR scan plots are shown. The left plot displays a color-coded SAR distribution on a grid with X (mm) from -50 to 0 and Y (mm) from -170 to -145. The right plot displays a similar distribution on a grid with X (mm) from -100 to 100 and Y (mm) from -160 to -145. A color scale bar at the bottom indicates SAR values from 0.00 to 0.04 W/kg.

ZOOM SCAN RESULTS:

Spot SAR

(W/kg):

Change during

Scan (%)

Max E-field

(V/m):

Max SAR (W/kg)

Location of Max

(mm):

Start Scan

End Scan

0.008

0.008

0

4.47

1g

10g

0.029

0.016

X

Y

Z

78.1

-30.0

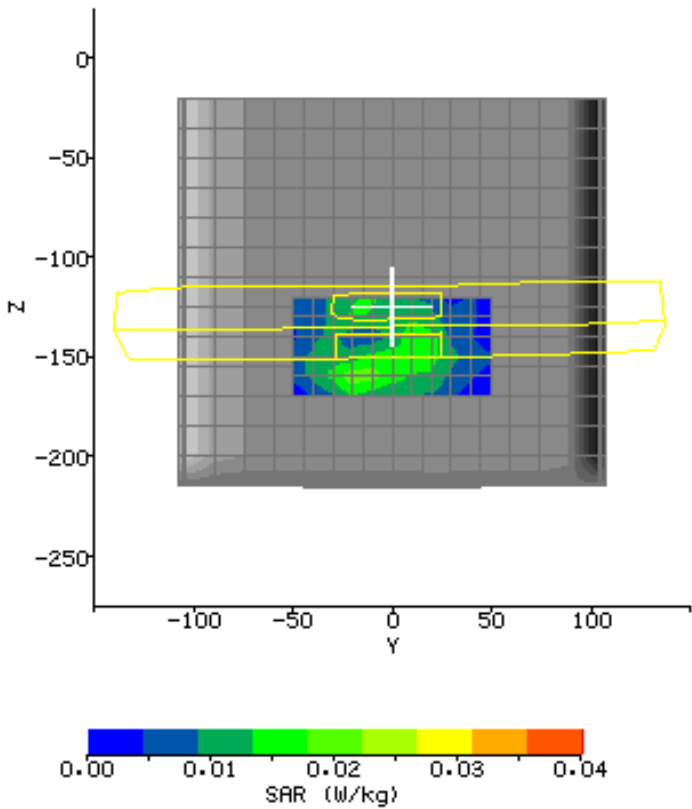
-158.9

Plot #6(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0

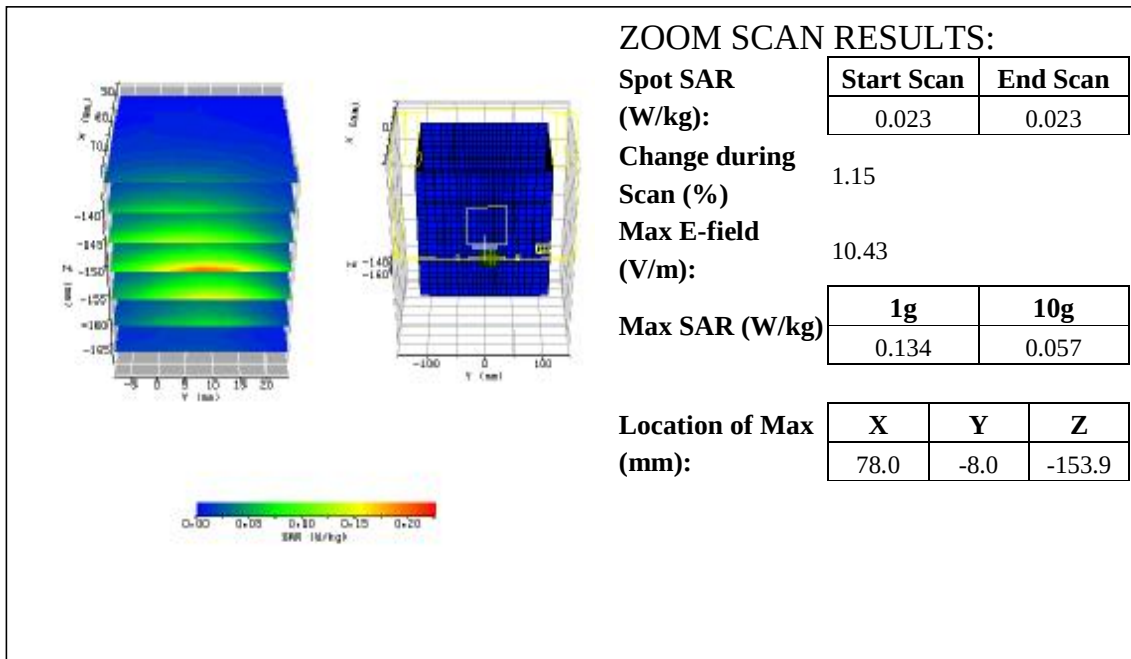


Plot #7(1/2)

Date:	2005/1/27	Position:	EUT bottom at phantom box outside 0mm
Filename:	bottom 0mm mid 11g.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2437 MHz
Shape File:	CA27-rear side.csv	Power Level:	15.974 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries	-			
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1

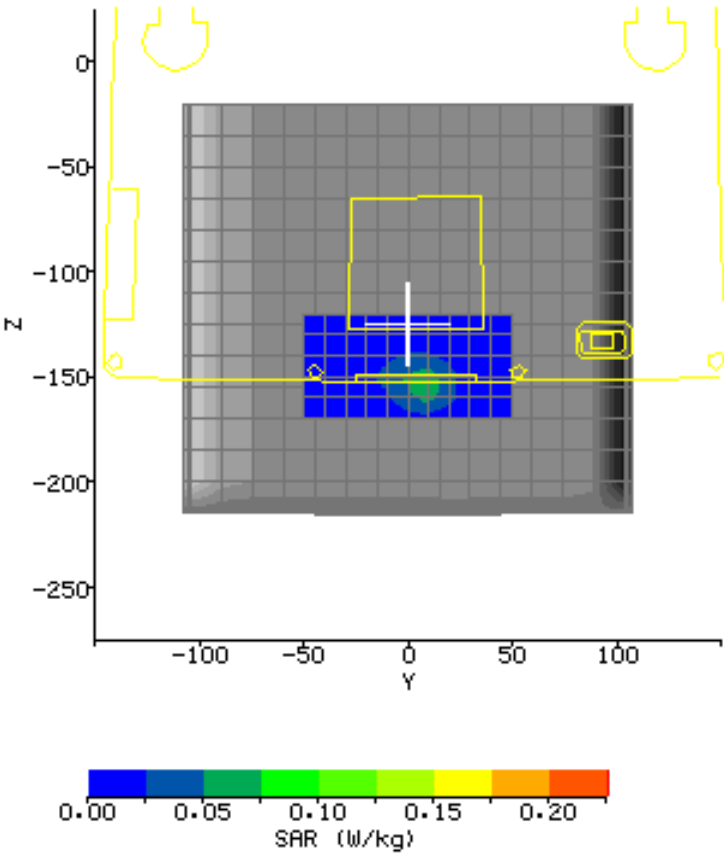


Plot #7(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0

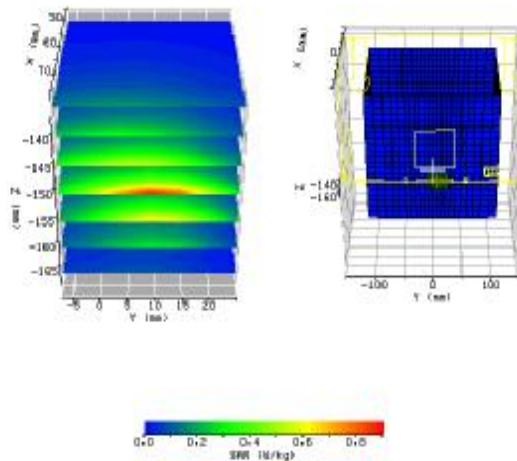


Plot #8(1/2)

Date:	2005/1/28	Position:	EUT bottom at phantom box outside 0mm
Filename:	bottom 0mm mid 11b.txt	Phantom:	HeadBox2-test.csv
Device Tested:	Tablet Personal Computer	Head Rotation:	0
Antenna:	PIFA antenna	Test Frequency:	2437 MHz
Shape File:	CA27-rear side.csv	Power Level:	15.381 dBm

Probe:	0149			
Cal File:	SN0149_2450_CW_BODY			
Cal Factors:		X	Y	Z
	Air	365	444	414
	DCP	20	20	20
	Lin	.561	.561	.561
Amp Gain:	2			
Averaging:	1			
Batteries				
Replaced:	-			

Liquid:	15.5cm
Type:	2450 MHz Body
Conductivity:	1.889
Relative Permittivity:	50.716
Liquid Temp (deg C):	23.2
Ambient Temp (deg C):	23.5
Ambient RH (%):	50.2
Density (kg/m3):	1000
Software Version:	2.3VPM
Crest Factor:	1



ZOOM SCAN RESULTS:

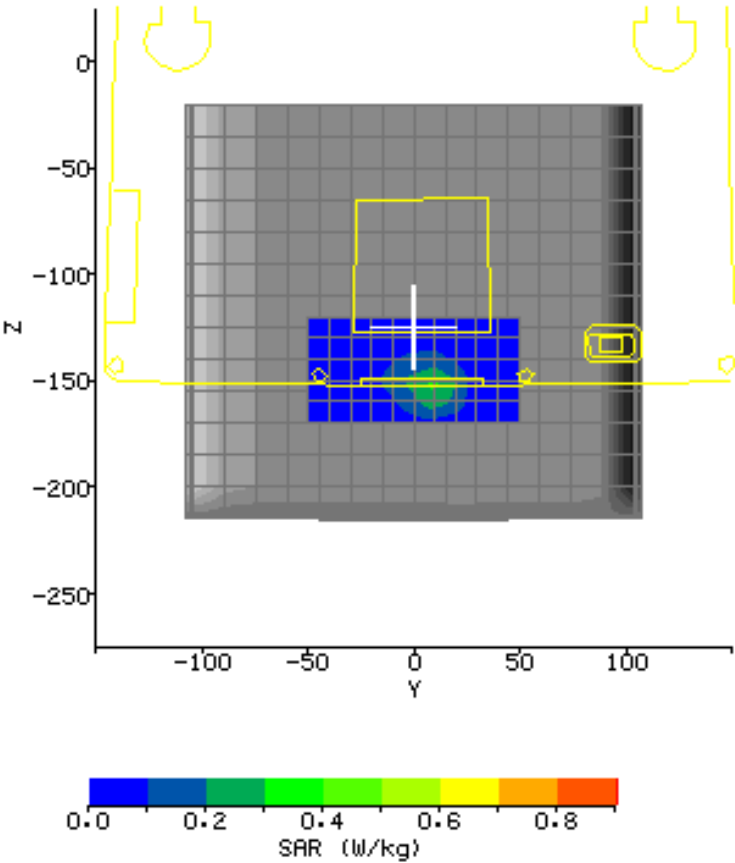
Spot SAR (W/kg):	Start Scan	End Scan	
	0.101	0.099	
Change during Scan (%)	-1.62		
Max E-field (V/m):	21.71		
Max SAR (W/kg)	1g	10g	
	0.576	0.243	
Location of Max (mm):	X	Y	Z
	78.0	-7.0	-153.0

Plot #8(2/2)

AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	50.0	10.0
Z	-170.0	-120.0	5.0



APPENDIX B - Photographs

(External)



(Antenna)



**APPENDIX C - E-Field Probe and 2450MHz Balanced Dipole Antenna Calibration
Data**



**IMMERSIBLE SAR PROBE
CALIBRATION REPORT
Part Number: IXP – 050**

S/N 0149

May 2004



Indexsar Limited
Oakfield House
Cudworth Lane
Newdigate
Surrey RH5 5BG
Tel: +44 (0) 1306 632 870
Fax: +44 (0) 1306 631 834
e-mail: enquiries@indexsar.com

INTRODUCTION

This Report presents measured calibration data for a particular Indexsar SAR probe (S/N 0149) and describes the procedures used for characterisation and calibration.

Indexsar probes are characterised using procedures that, where applicable, follow the recommendations of CENELEC [1] and IEEE [2] standards. The procedures incorporate techniques for probe linearisation, isotropy assessment and determination of liquid factors (conversion factors). Calibrations are determined by comparing probe readings with analytical computations in canonical test geometries (waveguides) using normalised power inputs.

Each step of the calibration procedure and the equipment used is described in the sections below.

CALIBRATION PROCEDURE

1. Equipment Used

For the first part of the characterisation procedure, the probe is placed in an isotropy measurement jig as pictured in Figure 1. In this position the probe can be rotated about its axis by a non-metallic belt driven by a stepper motor.

The probe is attached via its amplifier and an optical cable to a PC. A schematic representation of the test geometry is illustrated in Figure 2.

A balanced dipole (900 MHz) is inserted horizontally into the bracket attached to a second belt (Figure 1). The dipole can also be rotated about its axis. A cable connects the dipole to a signal generator, via a directional coupler and power meter. The signal generator feeds an RF amplifier at constant power, the output of which is monitored using the power meter. The probe is positioned so that its sensors line up with the rotation center of the source dipole. By recording output voltage measurements of each channel as both the probe and the dipole are rotated, data are obtained from which the spherical isotropy of the probe can be optimised and its magnitude determined.

The calibration process requires E-field measurements to be taken in air, in 900 MHz simulated brain liquid and at other frequencies/liquids as appropriate.

2. Linearising probe output

The probe channel output signals are linearised in the manner set out in Refs [1] and [2]. The following equation is utilized for each channel:

$$U_{lin} = U_{o/p} + U_{o/p}^2 / DCP \quad (1)$$

where U_{lin} is the linearised signal, $U_{o/p}$ is the raw output signal in voltage units and DCP is the diode compression potential in similar voltage units.

DCP is determined from fitting equation (1) to measurements of U_{lin} versus source feed power over the full dynamic range of the probe. The DCP is a characteristic of the schottky diodes used as the sensors. For the IXP-050 probes with CW signals the DCP values are typically 0.10V (or 20 in the voltage units used by Indexsar software, which are $V*200$).

3. Selecting channel sensitivity factors to optimise isotropic response

The basic measurements obtained using the calibration jig (Fig 1) represent the output from each diode sensor as a function of the presentation angle of the source (probe and dipole rotation angles). The directionality of the orthogonally-arranged sensors can be checked by analysing the data using dedicated Indexsar software, which displays the data in 3D format as in Figure 3. The left-hand side of this diagram shows the individual channel outputs after linearisation (see above). The program uses these data to balance the channel outputs and then applies an optimisation process, which makes fine adjustments to the channel factors for optimum isotropic response.

The next stage of the process is to calibrate the Indexsar probe to a W&G EMR300 E-field meter in air. The principal reasons for this are to obtain conversion factors applicable should the probe be used in air and to provide an overall measure of the probe sensitivity.

A multiplier is applied to factors to bring the magnitudes of the average E-field measurements as close as possible to those of the W&G probe.

The following equation is used (where linearised output voltages are in units of $V*200$):

$$E_{air}^2 (V/m) = U_{linx} * Air Factor_x + U_{liny} * Air Factor_y + U_{linz} * Air Factor_z \quad (2)$$

It should be noted that the air factors are not separately used for normal SAR testing. The IXP-050 probes are optimised for use in tissue-simulating liquids and do not behave isotropically in air.

4. 900 MHz Liquid Calibration

Conversion factors for use when the probes are immersed in tissue-simulant liquids at 900 MHz are determined either using a waveguide or by comparison to a reference probe that has been calibrated by NPL. Waveguide procedures are described later. The summary sheet indicates the method used for the probe S/N 0149.

The conversion factor, referred to as the 'liquid factor' is also applied to the measurements of each channel. The following equation is used (where output voltages are in units of $V*200$):

$$E_{liq}^2 (V/m) = U_{linx} * Air Factor_x * Liq Factor_x + U_{liny} * Air Factor_y * Liq Factor_y + U_{linz} * Air Factor_z * Liq Factor_z \quad (3)$$

A 3D representation of the spherical isotropy for probe S/N 0149 using these factors is shown in Figure 3.

The rotational isotropy can also be determined from the calibration jig measurements and is reported as the 900MHz isotropy in the summary table. Note that waveguide measurements can also be used to determine rotational isotropy (Fig. 5).

The design of the cells used for determining probe conversion factors are waveguide cells as shown in Figure 4. The cells consist of a coax to waveguide transition and an open-ended section of waveguide containing a dielectric separator. Each waveguide cell stands in the upright position and is filled with liquid within 10 mm of the open end. The separator provides a liquid seal and is designed for a good electrical transition from air filled guide to liquid filled guide. The choice of cell depends on the portion of the frequency band to be examined and the choice of liquid used. The depth of liquid ensures there is negligible radiation from the waveguide open top and that the probe calibration is not influenced by reflections from nearby objects. The return loss at the coaxial connector of the filled waveguide cell is measured initially using a network analyser and this information is used subsequently in the calibration procedure. The probe is positioned in the centre of the waveguide and is adjusted vertically or rotated using stepper motor arrangements. The signal generator is connected to the waveguide cell and the power is monitored with a coupler and a power meter. A fuller description of the waveguide method is given below.

The liquid dielectric parameters used for the probe calibrations are listed in the Tables below. The final calibration factors for the probe are listed in the summary chart.

WAVEGUIDE MEASUREMENT PROCEDURE

The calibration method is based on setting up a calculable specific absorption rate (SAR) in a vertically-mounted WG8 (R22) waveguide section [1]. The waveguide has an air-filled, launcher section and a liquid-filled section separated by a matching window that is designed to minimise reflections at the liquid interface. A TE_{01} mode is launched into the waveguide by means of a N-type-to-waveguide adapter. The power delivered to the liquid section is calculated from the forward power and reflection coefficient measured at the input to the waveguide. At the centre of the cross-section of the waveguide, the local spot SAR in the liquid as a function of distance from the window is given by functions set out in IEEE1528 as below:

Because of the low cutoff frequency, the field inside the liquid nearly propagates as a TEM wave. The depth of the medium (greater than three penetration depths) ensures that reflections at the upper surface of the liquid are negligible. The power absorbed in the liquid is determined by measuring the waveguide forward and reflected power. Equation (4) shows the relationship between the SAR at the cross-sectional center of the lossy waveguide and the longitudinal distance (z) from the dielectric separator

$$SAR(z) = \frac{4(P_f - P_b)}{r abd} e^{-2z/d} \quad (4)$$

where the density ρ is conventionally assumed to be 1000 kg/m^3 , ab is the cross-sectional area of the waveguide, P_f and P_b are the forward and reflected power inside the lossless section of the waveguide, respectively. The penetration depth d , which is the reciprocal of the waveguide-mode attenuation coefficient, is determined from a scan along the z-axis and compared with the theoretical value determined from Equation (5) using the measured dielectric properties of the lossy liquid.

$$d = \left[\text{Re} \left\{ \sqrt{(p/a)^2 + j\omega m_o (s + j\omega e_o e_r)} \right\} \right]^{-1}. \quad (5)$$

Table A.1 of [1] can be used for designing calibration waveguides with a return loss greater than 30 dB at the most important frequencies used for personal wireless communications. Values for the penetration depth for these specific fixtures and tissue-simulating mixtures are also listed in Table A.1.

According to [1], this calibration technique provides excellent accuracy, with standard uncertainty of less than 3.6% depending on the frequency and medium. The calibration itself is reduced to power measurements traceable to a standard calibration procedure. The practical limitation to the frequency band of 800 to 2500 MHz because of the waveguide size is not severe in the context of compliance testing.

CALIBRATION FACTORS MEASURED FOR PROBE S/N 0149

The probe was calibrated at 900, 1800, 1900 and 2450MHz MHz in liquid samples representing both brain liquid and body fluid at these frequencies. The calibration was for CW signals only, and the axis of the probe was parallel to the direction of propagation of the incident field i.e. end-on to the incident radiation. The axial isotropy of the probe was measured by rotating the probe about its axis in 10 degree steps through 360 degrees in this orientation.

The reference point for the calibration is in the centre of the probe's cross-section at a distance of 2.7 m from the probe tip in the direction of the probe amplifier. A value of 2.7 mm should be used for the tip to sensor offset distance in the software.

It is important that the diode compression point and air factors used in the software are the same as those quoted in the results tables, as these are used to convert the diode output voltages to a SAR value.

DIELECTRIC PROPERTIES OF LIQUIDS

The dielectric properties of the brain and body tissue-simulant liquids employed for calibration are listed in the tables below. The measurements were performed prior to each waveguide test using an Indexsar DiLine measurement kit, which uses the TEM method as recommended in [2].

AMBIENT CONDITIONS

Measurements were made in the open laboratory at $22 \pm 2.0^\circ\text{C}$. The temperature of the liquids in the waveguide used was measured using a mercury thermometer.

RESPONSE TO MODULATED SIGNALS

To measure the response of the probe and amplifier to modulated signals, the probe is held vertically in a liquid-filled waveguide.

An RF amplifier is allowed to warm up and stabilise before use. A spectrum analyser is used to demonstrate that the peak power of the RF amplifier for the CW signals and the pulsed signals are within 0.1dB of each other when the signal generator is switched from CW to modulated output. Subsequently, the power levels recorded are read from a power meter when a CW signal is being transmitted.

The test sequence involves manually stepping the power up in regular (e.g. 2 dB) steps from the lowest power that gives a measurable reading on the SAR probe up to the maximum that the amplifiers can deliver.

At each power level, the individual channel outputs from the SAR probe are recorded at CW and then recorded again with the modulation setting. The results are entered into a spreadsheet. Using the spreadsheets, the modulated power is calculated by applying a factor to the measured CW power (e.g. for GSM, this factor is 9.03dB). This process is repeated 3 times with the response maximised for each channel sensor in turn.

The probe channel output signals are linearised in the manner set out in Section 1 above using equation (1) with the DCPs determined from the linearisation procedure. Calibration factors for the probe are used to determine the E-field values corresponding to the probe readings using equation (3). SAR is determined from the equation

$$\text{SAR (W/kg)} = E_{\text{liq}}^2 \text{ (V/m)} * \sigma \text{ (S/m)} / 1000 \quad (6)$$

Where σ is the conductivity of the simulant liquid employed.

Using the spreadsheet data, the DCP value for linearising each of the individual channels (X, Y and Z) is assessed separately. The corresponding DCP values are listed in the summary page of the calibration factors for each probe.

Figure 7 shows the linearised probe response to GSM signals, Figure 8 the response to GPRS signals (GSM with 2 timeslots) and Figure 9 the response to CDMA IS-95A and W-CDMA signals.

Additional tests have shown that the modulation response is similar at 1800MHz and is not affected by the orientation between the source and the probe.

VPM (Virtual Probe Miniaturisation)

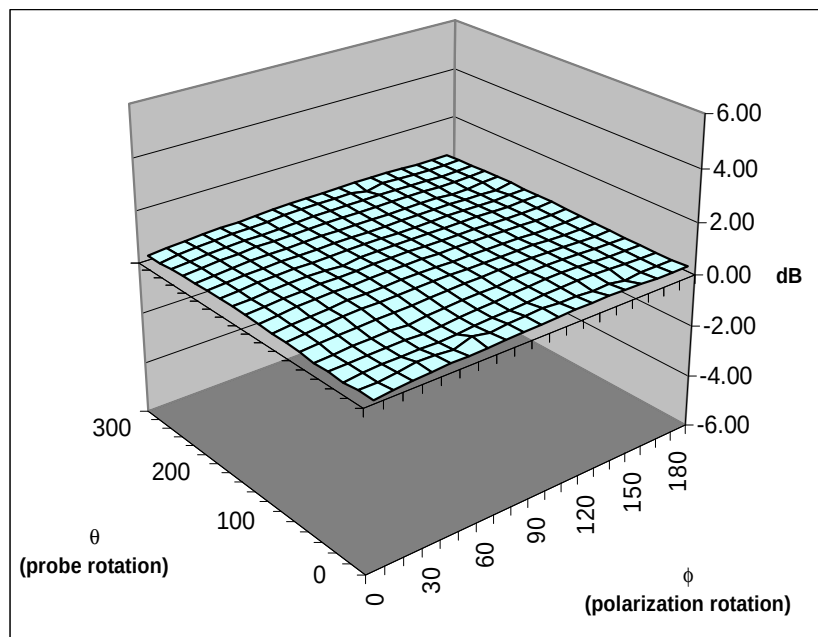
SAR probes with 3 diode-sensors in an orthogonal arrangement are designed to display an isotropic response when exposed to a uniform field. However, the probes are ordinarily used for measurements in non-uniform fields and isotropy is not assured when the field gradients are significant compared to the dimensions of the tip containing the three orthogonally-arranged dipole sensors.

It becomes increasingly important to assess the effects of field gradients on SAR probe readings when higher frequencies are being used. For Indexsar IXP-050 probes, which are of 5mm tip diameter, field gradient effects are minor at GSM frequencies, but are major above 5GHz. Smaller probes are less affected by field gradients and so probes, which are significantly less than 5mm diameter, would be better for applications above 5GHz.

The IndexSAR report IXS0223 describes theoretical and experimental studies to evaluate the issues associated with the use of probes at arbitrary angles to surfaces and field directions. Based upon these studies, the procedures and uncertainty analyses referred to in P1528 are addressed for the full range of probe presentation angles.

In addition, generalized procedures for correcting for the finite size of immersible SAR probes are developed. Use of these procedures enables application of schemes for virtual probe miniaturization (VPM) – allowing probes of a specific size to be used where physically-smaller probes would otherwise be required.

Given the typical dimensions of 3-channel SAR probes presently available, use of the VPM technique extends the satisfactory measurement range to higher frequencies.



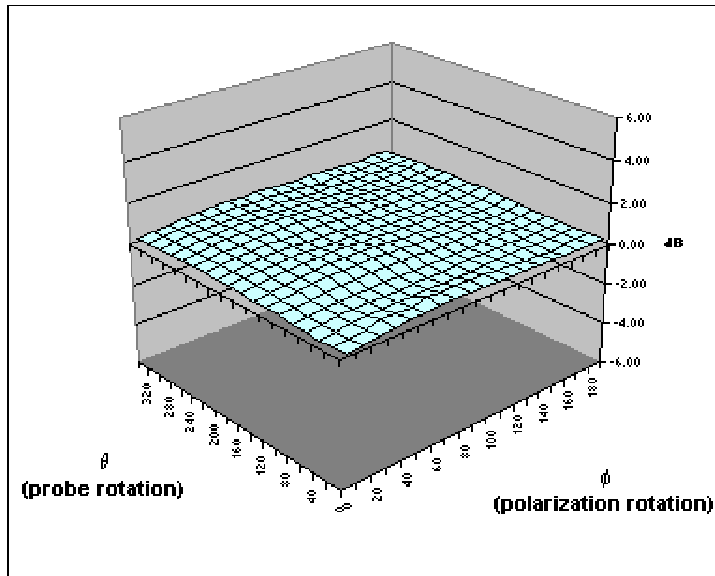
Surface Isotropy diagram of IXP-050 Probe S/N 0149 at 900MHz after VPM

Probe tip radius 1.25
X Ch. Angle to red dot 7

	Head		Body	
Frequency	Bdy. Corr. – f(0)	Bdy. Corr. – d(mm)	Bdy. Corr. – f(0)	Bdy. Corr. – d(mm)
900	0.2	1.0	0.31	2.0
1800	0.2	2.0	0.27	1.6
1900	0.19	1.7	0.3	1.4
2450	0.24	2.0	0.72	2.0

SUMMARY OF CALIBRATION FACTORS FOR PROBE IXP-050 S/N 0149

Spherical isotropy measured at 900 MHz0.28 (+/-) dB



	X	Y	Z	
Air factors	365	444	414	(V*200)
DCPs	20	20	20	(V*200)
GSM	13.4	9.6	7.9	(V*200)
CDMA	20	20	20	(V*200)

f (MHz)	Axial isotropy (+/- dB)		SAR conversion factors (liq/air)		Notes
	BRAIN	BODY	BRAIN	BODY	
450	0.08	0.07	0.344	0.360	1,2,3
835	0.08	0.07	0.344	0.360	1,2,3
900	0.08	0.07	0.344	0.360	1,2,3
1800	0.10	0.11	0.438	0.477	1,2,3
1900	0.11	0.12	0.441	0.504	1,2,3
2450	0.11	0.11	0.504	0.561	1,2,3

Notes				
1)	Calibrations done at 22C +/- 2C			
2)	Waveguide calibration			
3)	Checked using box-phantom validation test			

(the graph shows a simple, spreadsheet representation of surface shown in 3D in Figure 3 below)

PROBE SPECIFICATIONS

Indexsar probe 0149, along with its calibration, is compared with CENELEC and IEEE standards recommendations (Refs [1] and [2]) in the Tables below. A listing of relevant specifications is contained in the tables below:

Dimensions	S/N 0149	CENELEC [1]	IEEE [2]
Overall length (mm)	350		
Tip length (mm)	10		
Body diameter (mm)	12		
Tip diameter (mm)	5.2	8	8
Distance from probe tip to dipole centers (mm)	2.7		

Dynamic range	S/N 0149	CENELEC [1]	IEEE [2]
Minimum (W/kg)	0.01	<0.02	0.01
Maximum (W/kg)	>35	>100	100
N.B. only measured to 35 W/kg			

Linearity of response	S/N 0149	CENELEC [1]	IEEE [2]
Over range 0.01 – 100 W/kg (+/- dB)	0.125	0.50	0.25

Isotropy (measured at 900MHz)	S/N 0149	CENELEC [1]	IEEE [2]
Axial rotation with probe normal to source (+/- dB) at 900, 1800, 1900 and 2450 MHz	0.12 Max (See table above)	0.5	0.25
Spherical isotropy covering all orientations to source (+/- dB)	0.28	1.0	0.50

Construction	Each probe contains three orthogonal dipole sensors arranged on a triangular prism core, protected against static charges by built-in shielding, and covered at the tip by PEEK cylindrical enclosure material. No adhesives are used in the immersed section. Outer case materials are PEEK and heat-shrink sleeving.
Chemical resistance	Tested to be resistant to glycol and alcohol containing simulant liquids but probes should be removed, cleaned and dried when not in use.

REFERENCES

- [1] CENELEC, EN 50361, July 2001. Basic Standard for the measurement of specific absorption rate related to human exposure to electromagnetic fields from mobile phones.
- [2] IEEE 1528, Recommended practice for determining the spatial-peak specific absorption rate (SAR) in the human body due to wireless communications devices: Experimental techniques.

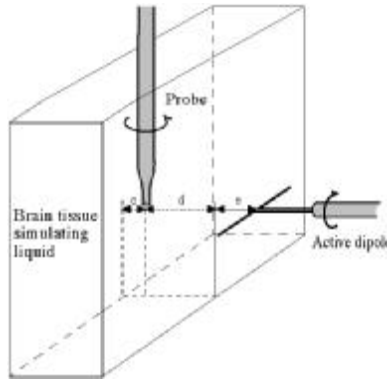
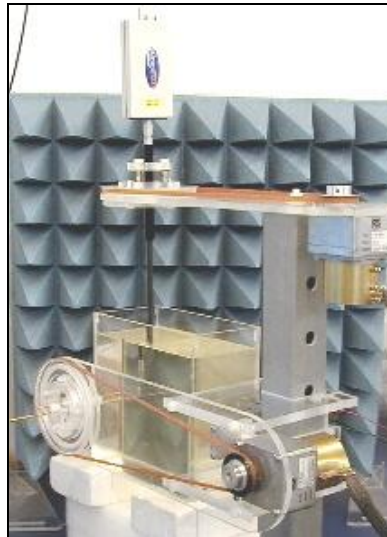


Figure 1. Spherical isotropy jig showing probe, dipole and box filled with simulated brain liquid (see Ref [2], Section A.5.2.1)

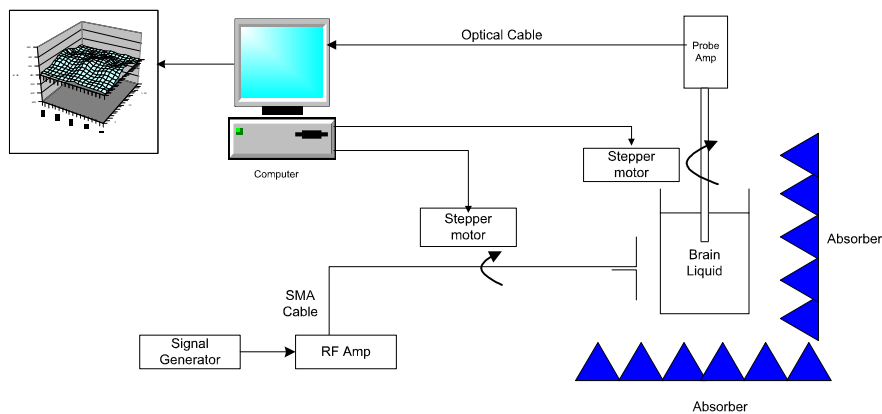


Figure 2. Schematic diagram of the test geometry used for isotropy determination

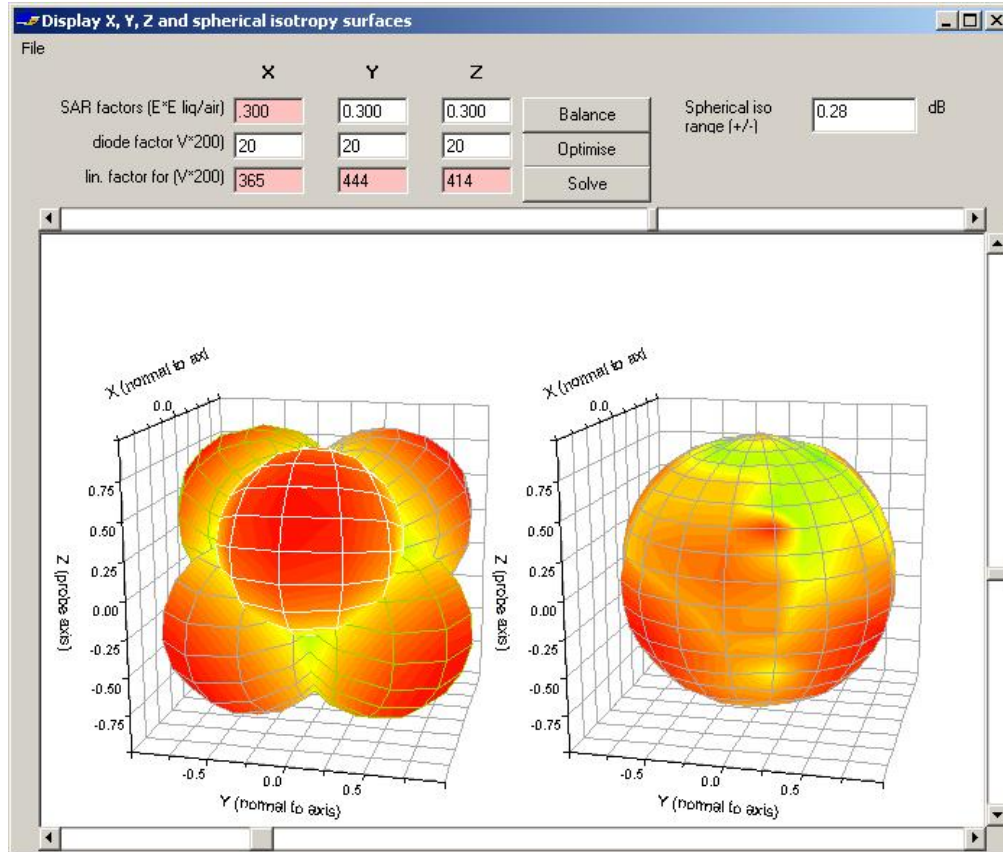


Figure 3. Graphical representation of the probe response to fields applied from each direction. The diagram on the left shows the individual response characteristics of each of the three channels and the diagram on the right shows the resulting probe sensitivity in each direction. The colour range in the figure images the lowest values as blue and the maximum values as red. For the probe S/N 0149, this range is (+/-) 0.28 dB. The probe is more sensitive to fields parallel to the axis and less sensitive to fields normal to the probe axis.

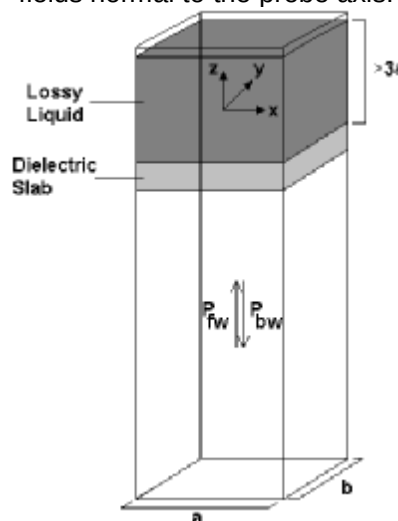


Figure 4. Geometry used for waveguide calibration (after Ref [2]. Section A.3.2.2)

IXP-050 S/N 0149

11-May-04

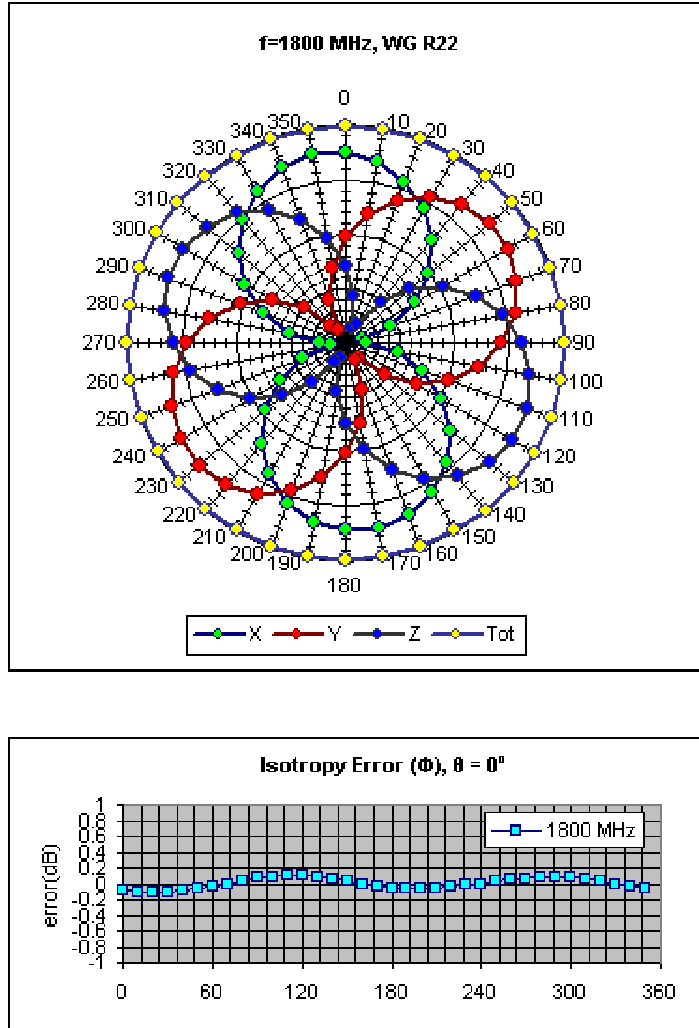


Figure 5. Example of the rotational isotropy of probe S/N 0149 obtained by rotating the probe in a liquid-filled waveguide at 1800 MHz. Similar distributions are obtained at the other test Frequencies (900 and 2450 MHz) both in brain liquids and body fluids (see summary table).

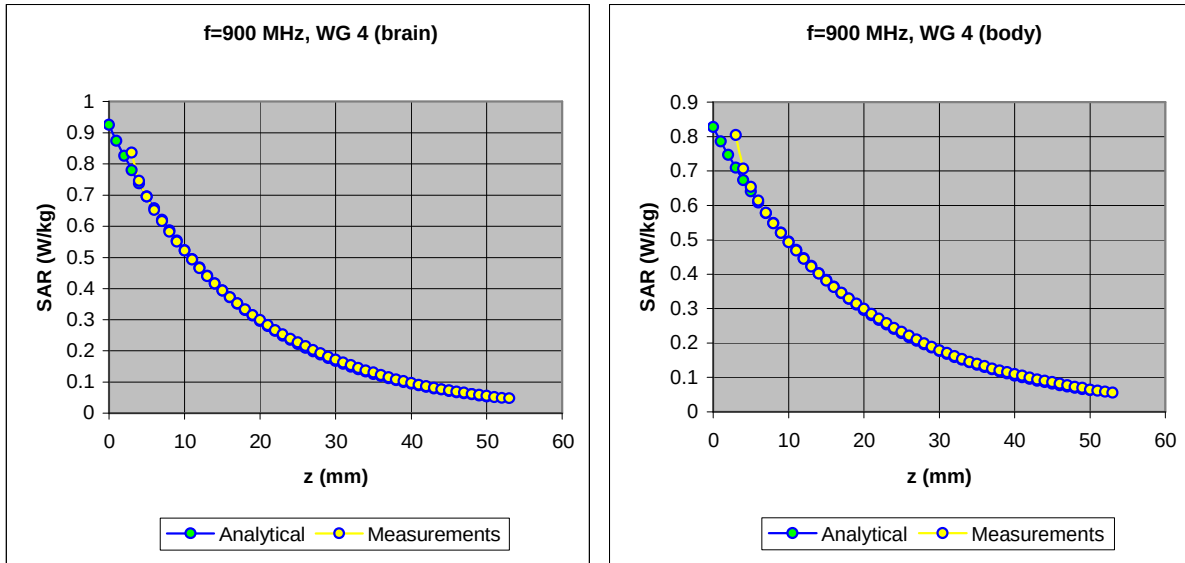
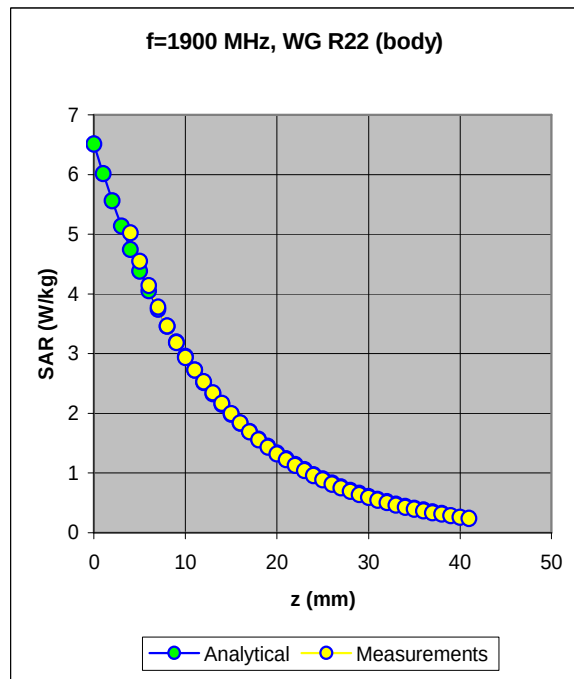
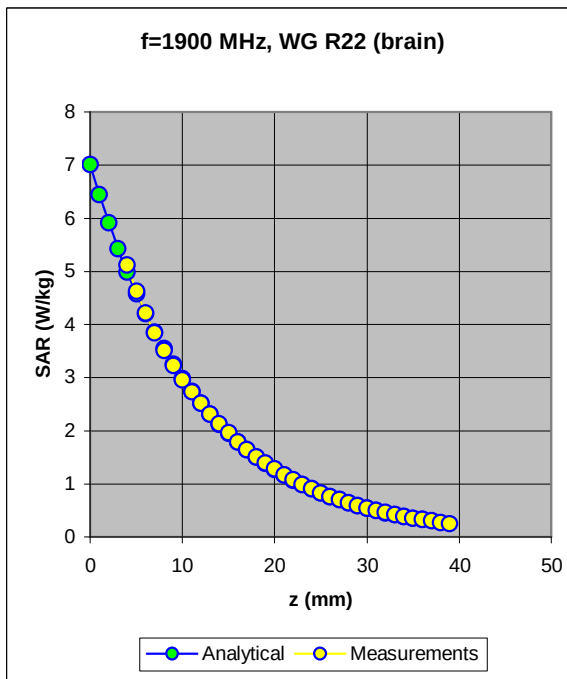
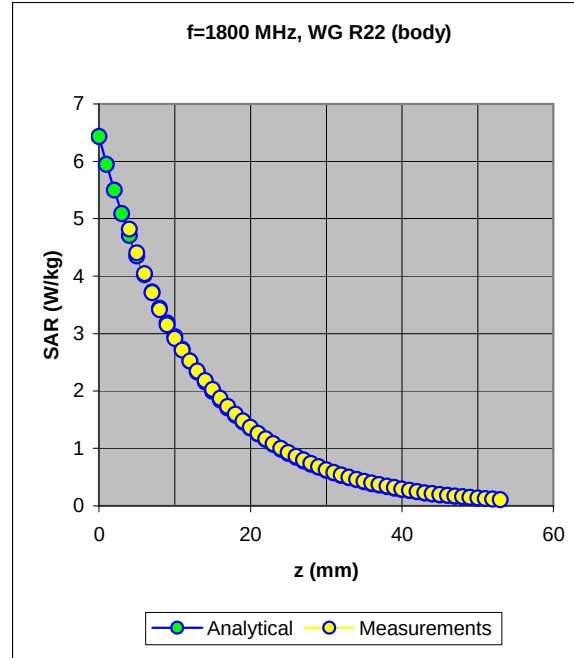
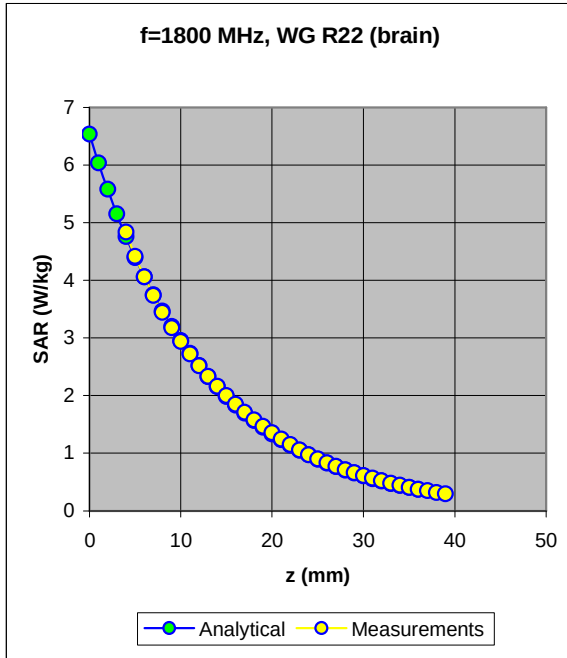


Figure 6. The measured SAR decay function along the centreline of the WG4 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.



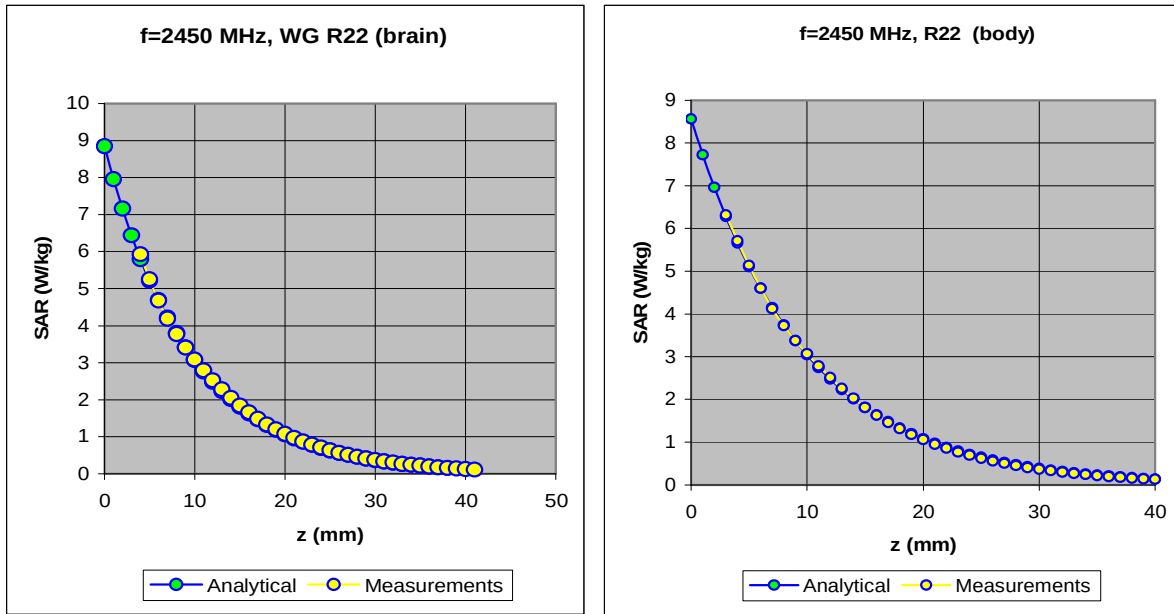


Figure 7. The measured SAR decay function along the centreline of the R22 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.

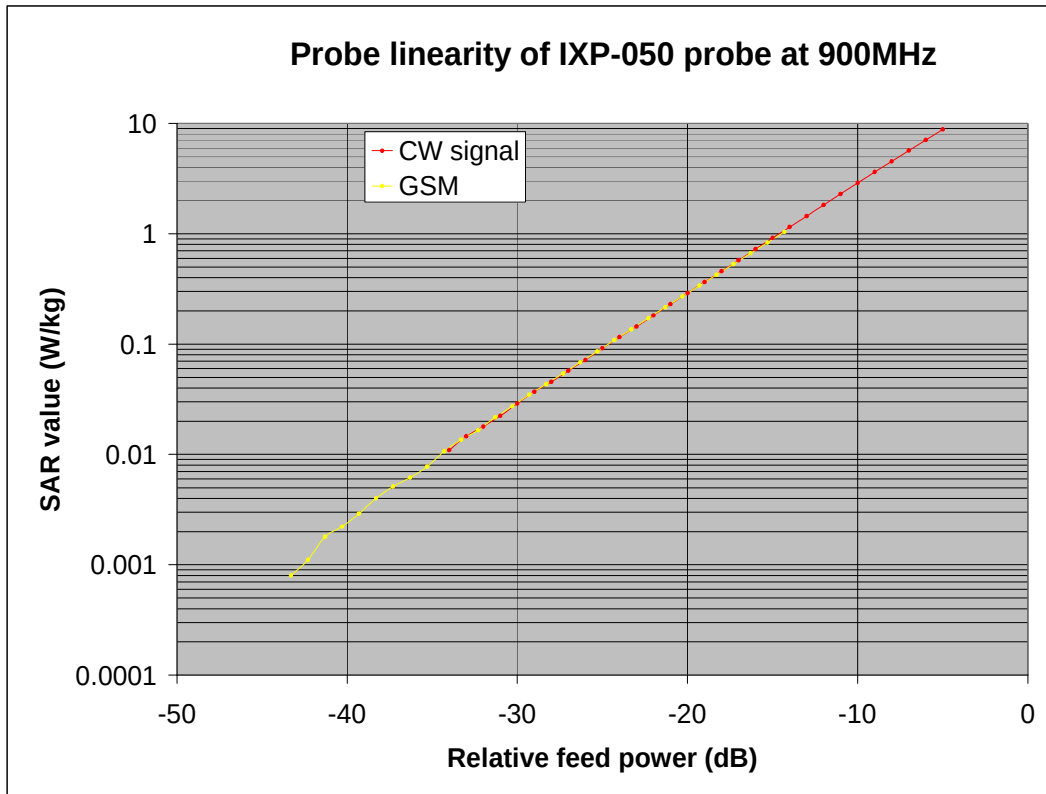


Figure 8. The GSM response of an IXP-050 probe at 900MHz

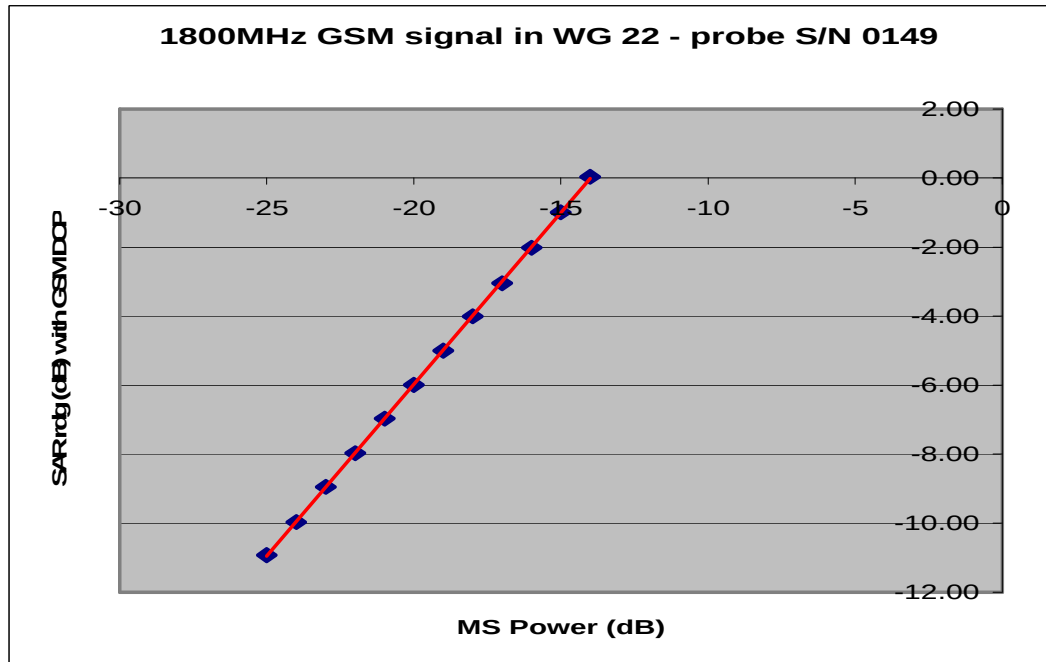


Figure 8a. The actual GSM response of IXP-050 probe S/N 0149 at 1800MHz

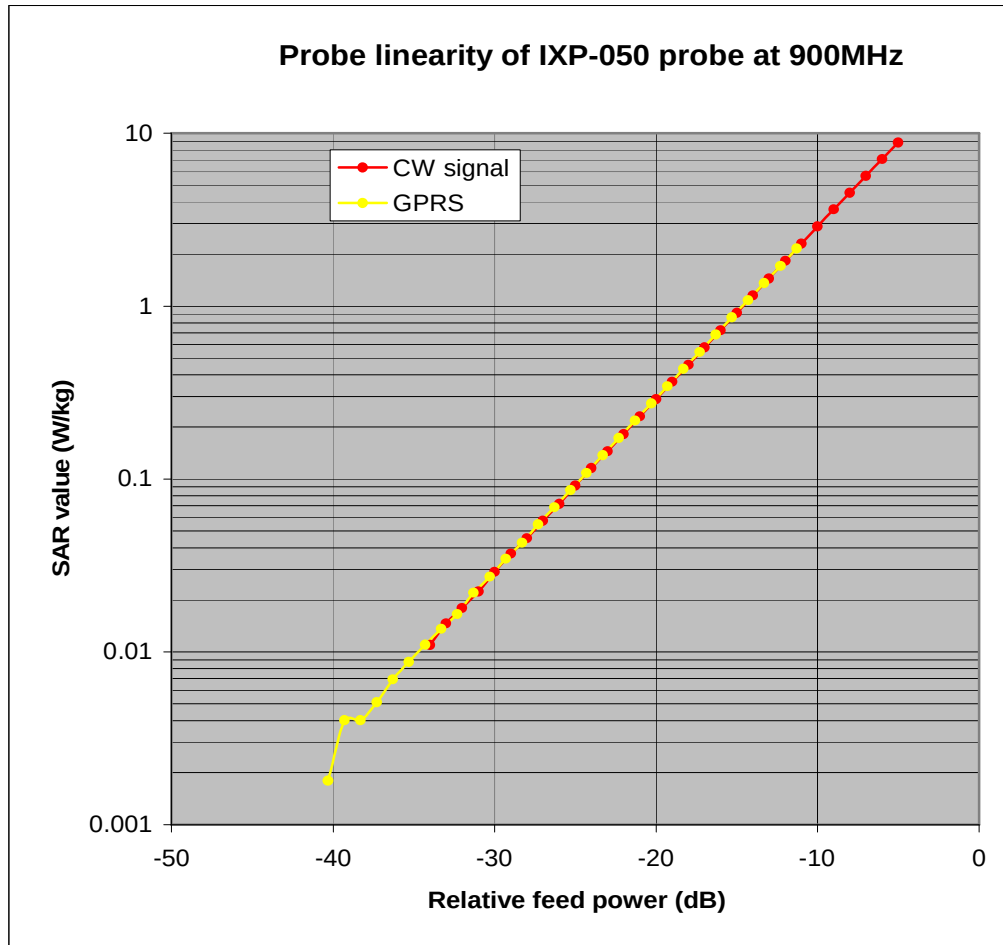


Figure 9. The GPRS response of an IXP-050 probe at 900MHz.

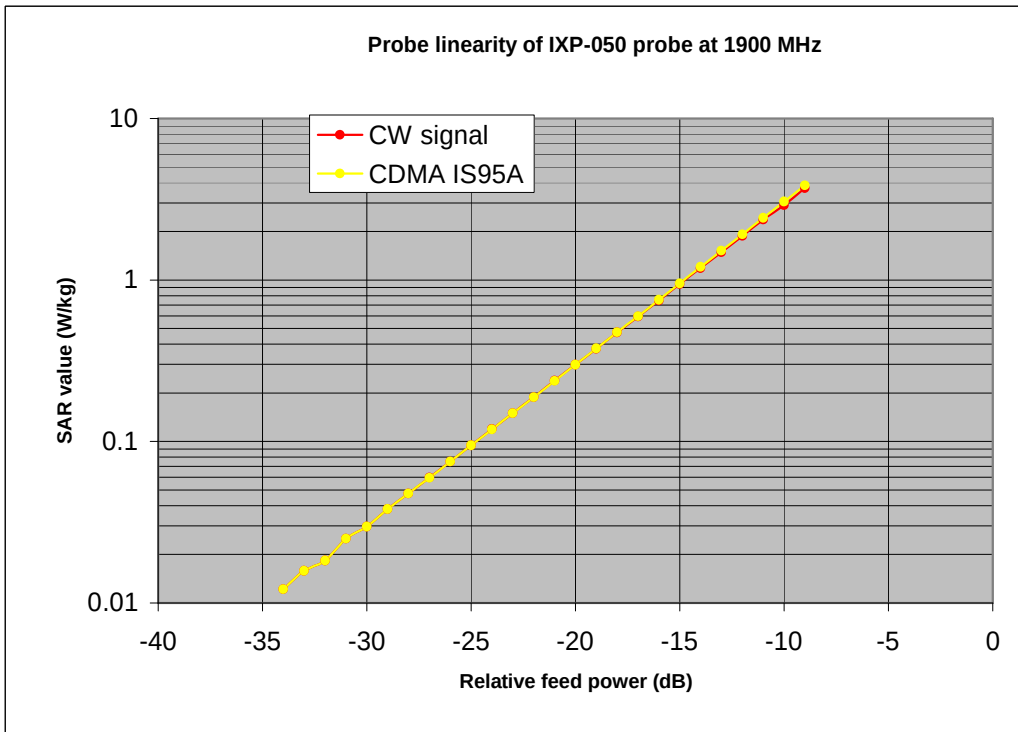
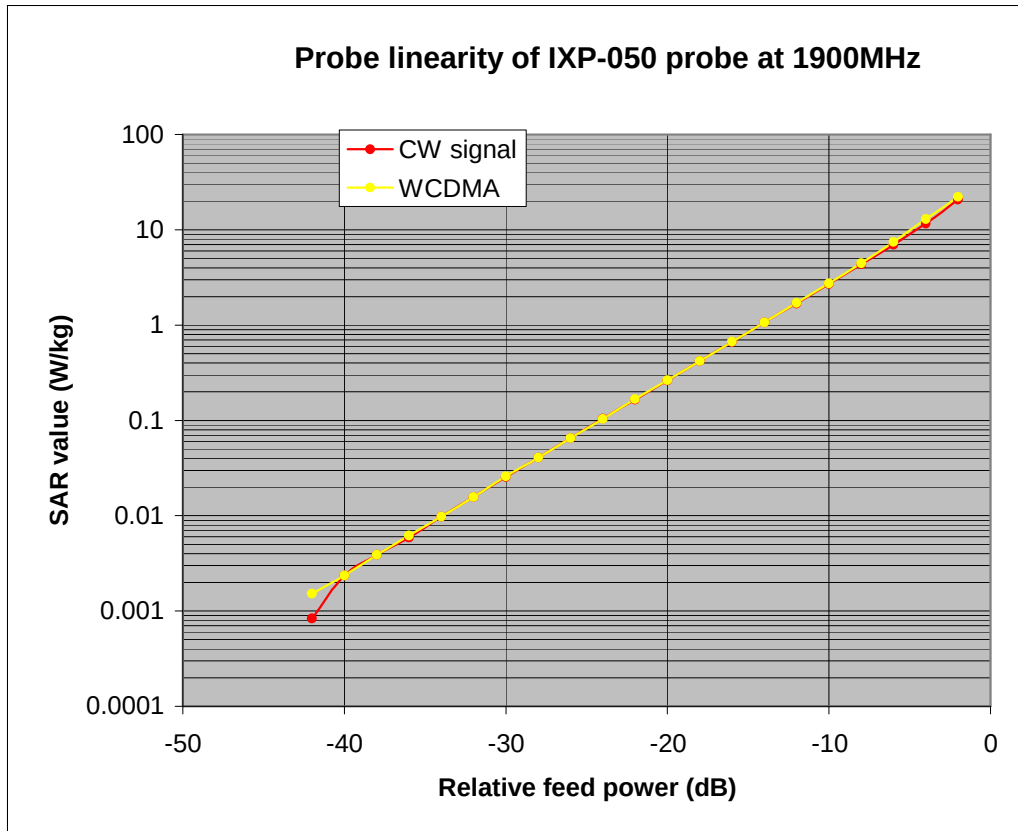


Figure 10. The CDMA response of an IXP-050 probe at 1900MHz.

Table indicating the dielectric parameters of the liquids used for calibrations at each frequency

<i>Liquid used</i>	<i>Relative permittivity (measured)</i>	<i>Conductivity (S/m) (measured)</i>
<i>900 MHz BRAIN</i>	<i>40.92</i>	<i>0.99</i>
<i>900 MHz BODY</i>	<i>57.27</i>	<i>1.045</i>
<i>1800 MHz BRAIN</i>	<i>40.63</i>	<i>1.37</i>
<i>1800 MHz BODY</i>	<i>52.89</i>	<i>1.53</i>
<i>1900 MHz BRAIN</i>	<i>40.33</i>	<i>1.47</i>
<i>1900 MHz BODY</i>	<i>52.84</i>	<i>1.55</i>
<i>2450 MHz BRAIN</i>	<i>40.73</i>	<i>1.82</i>
<i>2450 MHz BODY</i>	<i>54.56</i>	<i>2.04</i>

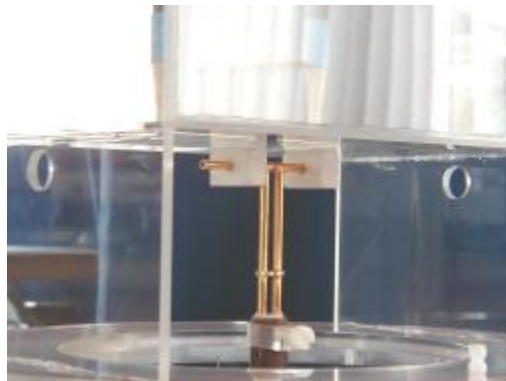


Report No. SN0048_2450
26th March 2003

INDEXSAR
2450MHz validation Dipole
Type IXD-245 S/N 0048

Performance measurements

- *MI Manning*



**Indexsar, Oakfield House, Cudworth Lane,
Newdigate, Surrey RH5 5DR. UK.**
Tel: +44 (0) 1306 631233 Fax: +44 (0) 1306 631834
e-mail: enquiries@indexsar.com

**Calibration / Conformance statement****Balanced Validation dipole**

Type:	IXD-245 2450MHz
-------	-----------------

Manufacturer:	IndexSAR, UK
---------------	--------------

Serial Number:	0048
----------------	------

Place of Calibration:	IndexSAR, UK
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IndexSAR Limited hereby declares that the IXD series dipole named above has been checked for conformity to the specifications given in the draft IEEE 1528 and CENELEC En 50361 standards on the date shown below.

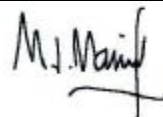
Date of Calibration/Check:	26 th March 2003
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The dipole named above should be periodically re-checked using the procedures set out in the dipole calibration document. It is important that the cautions regarding handling of the dipoles (given in the calibration document) are adhered to.

Next Calibration Date:	March 2005
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The calibration measurements were carried out using the methods described in the calibration document. Where applicable, the standards used in the calibration process are traceable to the UK's National Physical Laboratory.

Calibrated By:	
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Approved By:	
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1. Tests on Validation Dipole

Tests have been performed on a balanced dipole made for 2450MHz application according to the construction guidelines, dimensions and tolerances given in the draft IEEE1528 standard [1]. Measurements have been made of the impedance and return loss when positioned against the liquid-filled phantom and a validation test has been performed according to the procedures set out in IEEE 1528 [1].

2. Measurement Conditions

Measurements were performed using a box-shaped phantom made of PMMA with dimensions designed to meet the accuracy criteria for reasonably-sized phantoms that do not have liquid capacities substantially in excess of the volume of liquid required to fill the Indexsar upright SAM phantoms used for SAR testing of handsets against the ear.

An HP 8753B vector network analyser was used for the return loss measurements.

The dipole was placed in a special holder made of low-permittivity, low-loss materials. This holder enables the dipole to be positioned accurately in the centre of the base of the Indexsar box-phantom used for flat-surface testing and validation checks.

The validation dipoles are supplied with special spacers made from a low-permittivity, low-loss foam material. These spacers are fitted to the dipole arms to ensure that, when the dipole is offered up to the phantom surface, the spacing between the dipole and the liquid surface is accurately aligned according to the guidance in the relevant standards documentation. The spacers are rectangular with a central hole equal to the dipole arm diameter and dimensioned so that the longer side can be used to ensure a spacing of 15mm from the liquid in the phantom (for tests at 900MHz and below) and the shorter side can be used for tests at 1800MHz and above to ensure a spacing of 10mm from the liquid in the phantom. The spacers are made on a CNC milling machine with an accuracy of 1/40th mm but they may suffer wear and tear and need to be replaced periodically. The material used is Rohacell, which has a relative permittivity of approx. 1.05 and a negligible loss tangent.

The apparatus supplied by Indexsar for dipole validation tests thus includes:

Balanced dipoles for each frequency required are dimensioned according to the guidelines given in IEEE 1528 [1]. The dipoles are made from semi-rigid 50 Ohm co-ax, which is joined by soldering and is gold-plated subsequently. The constructed dipoles are easily deformed, if mis-handled, and periodic checks need to be made of their symmetry.

Rohacell foam spacers designed for presenting the dipoles to 2mm thick PMMA box phantoms. These components also suffer wear and tear and should be replaced when the central hole is a loose-fit on the dipole arms or if the edges are too worn to ensure accurate alignment. The standard spacers are dimensioned for use with 2mm wall thickness (additional spacers are available for 4mm wall thickness).

3. SAR Validation Measurement

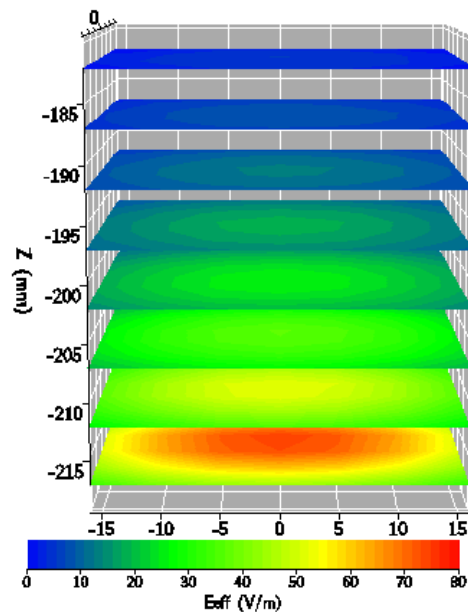
A SAR validation check was performed with the box-phantom located on the SARA2 phantom support base on the SARA2 robot system. Tests were then conducted at a feed power level of approx. 0.25W. The actual power level was recorded and used to normalise the results obtained to the standard input power conditions of 1W (forward power). The ambient temperature was 24°C.

The phantom was filled with a 2450MHz brain liquid using a recipe from [1], which was measured using an Indexsar DiLine kit at 2450MHz. Measurements were taken at 23°C and 30°C and interpolation was used to find the properties at 24°C which were as below:

Relative Permittivity **39.221**
Conductivity **1.8714 S/m**

The SARA2 software version 0.420N was used with an Indexsar probe previously calibrated using waveguide techniques.

The 3D measurement made using the dipole at the bottom of the phantom box is shown below:



The volume-averaged SAR results, normalised to an input power of 1W (forward power) are:

Averaged over 1 cm³ (1g) of tissue **51.376 W/kg**
Averaged over 10cm³ (10g) of tissue **23.888 W/kg**

These results can be compared with Table 8.1 in [1]. The agreement is within 10%.

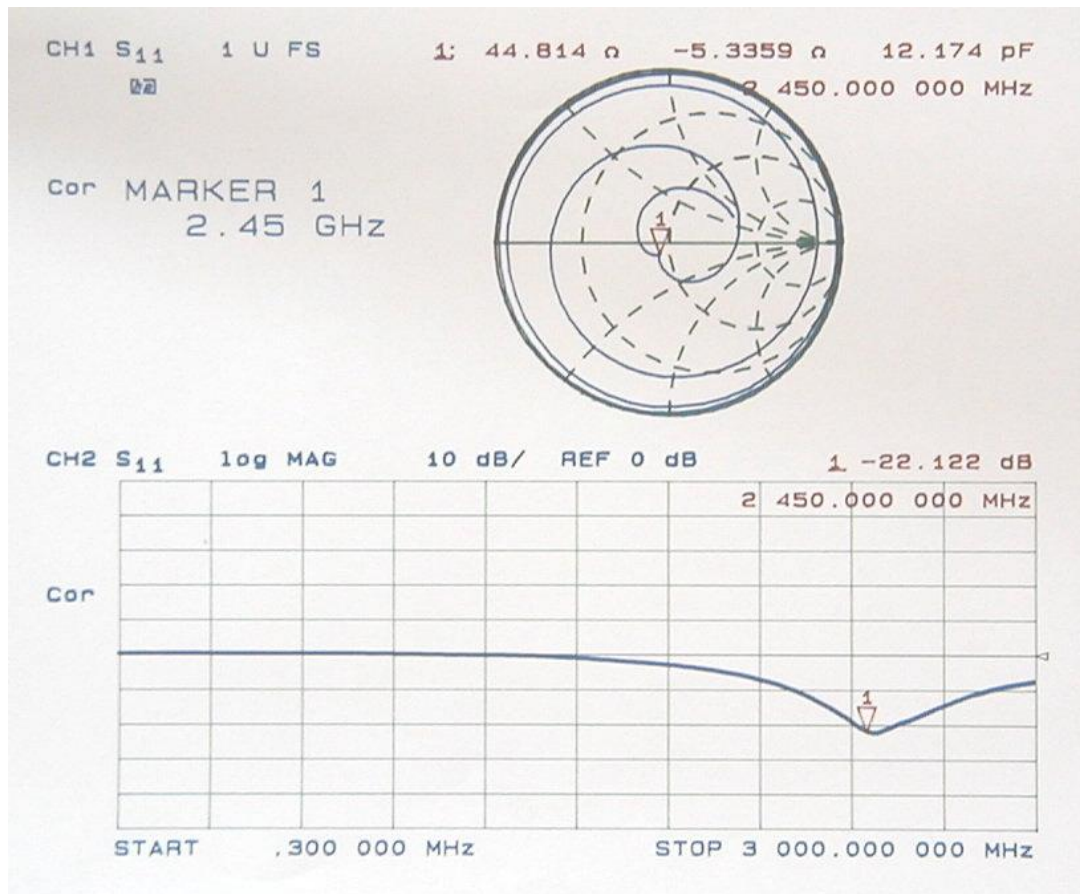
4. Dipole impedance and return loss

The dipoles are designed to have low return loss ONLY when presented against a lossy-phantom at the specified distance. A Vector Network Analyser (VNA) was used to perform a return loss measurement on the specific dipole when in the measurement-location against the box phantom. The distance was as specified in the standard i.e. 10mm from the liquid (for 2450MHz). The Indexsar foam spacers (described above) were used to ensure this condition during measurement.

The impedance was measured at the SMA-connector with the network analyser.
The following parameters were measured:

Dipole impedance at 2450 MHz $\text{Re}\{Z\} = 44.814 \Omega$
 $\text{Im}\{Z\} = -5.3359 \Omega$

Return loss at 2450MHz **-22.122 dB**



5. Dipole handling

The dipoles are made from standard, copper-sheathed coaxial cable. In assembly, the sections are joined using ordinary soft-soldering. This is necessary to avoid excessive heat input in manufacture, which would destroy the polythene dielectric used for the cable. The consequence of the construction material and the assembly technique is that the dipoles are fragile and can be deformed by rough handling. Conversely, they can be straightened quite easily as described in this report.

If a dipole is suspected of being deformed, a normal workshop lathe can be used as an alignment jig to restore the symmetry. To do this, the dipole is first placed in the headstock of the lathe (centred on the plastic or brass spacers) and the headstock is rotated by hand (do NOT use the motor). A marker (lathe tool or similar) is brought up close to the end of one dipole arm and then the headstock is rotated by 0.5 rev. to check the opposing arm. If they are not balanced, judicious deformation of the arms can be used to restore the symmetry.

If a dipole has a failed solder joint, the dipole can be fixed down in such a way that the arms are co-linear and the joint re-soldered with a reasonably-powerful electrical soldering iron. Do not use gas soldering irons. After such a repair, electrical tests must be performed as described below.

Please note that, because of their construction, the dipoles are short-circuited for DC signals.

6. Tuning the dipole

The dipole dimensions are based on calculations that assumed specific liquid dielectric properties. If the liquid dielectric properties are somewhat different, the dipole tuning will also vary. A pragmatic way of accounting for variations in liquid properties is to 'tune' the dipole (by applying minor variations to its effective length). For this purpose, Indexsar can supply short brass tube lengths to extend the length of the dipole and thus 'tune' the dipole. It cannot be made shorter without removing a bit from the arm. An alternative way to tune the dipole is to use copper shielding tape to extend the effective length of the dipole. Do both arms equally.

It should be possible to tune a dipole as described, whilst in place in the measurement position as long as the user has access to a VNA for determining the return loss.

7. Reference

[1] Draft recommended practice for determining the peak spatial-average specific absorption rate (SAR) in the human body due to wireless communications devices: Measurement Techniques. Draft CD1.1 – December 29, 2002.